**On elliptic solves for 3D XMHD** 

#### L. Chacón

Los Alamos National Laboratory P.O. Box 1663, Los Alamos, NM 87545

> CEMM MEETING OCT. 29TH, 2006 PHILADELPHIA, PA USA

> > Reports of interest

- 1. Simulation-Based Engineering Science (SBES): Revolutionizing Engineering Science through Simulation, Feb. 2006, NSF Report
- 2. Fusion Simulation Project: Integrated Simulation & Optimization of Fusion Systems, Dec. 01, FESAC ISOFS Subcommittee Report



# Outline

- Motivation
- Parabolization: key for SCALABILITY
- Application: Resistive 3D MHD
- Application: Hall MHD
- Implicit + AMR: proof of principle



## Challenges in fusion simulation: "The tyranny of scales"



(a) Time scales in fusion plasmas (FSP report)

(b) Length scales in a typical fusion plasma (Tang, *Phys. Plasmas*, 9 (5), 2002)

"The tyranny of scales will not be simply defeated by building bigger and faster computers" (SBES report, p. 30)



#### **Requirements and impact of algorithms?**





(c) Computational requirements for fusion plasma integrated simulation (FSP report) (d) Impact of algorithms in gas combustion effective FLOPS (SBES report)

"Faster and more cost-effective hardware is a strong driver for simulation-based engineering. However, algorithmic improvements have been far more important." (SBES report, p. 50)



# Algorithmic challenges in XMHD (I)

- XMHD is a strongly hyperbolic PDE system.
- Numerically, XMHD is a nonlinear algebraic system of very stiff equations:
  - Elliptic stiffness (diffusion): Jacobian condition number  $\sim \frac{\Delta t D}{\Delta x^2}$
  - Hyperbolic stiffness (linear and dispersive waves): Jacobian condition number  $\sim \Delta t \, \omega_{fast} \sim \frac{\Delta t}{\Delta t_{CFL}} \gg 1$
- An implicit integration of XMHD *may be* advantageous to step over wave phenomena and get to the dynamical time scale of interest.

Implicit methods require inversion of very large, sparse matrices!



## Algorithmic challenges in XMHD (II)

- Brute-force algorithms will not be able to cover the span between disparate time/length scales, regardless of computer power (gas combustion example).
- Key algorithmic feature: **SCALABILITY**!
  - Minimize number of degrees of freedom (grid points) without sacrificing spatial resolution: spatial adaptivity
  - Be able to follow lowest frequency time scales (application dependent): implicit time stepping

It is our contention that fully implicit, spatially adaptive methods are essential for scalability, and thus an integral part of a predictive plasma simulation tool!

Scalable algorithm: CPU  $\sim O(N/np)$ , N is # dof, np is # procs



#### **Alternatives for inversion algorithms: NOT SCALABLE**

• Explicit (trivial option, here for comparison):

$$CPU \sim \frac{T_{max}}{\Delta t_{CFL}} \times \frac{N}{np} \sim \mathcal{O}(N^{1+\alpha/d}/np) ;$$

d is # dimensions,  $\alpha=1,2$  for linear, dispersive waves

- Implicit (requires matrix inversion). Naive options are NOT scalable:
  - Direct methods: good parallelization, but do not scale with problem size:

$$CPU \sim \mathcal{O}\left(rac{N^{(3-2/d)}}{np^{\beta}}
ight) \ , \ \beta \gtrsim 1$$

 Iterative methods (unpreconditioned Krylov, stationary, etc.): good paralellization, but VERY slow convergence:

$$CPU \sim \mathcal{O}\left(\frac{N^{\alpha}}{np^{\beta}}\right) \ , \ \alpha > 1 \ ; \ \beta \gtrsim 1$$

Scalingwise, direct solver is WORSE than explicit for  $d>1+\frac{\alpha}{2}\approx 2$ 



