

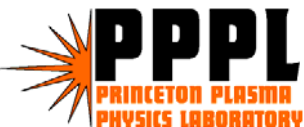
Tokamak Pellet and Gas Fueling Simulations

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Collaborators

- P. Colella and Applied Numerical Algorithms Group (LBNL)
- S. C. Jardin (PPPL)
- P. Parks (GA)
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Outline

- Introduction and motivation
- Description of physical phenomenon
 - *Spatial and temporal scales*
- Equations and models
- Adaptive mesh refinement (AMR) for shaped plasma in flux-tube coordinates
- Results
 - *HFS vs. LFS Pellet injection*
- Supersonic Gas Injection
 - *Nozzle results*
- Future Directions and Conclusion

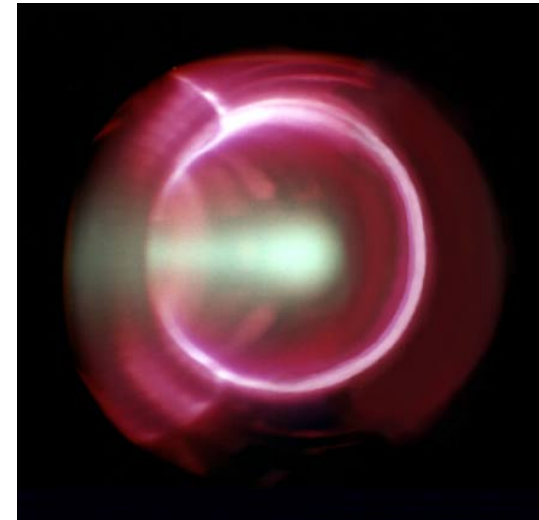
Pellet Injection: Objective and Motivation

- Motivation

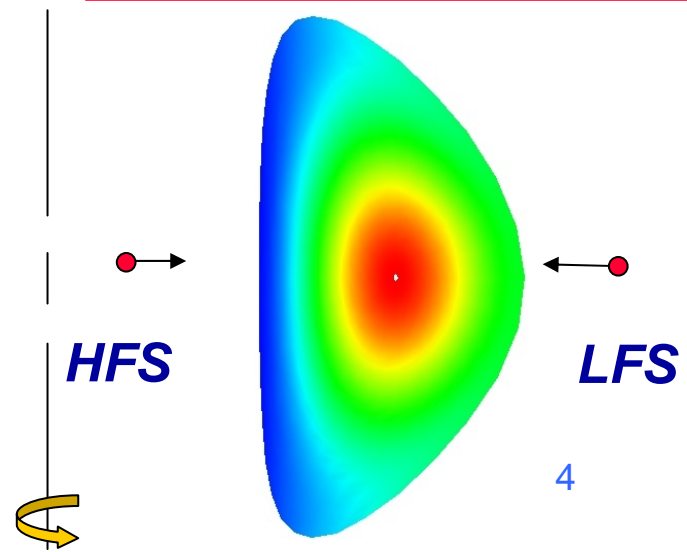
- *Injection of frozen hydrogen pellets is a viable method of fueling a tokamak*
- *Presently there is no satisfactory simulation or comprehensive predictive model for pellet injection (esp. for ITER)*

- Objectives

- *Develop a comprehensive simulation capability for pellet injection into tokamaks*
- *Identify the mechanisms for mass distribution during pellet injection in tokamaks*
- *Quantify the differences between “inside launch” (HFS) and “outside launch” (LFS)*



Pellet injection in TFTR



Physical Processes: Description

- Non-local electron transport along field lines rapidly heats the pellet cloud (τ_e).
 - Frozen pellet encounters hot plasma and ablates rapidly
 - Neutral gas surrounding the solid pellet is ionized
 - Ionized, but cool plasma, continues to get heated by electrons
 - A high β “plasmoid” is created
- Ionized plasmoid expands
 - Fast magnetosonic time scale τ_f
- Pellet mass moves across flux surfaces τ_a .
 - So-called “anomalous” transport across flux surfaces is accompanied by reconnection
- Pellet mass expands along field lines τ_c .
 - Pellet mass distribution continues along field lines until pressure equilibration
- Pellet lifetime τ_p

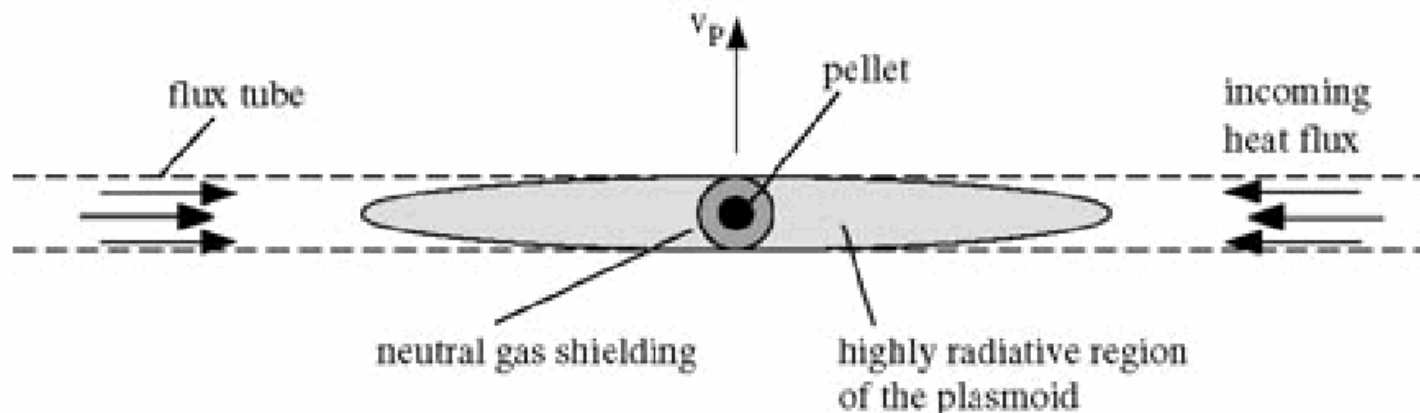


Figure from Müller et al., Nuclear Fusion 42 (2002)

Scales and Resolution Requirements

- Time Scales $\tau_e < \tau_f < \tau_a < \tau_c < \tau_p$
- Spatial scales: Pellet radius $r_p \ll$ Device size $L \sim O(10^{-3})$
- Presence of magnetic reconnection further complicates things
 - *Thickness of resistive layer scales with $\sim \eta^{1/2}$*
 - *Time scale for reconnection is $\sim \eta^{-1/2}$*
- Pellet cloud density $\sim O(10^4)$ times ambient plasma density
- Electron heat flux is non-local
- Large pressure and density gradients in the vicinity of cloud
- Pellet lifetime $\sim O(10^{-3})$ s \rightarrow long time integrations

Resolution estimates

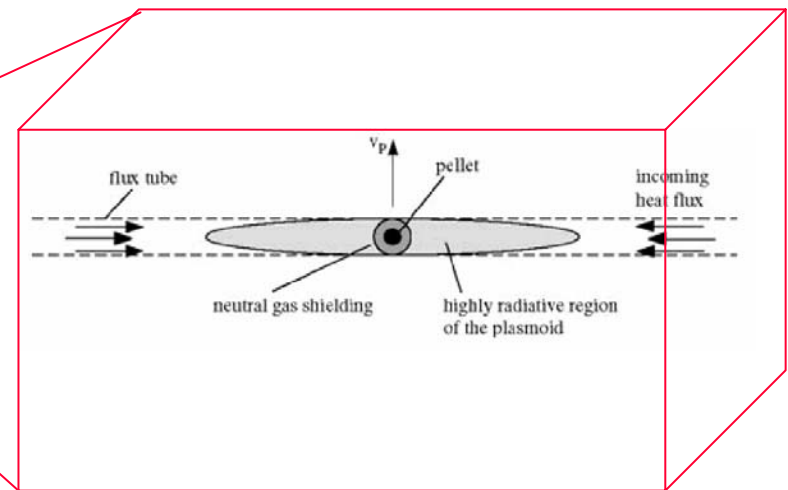
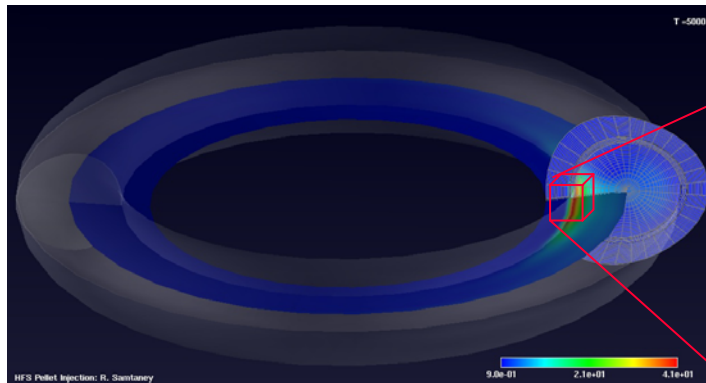
Tokamak	Major Radius	N	N_{steps}	Spacetime Points
CDXU (Small)	0.3	2×10^7	2×10^5	4×10^{12}
DIID (Medium)	1.75	3.3×10^9	7×10^6	2.3×10^{17}
ITER (Large)	6.2	1.5×10^{11}	9×10^7	1.4×10^{19}

Related Work - Local vs. Global Simulations

- Earliest ablation model by Parks (Phys. Fluids 1978)
 - Detailed multi-phase calculations in 2D of pellet ablation (MacAulay, PhD thesis, Princeton Univ 1993, Nuclear Fusion 1994)
 - Detailed 2D Simulations of pellet ablation by Ishizaki, Parks et al. (Phys. Plasmas 2004)
 - *Included atomic processes – ablation, dissociation, ionization, pellet fluidization and distortion, and Semi-analytical model for electron heat flux from background plasma*
 - In above studies, the domain of investigation was restricted to only a few cm around the pellet
 - *The magnetic field was static*
-
- 3D Simulations by Strauss and Park (Phys. Plasmas, 1998)
 - *Solve an initial value problem. Initial condition consisted of a density “blob” to mimic a fully ablated pellet cloud which, compared with device scales, was relatively large due to resolution restrictions*
 - *No motion of pellet modeled*
 - 3D Adaptive Mesh Simulation of pellet injection by Samtaney et al. (Comput. Phys. Comm, 2004)

Current Work

- Combine global MHD simulations in a tokamak geometry with detailed local physics including ablation, ionization and electron heating in the neighborhood of the pellet



- AMR techniques to mitigate the complexity of the large range of scales in the problem

Equations and Models

- Single fluid resistive MHD equations in conservation form

$$\frac{\partial U}{\partial t} + \underbrace{\left(\frac{1}{R} \frac{\partial RF}{\partial R} + \frac{\partial H}{\partial z} + \frac{1}{R} \frac{\partial G}{\partial \phi} \right)}_{\text{Hyperbolic terms}} = S + \underbrace{\left(\frac{1}{R} \frac{\partial RF_D}{\partial R} + \frac{\partial H_D}{\partial z} + \frac{1}{R} \frac{\partial G_D}{\partial \phi} \right)}_{\text{Diffusive terms}} + S_D + S_{\text{pellet}}$$