#### **Alternatives for inversion algorithms: SCALABLE**

- Scalable matrix inversion methods require MULTILEVEL approaches (divide and conquer in wavenumbers):
  - Direct-solve substructuring (X. Z. Tang).
  - FETI-DP (Glasser's talk).
  - Multilevel iterative (e.g., classical MG, algebraic MG).

$$CPU \sim \mathcal{O}\left(\frac{N \log(N)}{np^{\beta}}\right) \ , \ \beta \gtrsim 1$$

- Both approaches are being pursued in T-15 at LANL!
- This talk focuses on the second approach.
- A fundamental component of iterative ML methods (both classical and algebraic) is the existence of a SMOOTHER (convergent stationary iterative method).

Q: How to ensure the existence of a SMOOTHER for XMHD? A: Parabolization!



#### Parabolization and Schur complement: an example

• PARABOLIZATION EXAMPLE:

$$\partial_t u = \partial_x v \ , \ \partial_t v = \partial_x u.$$

$$u^{n+1} = u^n + \Delta t \partial_x v^{n+1},$$
  
$$v^{n+1} = v^n + \Delta t \partial_x u^{n+1}.$$

$$(I - \Delta t^2 \partial_{xx})u^{n+1} = u^n + \Delta t \partial_x v^n$$

• PARABOLIZATION via SCHUR COMPLEMENT:

$$\begin{bmatrix} D_1 & U \\ L & D_2 \end{bmatrix} = \begin{bmatrix} I & UD_2^{-1} \\ 0 & I \end{bmatrix} \begin{bmatrix} D_1 - UD_2^{-1}L & 0 \\ 0 & D_2 \end{bmatrix} \begin{bmatrix} I & 0 \\ D_2^{-1}L & I \end{bmatrix}.$$

Stiff off-diagonal blocks L, U now sit in diagonal via Schur complement  $D_1 - UD_2^{-1}L$ . The system has been "PARABOLIZED."

$$D_1 - UD_2^{-1}L = (I - \Delta t^2 \partial_{xx})$$



### How to build a successful fully implicit algorithm for XMHD

- Even if a smoother exists, MG is remarkably temperamental
- Combination of Krylov methods and MG is optimal:
  - MG provides scalability (as a preconditioner)
  - Krylov provides robustness
- We seek to develop a successful algorithm for XMHD based on Newton-Krylov-MG.
- We will start with resistive MHD, and then move to XMHD.
- Finally we will discuss the combination of implicit time stepping with dynamic grid adaptation.



### **Jacobian-Free Newton-Krylov Methods**

- Objective: solve nonlinear system  $\vec{G}(\vec{x}^{n+1}) = \vec{0}$  efficiently.
- Converge nonlinear couplings using Newton-Raphson method:
- Jacobian-free implementation:

$$\left(\frac{\partial \vec{G}}{\partial \vec{x}}\right)_k \vec{y} = J_k \vec{y} = \lim_{\epsilon \to 0} \frac{\vec{G}(\vec{x}_k + \epsilon \vec{y}) - \vec{G}(\vec{x}_k)}{\epsilon}$$

 $\partial \vec{G}$ 

 $\delta ec{x}_k = -ec{G}(ec{x}_k)$ 

- Krylov method of choice: GMRES (nonsymmetric systems).
- Right preconditioning: solve equivalent Jacobian system for  $\delta y = P_k \delta \vec{x}$ :

$$J_k P_k^{-1} \underbrace{\underline{P_k \delta \vec{x}}}_{\delta \vec{y}} = -\vec{G}_k$$

APPROXIMATIONS IN PRECONDITIONER DO NOT AFFECT ACCURACY OF CONVERGED SOLUTION; THEY ONLY AFFECT EFFICIENCY!