Hyperbolic terms

Diffusive terms

Density: Ablation
Energy: Electron heat flux

- Additional constraint $\nabla \cdot \mathbf{B} = 0$
- Mass source is given using the ablation model by Parks and Turnbull (Phy. Plasmas 1978) and Kuteev (Nuclear Fusion 1995)

$$\frac{dN}{dt} = -4\pi r_p^2 \frac{dr_p}{dt} 2n_m = 1.12 \times 10^{16} n_e^{0.333} T_e^{1.64} r_p^{1.33} M_i^{-0.333}$$

- Above equation uses cgs units
- Ablation occurs on the pellet surface $S_n = \dot{N} \delta(x - x_p)$
 - Regularized as a truncated Gaussian of width $10 r_p$
 - Pellet shape is spherical for all t
 - Pellet trajectory is specified as either HFS or LFS
 - Monte Carlo integration to determine average source in each finite volume

Electron Heat Flux Model

- Semi-analytical Model by Parks et al. (Phys. Plasmas 2000)
 - Assumes Maxwellian electrons and neglects pitch angle scattering

$$-\nabla \cdot \mathbf{q}_e = \frac{q_\infty n}{\tau_\infty} [g(u_+) + g(u_-)]$$

Where $g(u) = u^{\frac{1}{2}} K_1(u^{\frac{1}{2}})/4$, $u_\pm = \frac{\tau_\pm}{\tau_\infty}$ and $\tau_\pm = \pm \int_{\mp\infty}^{\mathbf{x}} n(s) ds$

- Solve for opacities as a “steady-state” solution to an advection-reaction equation
 - Upwind method
 - Advection velocity is \mathbf{b}

$$\frac{d\tau}{ds} = n(\mathbf{x}) \quad \hat{\mathbf{b}} \cdot \nabla \tau = n(\mathbf{x})$$

$$\frac{d\tau}{d\zeta} + \hat{\mathbf{b}} \cdot \nabla \tau = n(\mathbf{x})$$

- Ansatz for energy conservation
 - Sink term on flux surface outside cloud

$$-\nabla \cdot \mathbf{q}_e = \frac{1}{V_\psi - V_{cloud,\psi}} \int_{cloud,\psi} \nabla \cdot \mathbf{q}_e$$

Curvilinear coordinates for shaped plasma

- Adopt a flux-tube coordinate system (flux surfaces ψ are determined from a separate equilibrium calculation)

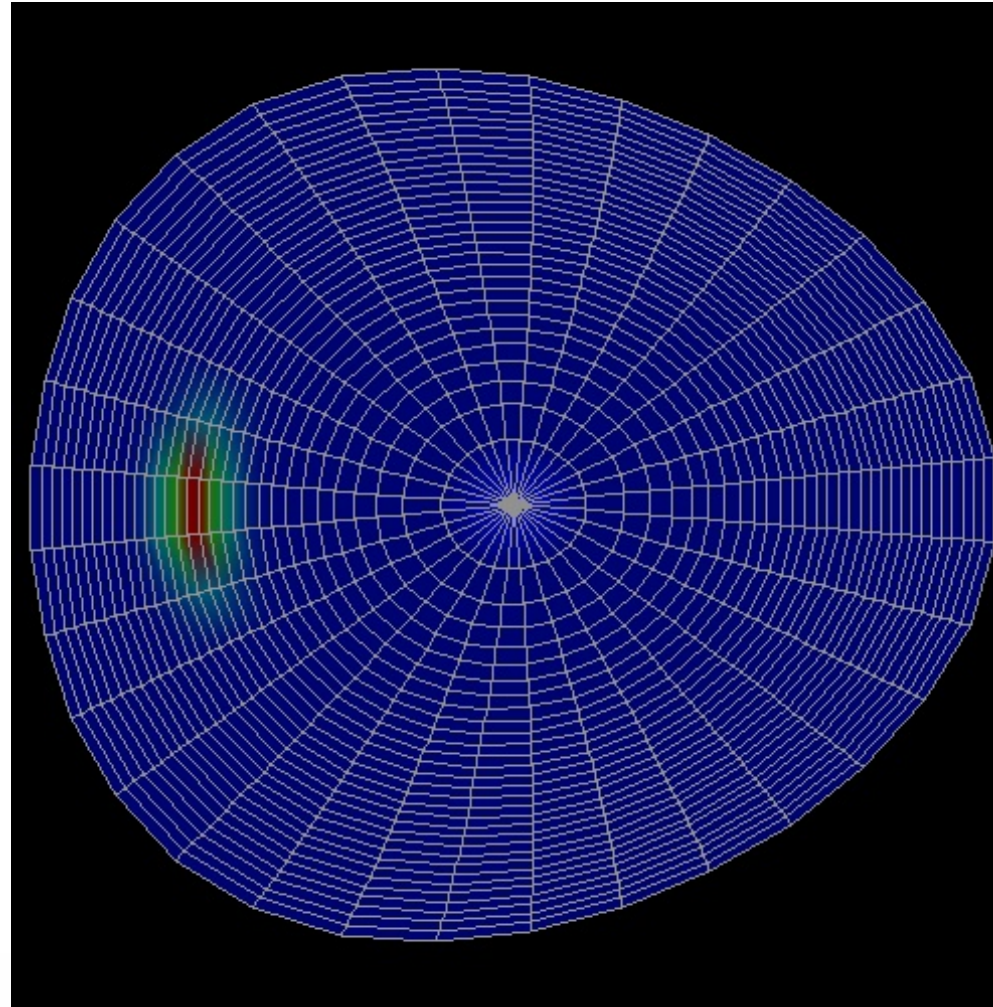
- $R = R(\xi, \eta)$, and $Z = Z(\xi, \eta)$
- $\xi = \xi(R, Z)$, and $\eta = \eta(R, Z)$
- Flux surfaces: $\psi = \psi_0 \xi$
- ϕ coordinate is retained as before

- Equations in transformed coordinates

$$\frac{\partial UJ}{\partial t} + \frac{1}{R} \frac{\partial R\tilde{F}}{\partial \xi} + \frac{1}{R} \frac{\partial R\tilde{H}}{\partial \eta} + \frac{1}{R} \frac{\partial \tilde{G}}{\partial \phi} = \tilde{S}$$

$$\tilde{F} = J(\xi_R F + \xi_z H) = z_\eta F - R_\eta H,$$

$$\tilde{H} = J(\eta_R F + \eta_z H) = -z_\xi F + R_\xi H,$$

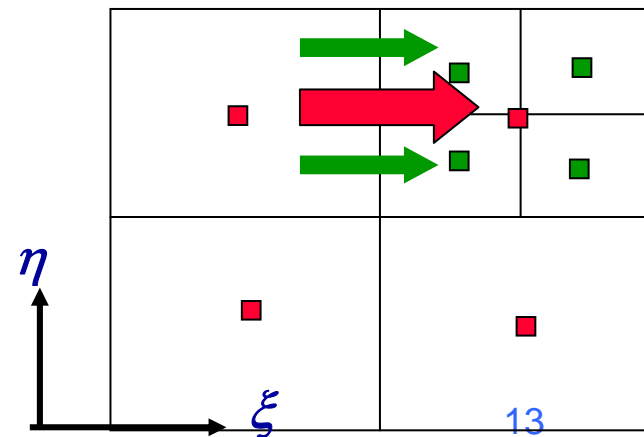


Numerical method

- Finite volume approach
- Explicit second order or third order TVD Runge-Kutta time stepping
- The hyperbolic fluxes are evaluated using upwinding methods
 - *seven-wave Riemann solver*
 - *Harten-Lee-vanLeer (HLL) Method (SIAM Review 1983)*
- Diffusive fluxes computed using standard second order central differences
- The solenoidal condition on \mathbf{B} is imposed using the *Central Difference* version of Constrained Transport (Toth JCP 161, 2000)
 - $\mathbf{r} \cdot \mathbf{B} \neq 0$ on coarse mesh cells adjacent to coarse-fine interfaces
- **Initial Conditions:** Express $\mathbf{B} = 1/R(\phi \mathbf{e}_r \psi + g(\psi) \phi) \neq \text{fnc}(\phi)$. Initial state is an MHD equilibrium obtained from a Grad-Shafranov solver.
- **Boundary Conditions:** Perfectly conducting for $\xi = \xi_0$, zero flux (due to zero area) at $\xi = \xi_i$, and periodic in η and ϕ

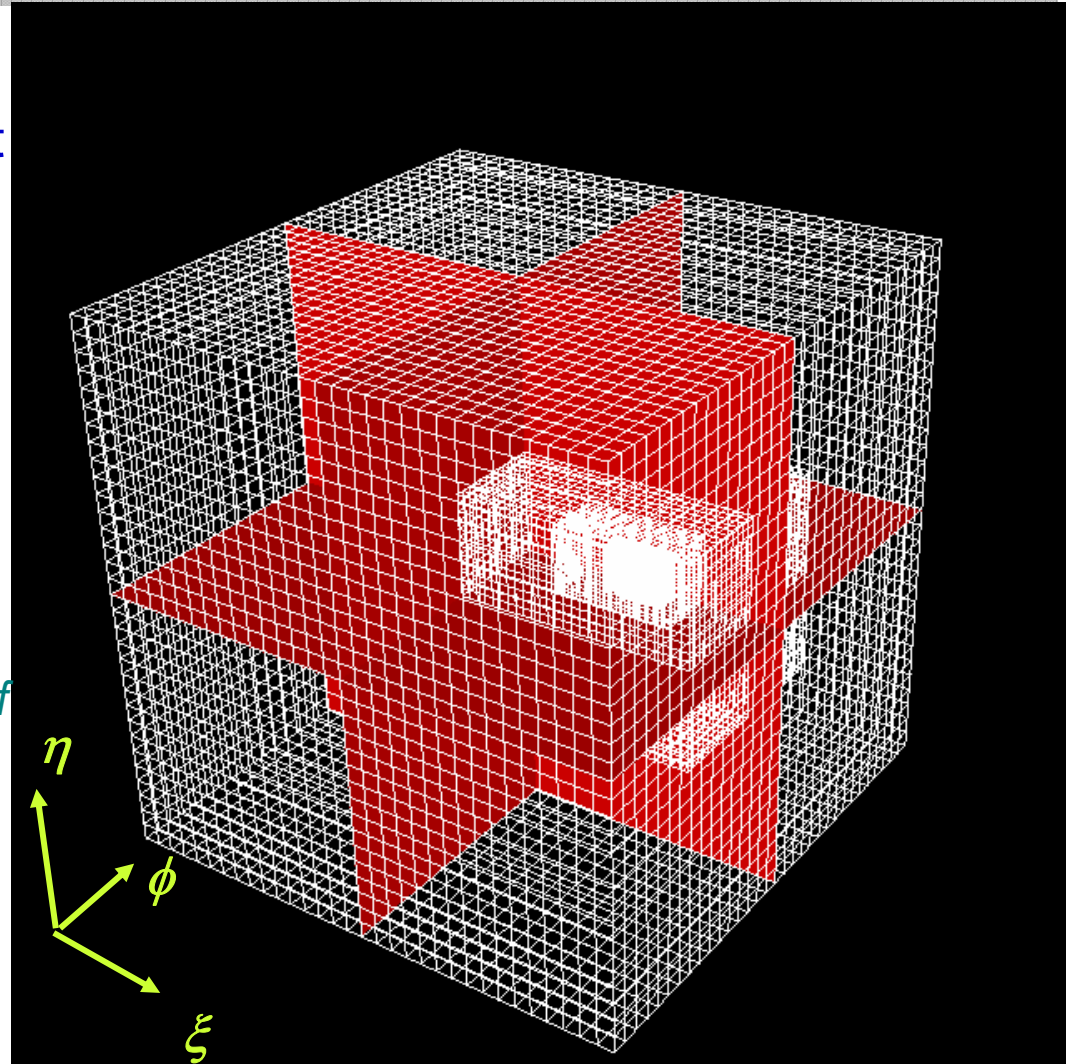
Adaptive Mesh Refinement with Chombo

- **Chombo** is a collection of C++ libraries for implementing block-structured adaptive mesh refinement (AMR) finite difference calculations
(<http://www.seesar.lbl.gov/ANAG/chombo>)
 - *(Chombo is an AMR developer's toolkit)*
- **Adaptivity in both space and time**
- Mesh generation: necessary to ensure volume preservation and areas of faces upon refinement
- Flux-refluxing step at end of time step ensures conservation

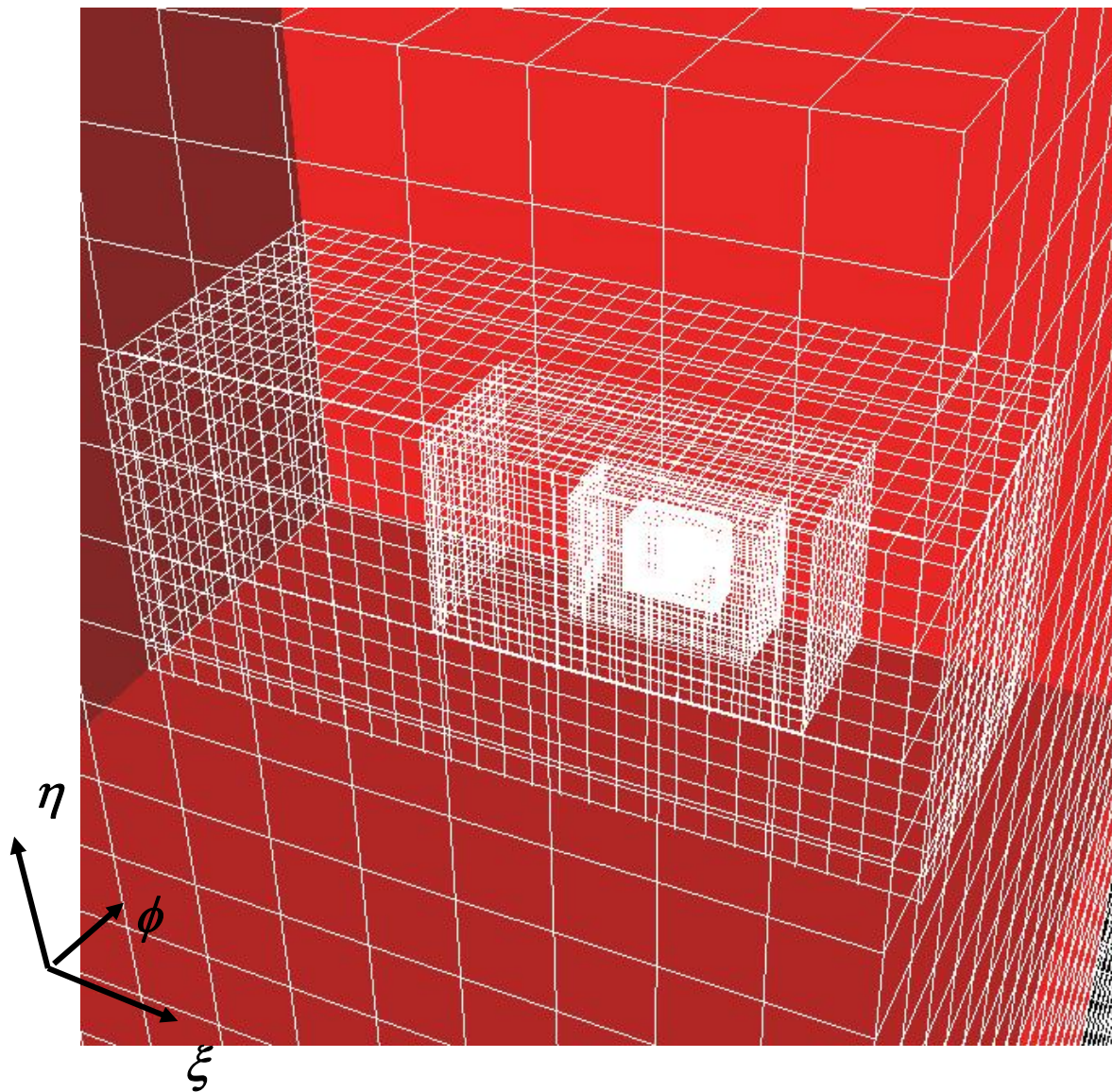


Pellet Injection: AMR

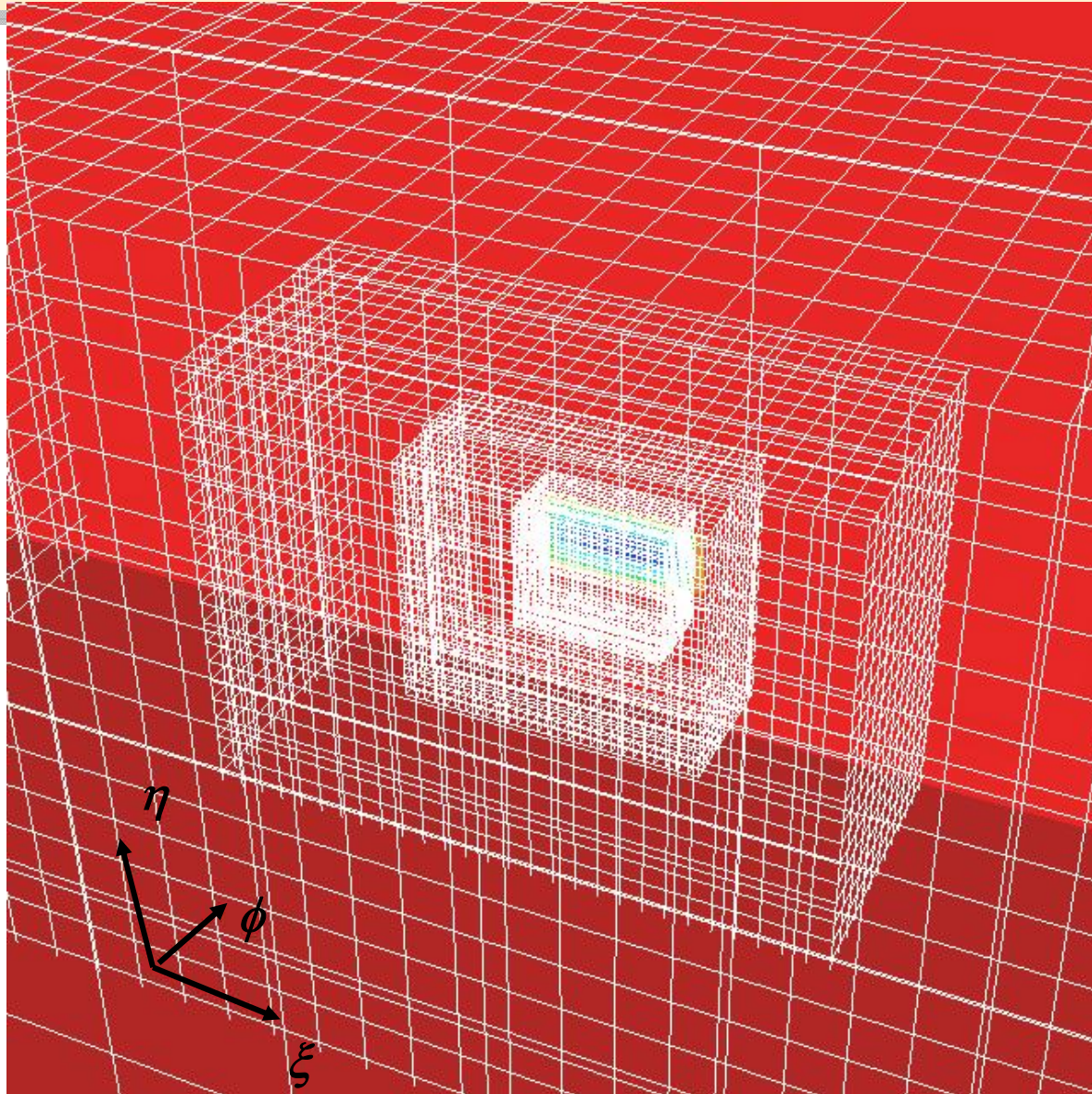
- Meshes clustered around pellet
- Computational space mesh structure shown on right
- Mesh stats
 - 32^3 – base mesh with 5 levels, and refinement factor 2
 - Effective resolution: 1024^3
 - Total number of finite volume cells: 113408
 - Finest mesh covers 0.015 % of the total volume
 - Time adaptivity:
 $1 (\Delta t)_{\text{base}} = 32 (\Delta t)_{\text{finest}}$



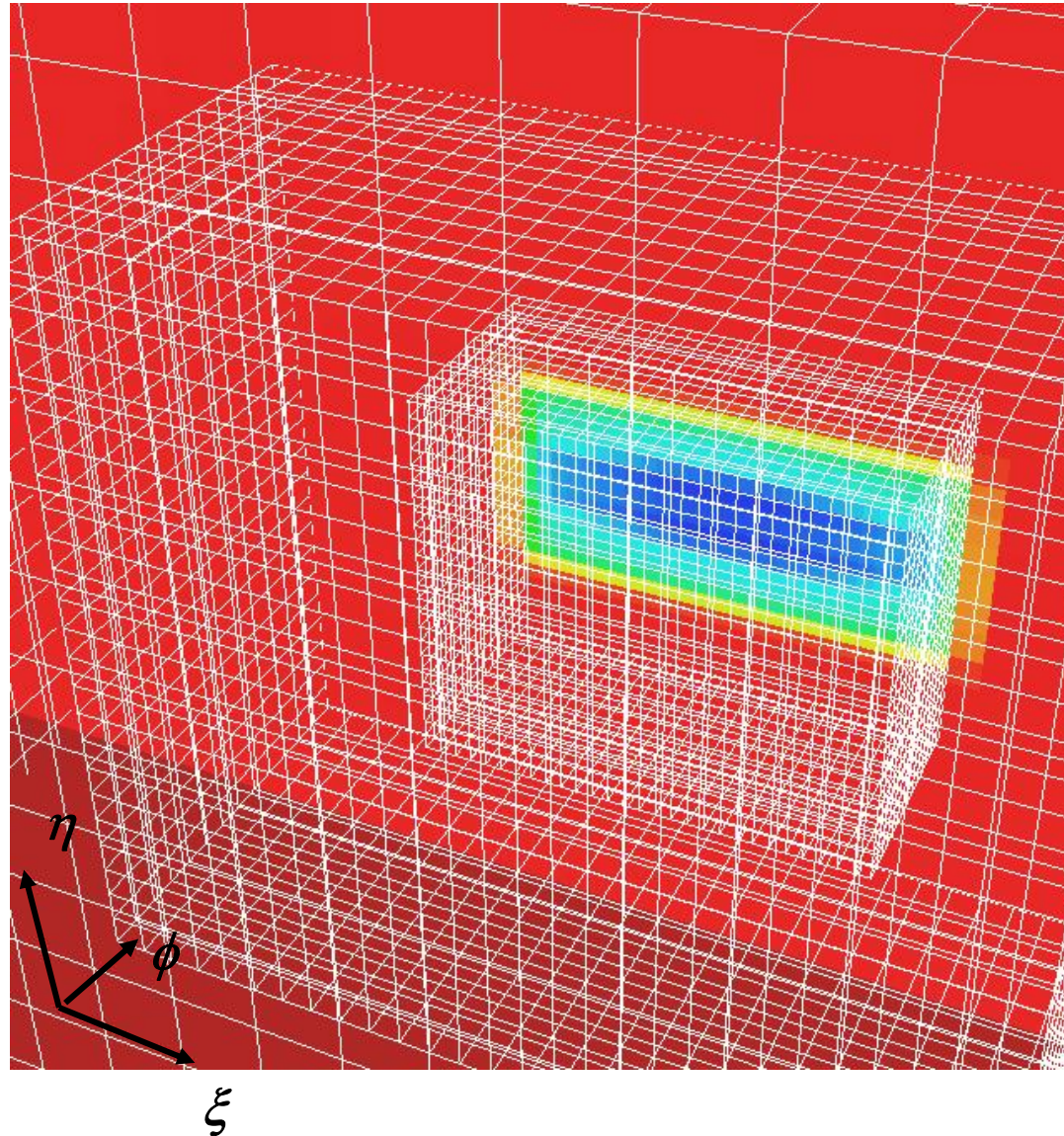
Pellet Injection: Zoom into Pellet Region