# Implicit resistive MHD solver



## **Resistive MHD model equations**

$$\begin{split} \frac{\partial \rho}{\partial t} &+ \nabla \cdot (\rho \vec{v}) = 0, \\ \frac{\partial \vec{B}}{\partial t} &+ \nabla \times \vec{E} = 0, \\ \frac{\partial (\rho \vec{v})}{\partial t} + \nabla \cdot \left[ \rho \vec{v} \vec{v} - \vec{B} \vec{B} &- \rho \nu \nabla \vec{v} + \overleftarrow{I} \left( p + \frac{B^2}{2} \right) \right] = 0, \\ \frac{\partial T}{\partial t} + \vec{v} \cdot \nabla T &+ (\gamma - 1) T \nabla \cdot \vec{v} = 0, \end{split}$$

- Plasma is assumed polytropic  $p \propto n^{\gamma}.$
- Resistive Ohm's law:

$$\vec{E} = -\vec{v} \times \vec{B} + \eta \nabla \times \vec{B}$$



#### **Resistive MHD Jacobian block structure**

• The linearized resistive MHD model has the following couplings:

$$\begin{split} \delta \rho &= L_{\rho}(\delta \rho, \delta \vec{v}) \\ \delta T &= L_{T}(\delta T, \delta \vec{v}) \\ \delta \vec{B} &= L_{B}(\delta \vec{B}, \delta \vec{v}) \\ \delta \vec{v} &= L_{v}(\delta \vec{v}, \delta \vec{B}, \delta \rho, \delta T) \end{split}$$

• Therefore, the Jacobian of the resistive MHD model has the following coupling structure:

$$J\delta\vec{x} = \begin{bmatrix} D_{\rho} & 0 & 0 & U_{v\rho} \\ 0 & D_{T} & 0 & U_{vT} \\ 0 & 0 & D_{B} & U_{vB} \\ L_{\rho v} & L_{Tv} & L_{Bv} & D_{v} \end{bmatrix} \begin{pmatrix} \delta\rho \\ \delta T \\ \delta \vec{B} \\ \delta \vec{v} \end{pmatrix}$$

• Diagonal blocks contain advection-diffusion contributions, and are "easy" to invert using MG techniques. Off diagonal blocks L and U contain all hyperbolic couplings.



#### **PARABOLIZATION: Schur complement formulation**

• We consider the block structure:

$$J\delta\vec{x} = \begin{bmatrix} M & U \\ L & D_v \end{bmatrix} \begin{pmatrix} \delta\vec{y} \\ \delta\vec{v} \end{pmatrix}$$
$$\delta\vec{y} = \begin{pmatrix} \delta\rho \\ \delta T \\ \delta\vec{B} \end{pmatrix} \quad ; \quad M = \begin{pmatrix} D_\rho & 0 & 0 \\ 0 & D_T & 0 \\ 0 & 0 & D_B \end{pmatrix}$$

• *M* is "easy" to invert (advection-diffusion, MG-friendly).

Schur complement analysis of 2x2 block J yields:

$$\begin{bmatrix} M & U \\ L & D_v \end{bmatrix}^{-1} = \begin{bmatrix} I & 0 \\ -LM^{-1} & I \end{bmatrix} \begin{bmatrix} M^{-1} & 0 \\ 0 & P_{Schur}^{-1} \end{bmatrix} \begin{bmatrix} I & -M^{-1}U \\ 0 & I \end{bmatrix},$$
$$P_{Schur} = D_v - LM^{-1}U.$$

- EXACT Jacobian inverse only requires  $M^{-1}$  and  $P_{Schur}^{-1}$ .
- Schur complement formulation is fundamentally unchanged in Hall MHD!



### **Physics-based preconditioner (I)**

• The Schur complement analysis translates into the following 3-step EXACT inversion algorithm:

Predictor : 
$$\delta \vec{y}^* = -M^{-1}G_y$$
  
Velocity update :  $\delta \vec{v} = P_{Schur}^{-1}[-G_v - L\delta \vec{y}^*], P_{Schur} = D_v - LM^{-1}U$   
Corrector :  $\delta \vec{y} = \delta \vec{y}^* - M^{-1}U\delta \vec{v}$ 

• MG treatment of  $P_{Schur}$  is impractical due to  $M^{-1}$ .