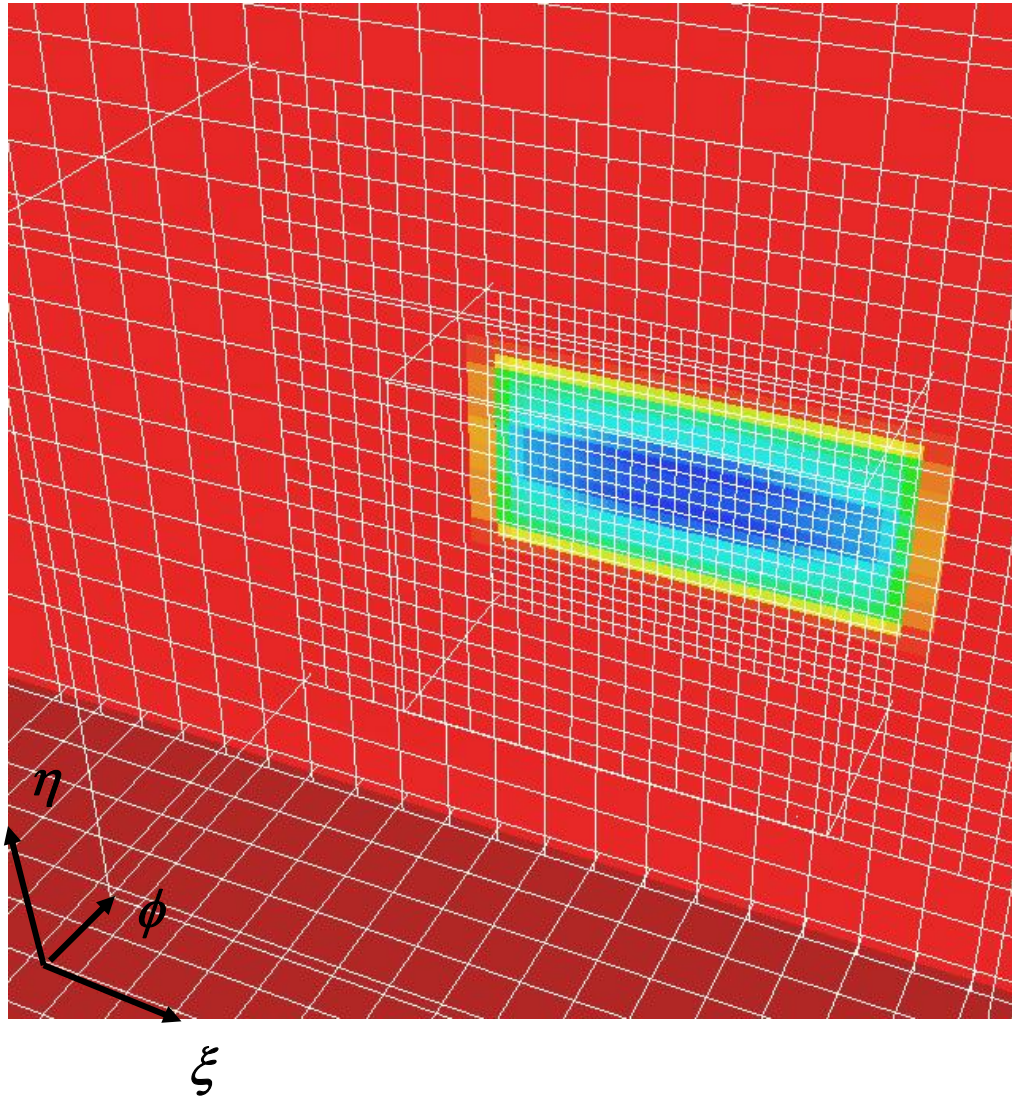
Pellet Injection: Further Zooming In



Pellet Injection: Pellet in Finest Mesh

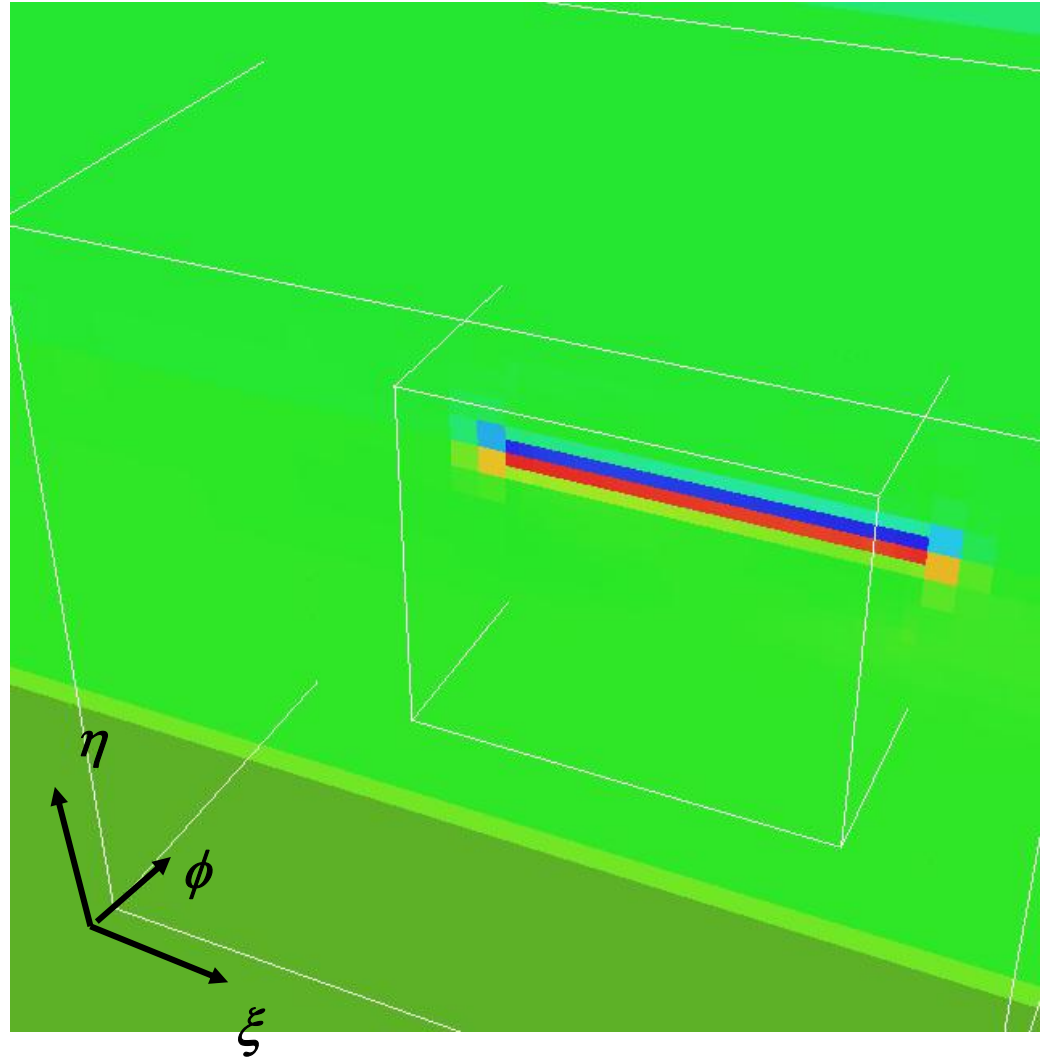


Pellet Injection: Pellet Cloud Density



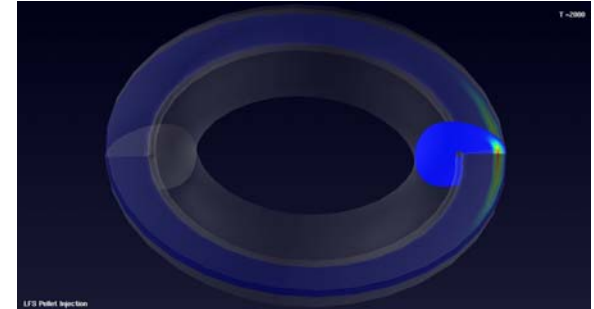
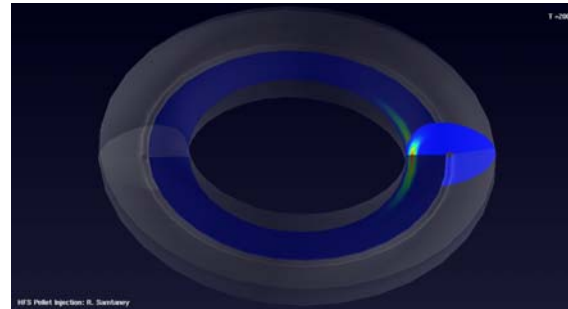
Pellet Injection: Zoom in on B-field

- Radial component of \mathbf{B} is initially zero near pellet
- Classical anti-parallel morphology indicative of reconnection
- B-field of field close to the pellet is distorted

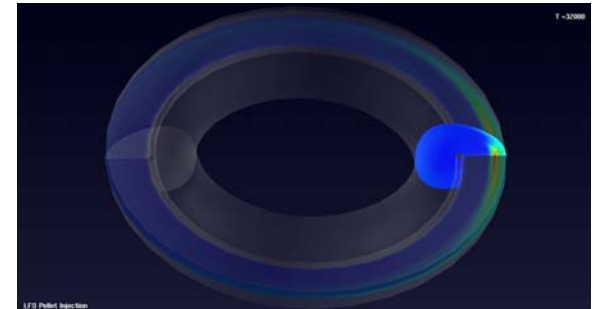


Results - HFS vs. LFS

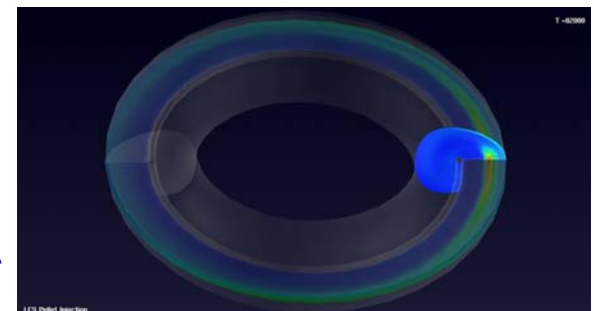
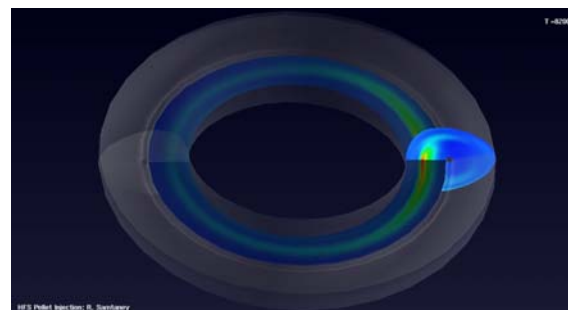
$B_T = 0.375T$
 $n_0 = 1.5 \times 10^{19}/m^3$
 $T_{e1} = 1.3Kev$
 $\beta = 0.05$
 $R_0 = 1m, a = 0.3 m$
 Pellet: $r_p = 1mm,$
 $v_p = 1000m/s$



$t=7$



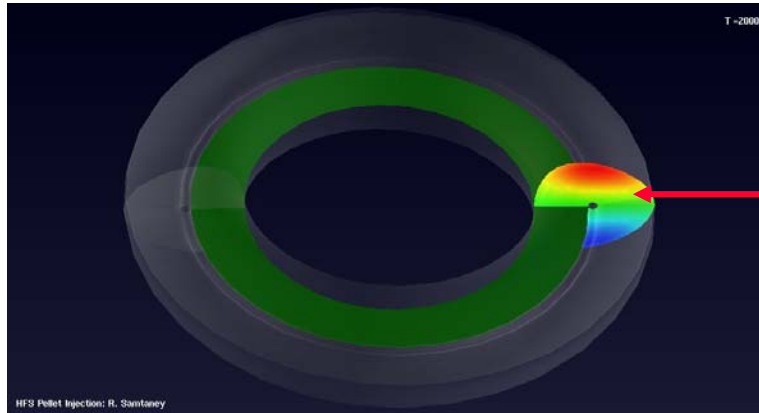
$t=100$



$t=256$

Results - B-field Distortion

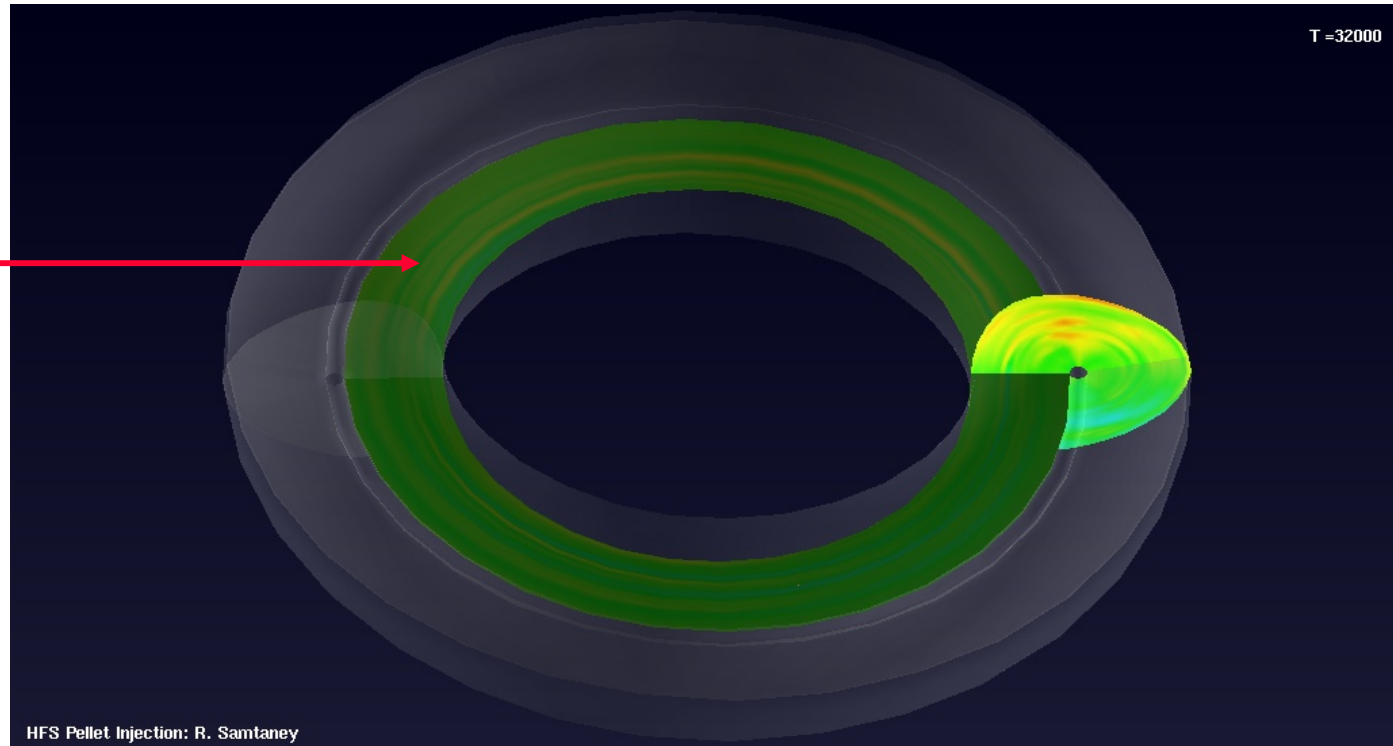
B_R



Initial Equilibrium

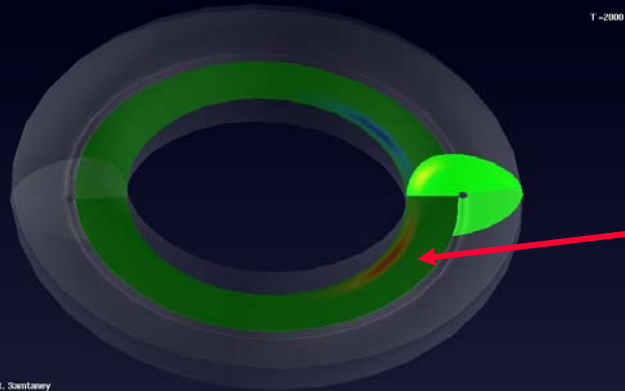
$t=6.2$

Striations



$t=98$

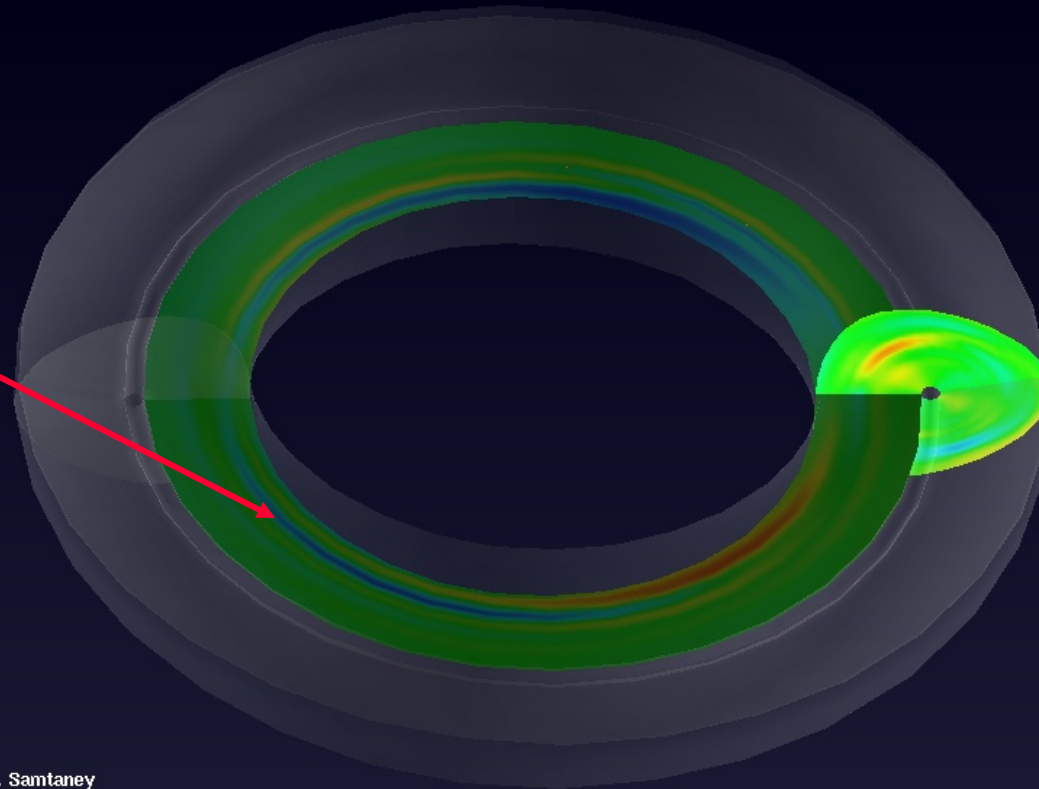
Results - Velocity u_ϕ



*Early expansion
along field lines*

$t=6.2$

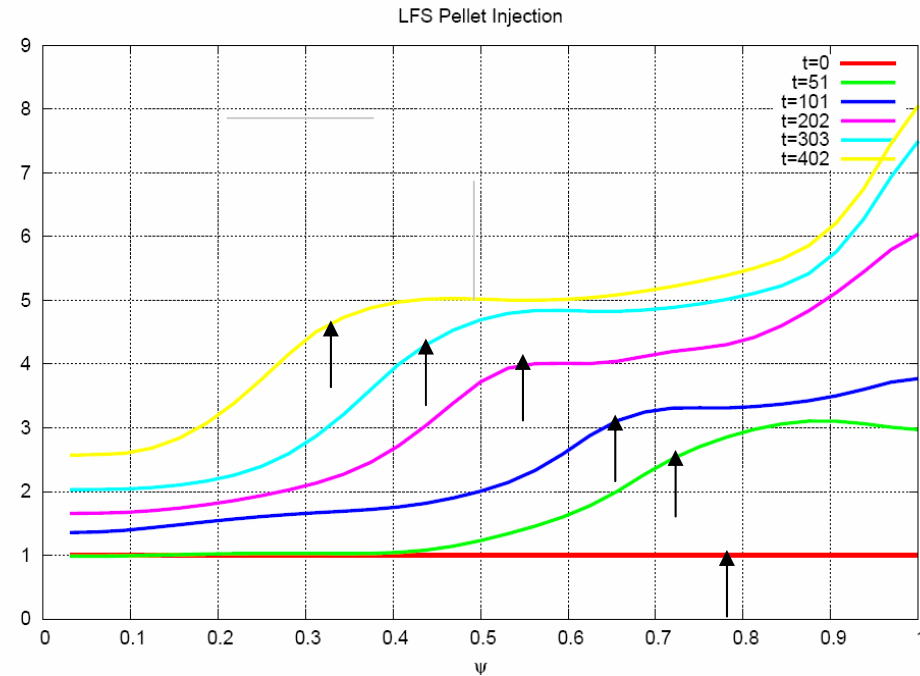
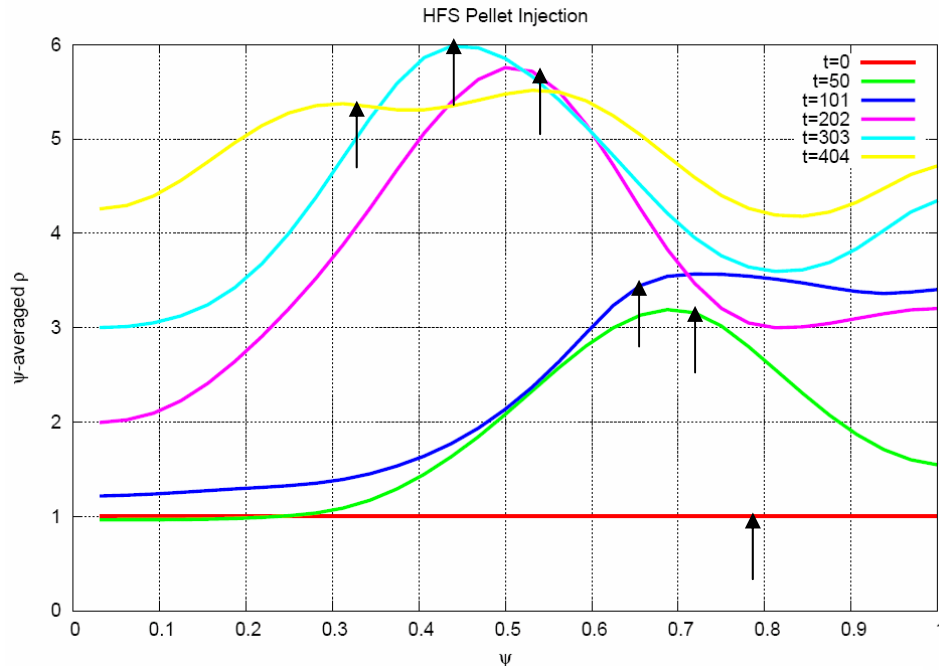
Striations



$t=98$

HFS Pellet Injection: R. Santaney

HFS vs. LFS - Average Density Profiles

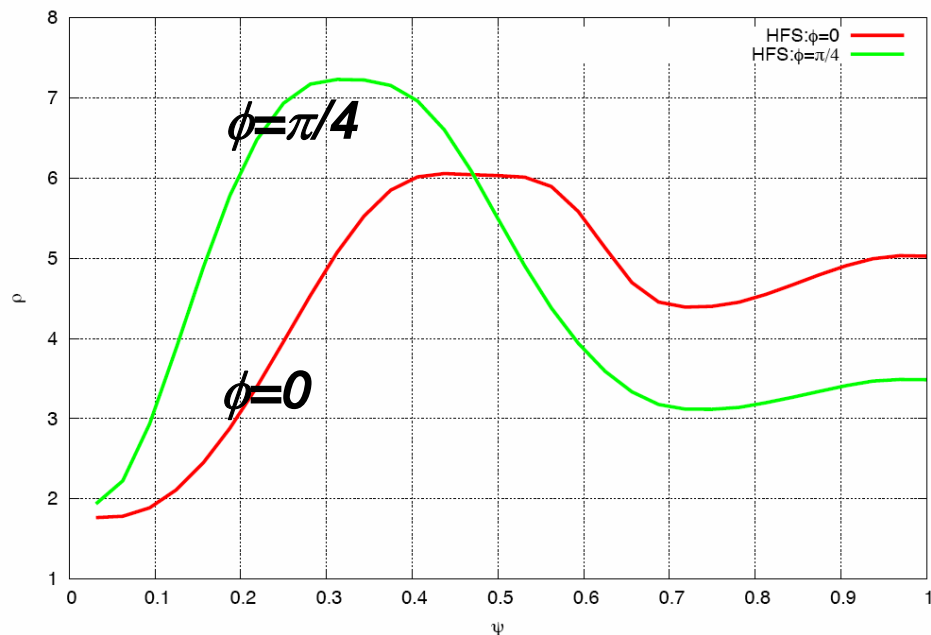


HFS Pellet injection shows better core fueling than LFS

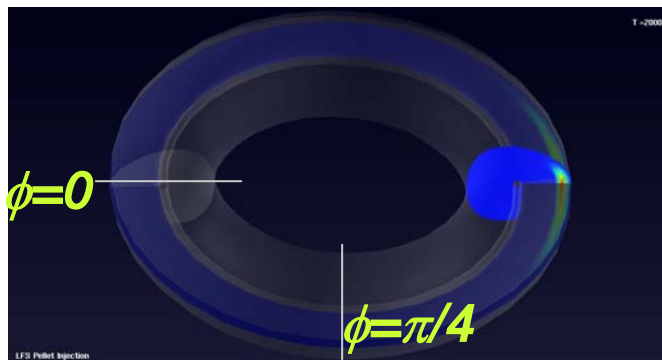
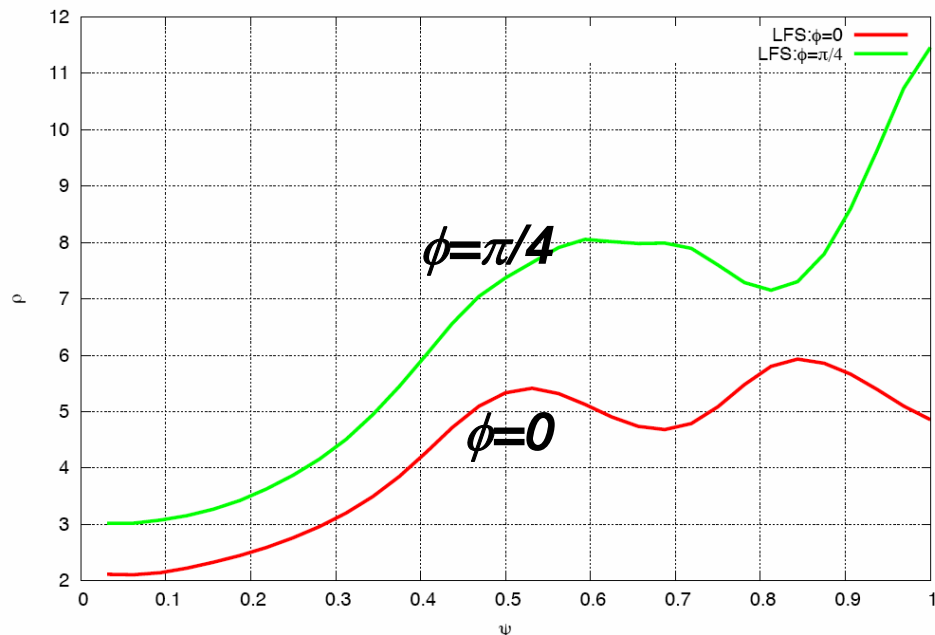
Arrows indicate average pellet location

HFS vs. LFS: Instantaneous Density Profiles

HFS Pellet Injection $t=250$

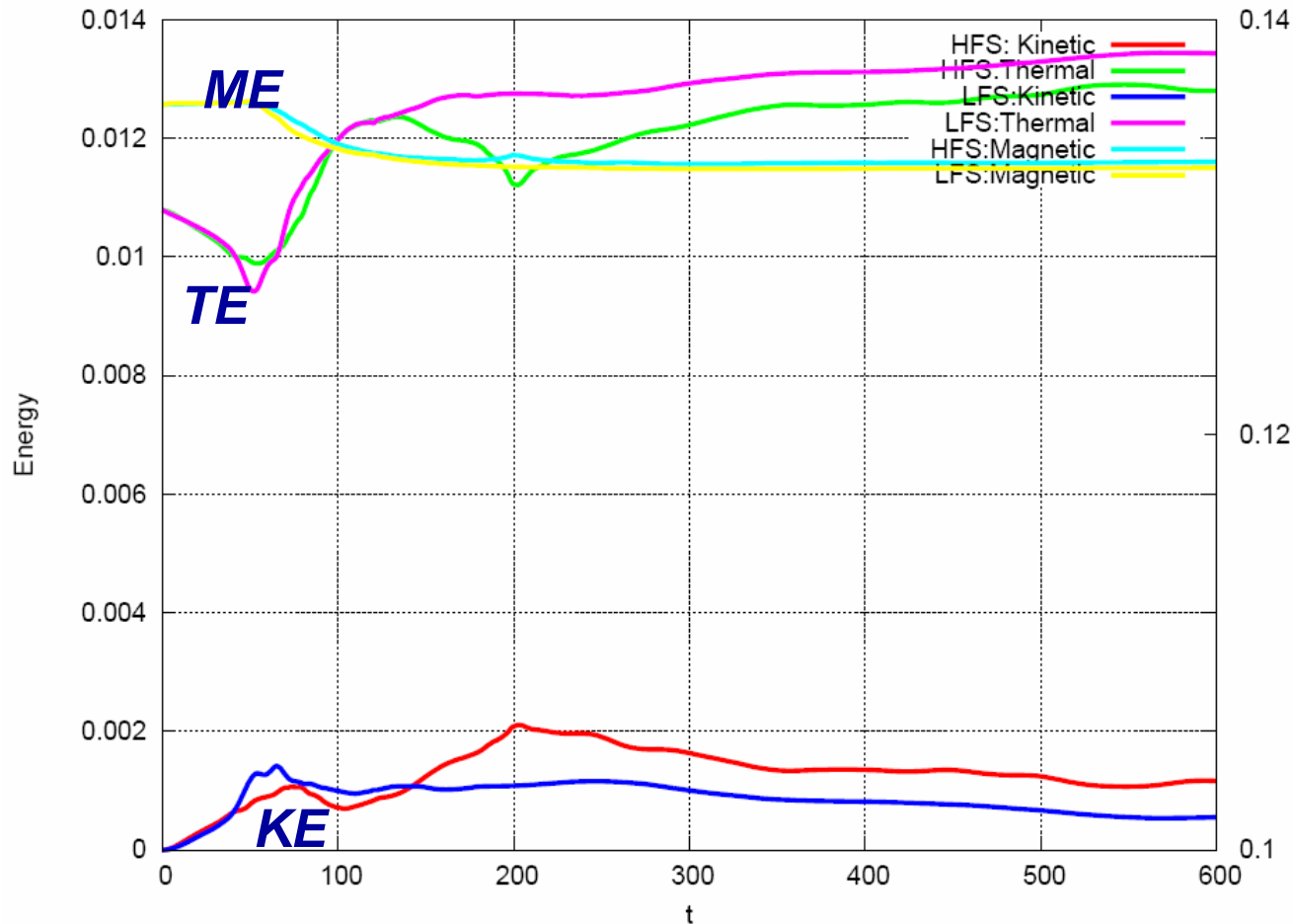


LFS Pellet Injection $t=250$



Radially outward shift in both cases indicates higher fueling efficiency for HFS

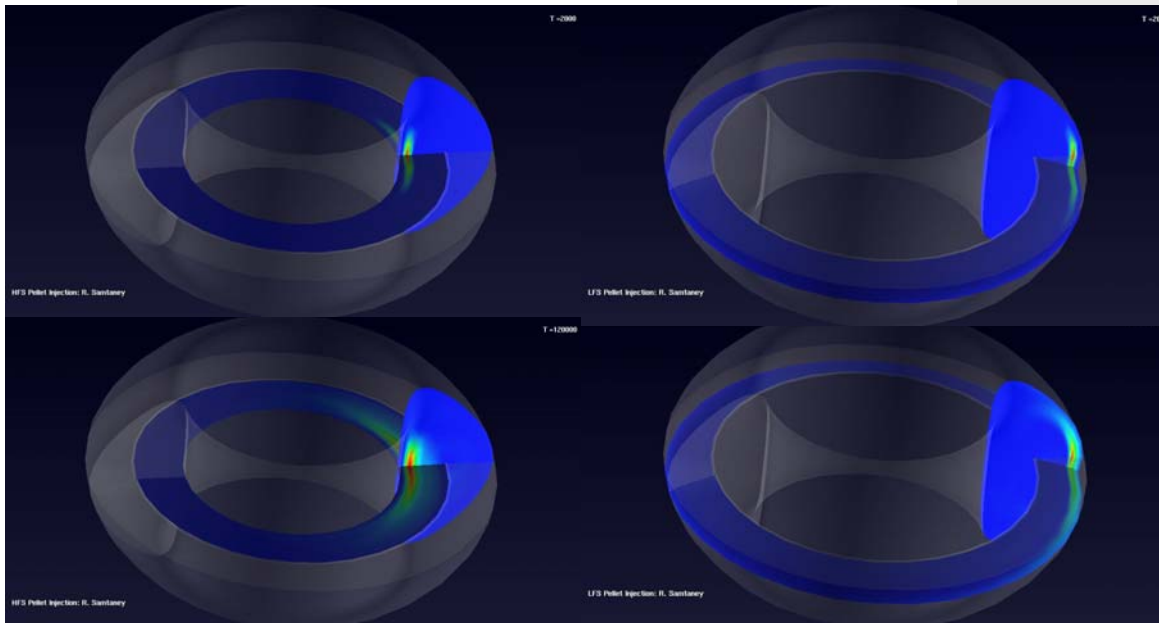
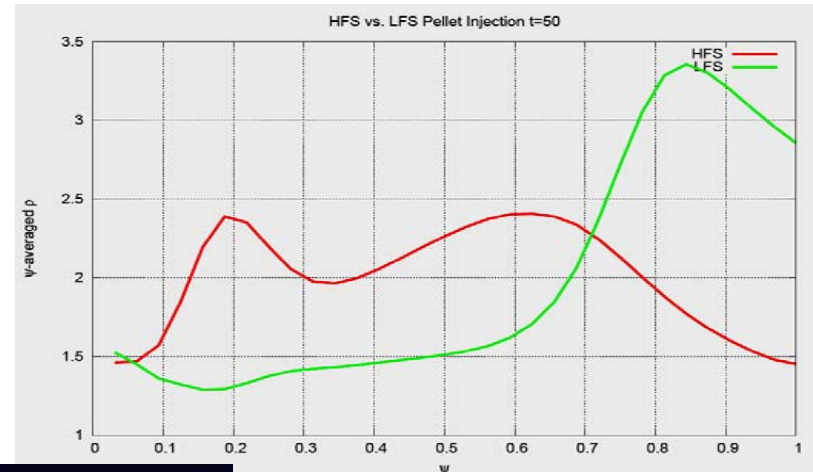
Results – Energy budget



For $0 < t < 120$: Rapid redistribution of thermal energy by electrons
Kinetic energy increases at expense of thermal energy
Thermal energy increases due to reconnection

Results (“DIII-D”): HFS vs. LFS

- $B_T = 1T$
- $T_{e1} = 4-6\text{Kev}$
- $n_0 = 1.5 \times 10^{19}/\text{m}^3$
- $\beta = 0.036$
- $R_0 = 1.7\text{m}$ $a = 0.55\text{m}$
- Pellet: radius $r_p = 1\text{mm}$, velocity $v_p = 1000\text{m/s}$



**Larger core fueling
for HFS than LFS**

Supersonic Gas Injection

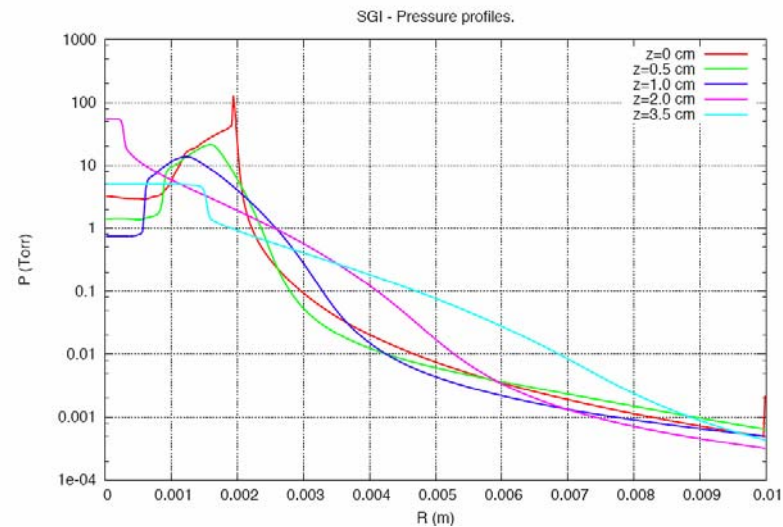
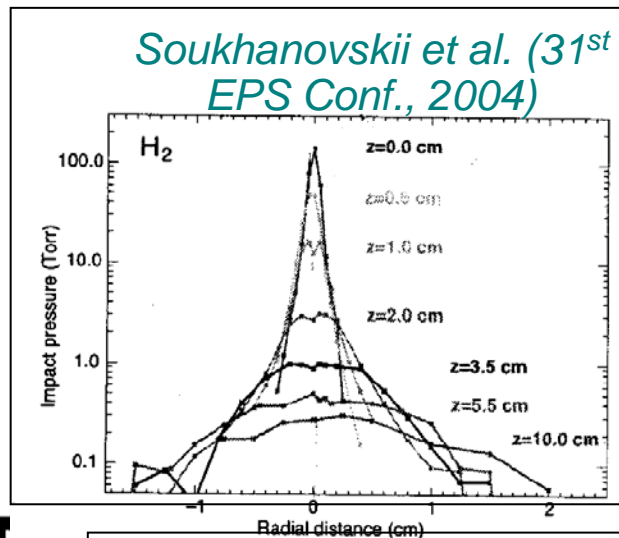
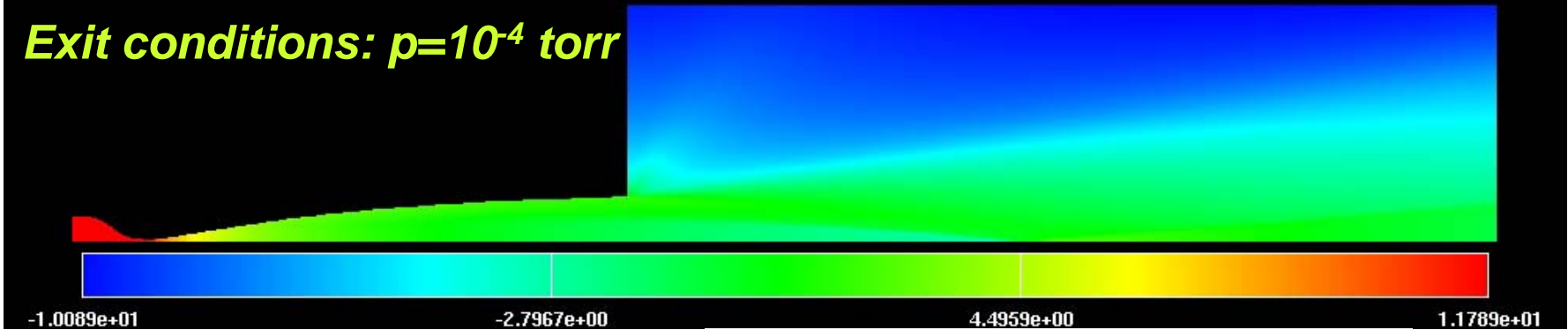
- New method for refueling
- SGI Experiments on NSTX
 - *Scaled down nozzle designed for hypersonic flows ($M=8$)*
- Computational modeling with “Nozzle” code
 - *Equations in conservative form*
 - *Finite volume approach*
 - *Explicit time stepping approach*
 - *Second order accurate in space and time*
 - *Efficient parallel and scalable implementation*
 - *Includes ionization model (Saha eqn. for equilibrium ionization)*
 - *Handle arbitrary moving or static geometries in 2D and axisymmetry*
 - *Also extensible to 3D static boundaries*
 - *Level-set approach to handle arbitrary geometry*

Nozzle code: Results

- Nozzle (Specified inflow. Outflow BC is characteristic)

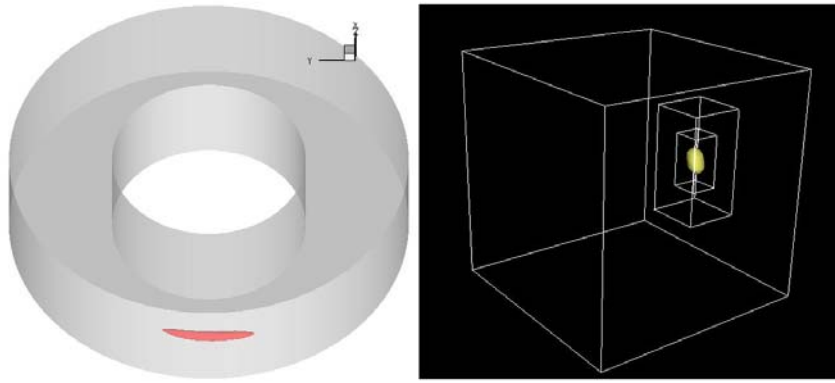
Reservoir conditions: $p=1000$ torr, $T=293$ K

Exit conditions: $p=10^{-4}$ torr

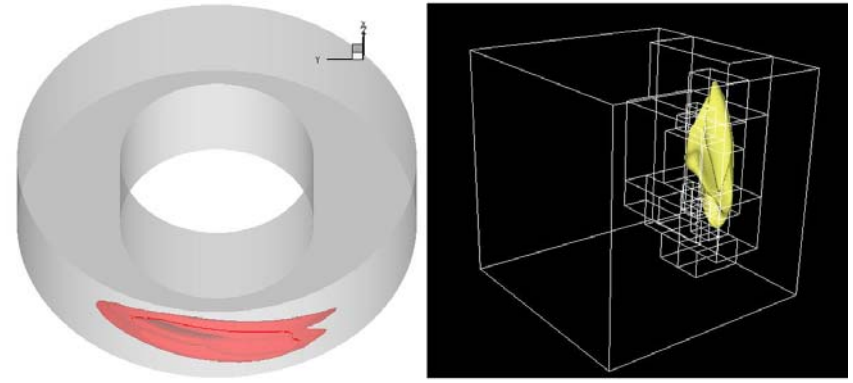


Boundary layer effects may be important in experiments

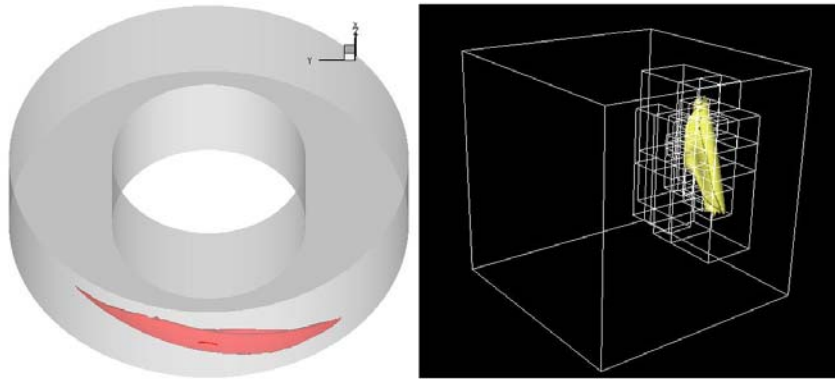
Pellet Injection: LFS Launch



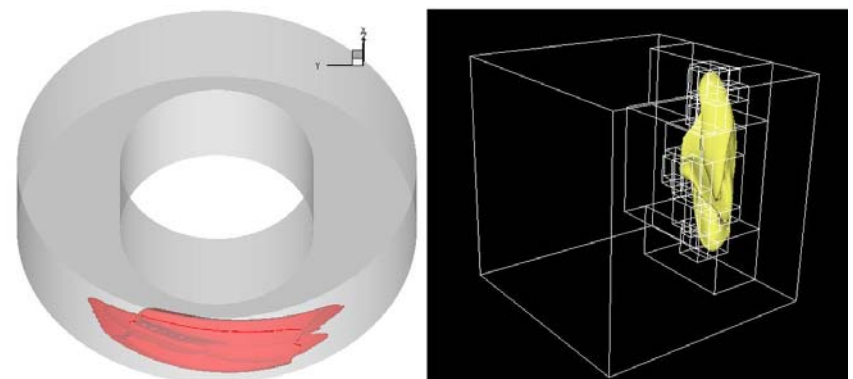
t=2



t=40

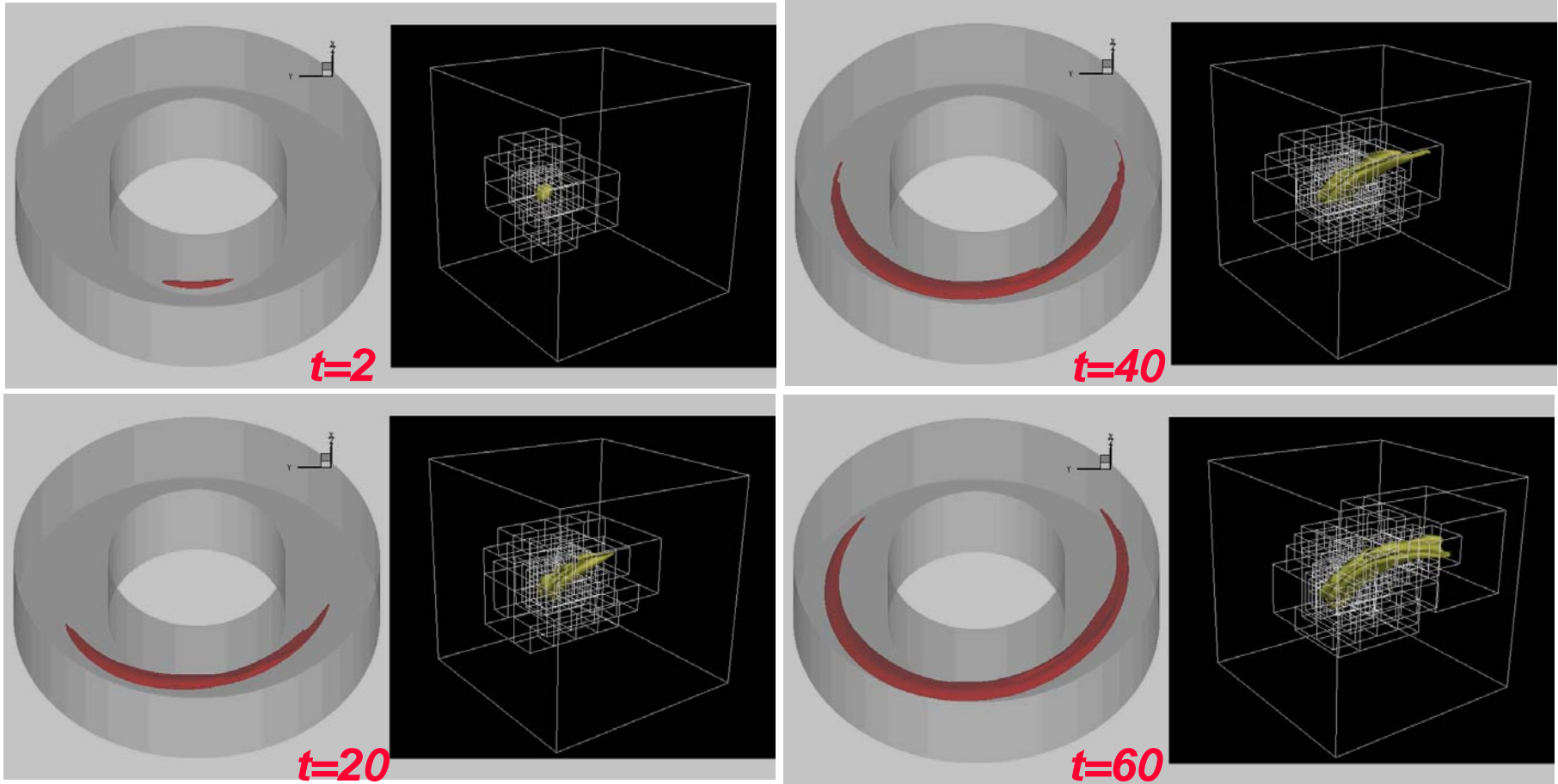


t=20



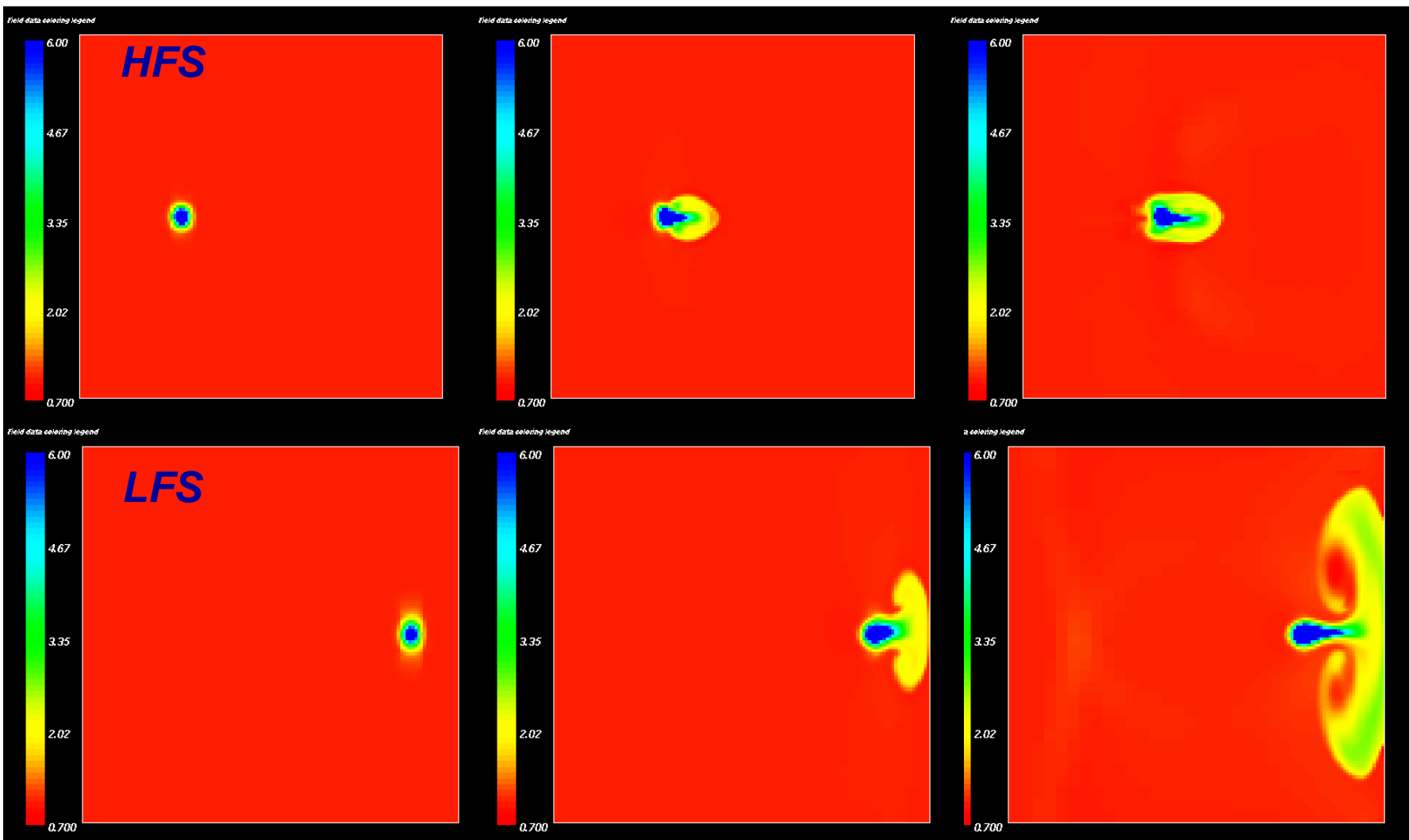
t=60

Pellet Injection: HFS Launch



Note: Left (right) side of frame shows physical (computational) space.

Pellet Injection: HFS vs. LFS



Anomalous transport across flux surfaces

Conclusion and Future Directions

- Pellet injection simulations performed with an AMR code with flux tube geometry
 - *Numerical method is upwind, conservative and preserves the solenoidal property of the magnetic field*
 - *Physics of non-local electron heat flux included in the simulations*
 - *HFS vs. LFS pellet launches*
 - *HFS core fueling is more effective*
 - *Outward radial shift due to $r B$ and $E \times B$*
 - *Simulation results are consistent with previous studies, and qualitatively consistent with experimental observations*
- Compared supersonic gas injection into NSTX
 - *Boundary layer profiles may be important and will be included in the Nozzle code*
- Future work
 - *Higher resolution AMR runs for DIII-D*
 - *Validation against DIII-D experiments*
 - *Predictions for ITER*
 - *Vertical launches (HFS is hard to achieve for ITER)*

Continue validation of gas injection

Effect of ionization and EM forces on gas injection