Need suitable simplifications (SEMI-IMPLICIT)!

- We consider the small-flow-limit case:  $M^{-1} \approx \Delta t$
- This approximation is equivalent to splitting flow in original equations.



#### **Physics-based preconditioner (II)**

• Small flow approximation:  $M^{-1} \approx \Delta t$  in steps 2 & 3 of Schur algorithm:

$$\begin{split} \delta \vec{y}^* &= -M^{-1} G_y \\ \delta \vec{v} &\approx P_{SI}^{-1} \left[ -G_v - L \delta \vec{y}^* \right] ; \ P_{SI} = D_v - \Delta t L U \\ \delta \vec{y} &\approx \delta \vec{y}^* - \Delta t U \delta \vec{v} \end{split}$$

where:

$$P_{SI} = \rho^{n} \left[ \overleftarrow{I} / \Delta t + \theta (\vec{v}_{0} \cdot \nabla \overleftarrow{I} + \overleftarrow{I} \cdot \nabla \vec{v}_{0} - \nu^{n} \nabla^{2} \overleftarrow{I}) \right] + \Delta t \theta^{2} W(\vec{B}_{0}, p_{0})$$
$$W(\vec{B}_{0}, p_{0}) = \vec{B}_{0} \times \nabla \times \nabla \times \left[ \overleftarrow{I} \times \vec{B}_{0} \right] - \vec{j}_{0} \times \nabla \times \left[ \overleftarrow{I} \times \vec{B}_{0} \right] - \nabla \left[ \overleftarrow{I} \cdot \nabla p_{0} + \gamma p_{0} \nabla \cdot \overleftarrow{I} \right]$$

- *P*<sub>SI</sub> is block diagonally dominant by construction!
- We employ multigrid methods (MG) to approximately invert  $P_{SI}$  and M: 1 V(4,4) cycle



# **Efficiency:** $\Delta t$ scaling (2D tearing mode)

#### $32 \times 32$

$\Delta t$	Newton/ $\Delta t$	$GMRES/\Delta t$	CPU (s)	$CPU_{exp}/CPU$	$\Delta t/\Delta t_{CFL}$
2	5.9	20.9	115	3.1	354
3	5.9	25.6	139	3.8	531
4	6.0	30.5	163	4.3	708
6	6.0	34.7	184	5.8	1062

#### $128 \times 128$

$\Delta t$	Newton/ $\Delta t$	$GMRES/\Delta t$	CPU (s)	$CPU_{exp}/CPU$	$\Delta t/\Delta t_{CFL}$
0.5	4.9	8.4	764	8.0	380
0.75	5.7	10.2	908	10.0	570
1.0	5.0	11.5	1000	12.7	760
1.5	5.6	14.7	1246	14.6	1140



# **Efficiency: grid scaling**

#### $\Delta t \approx 1100 \Delta t_{CFL}$ , 10 time steps

Grid	$\Delta t$	Newton/ $\Delta t$	$GMRES/\Delta t$	CPU	$\widehat{CPU}$
32x32	6	6.0	34.7	184	5.3
64x64	3	5.8	22.9	468	20.4
128x128	1.5	5.6	14.8	1246	84.2

Why does GMRES/ $\Delta t$  decrease with resolution?



## **Effect of spatial truncation error**





#### Sample 3D results: Screw pinch in 3D





### Sample 3D results: 3D KHI

Knoll and Brackbill, Phys. Plasmas 9 (9) 2002





# Implicit extended MHD solver



#### **Extended MHD model equations**

$$\begin{split} \frac{\partial \rho}{\partial t} &+ \nabla \cdot (\rho \vec{v}) = 0, \\ \frac{\partial \vec{B}}{\partial t} &+ \nabla \times \vec{E} = 0, \\ \frac{\partial (\rho \vec{v})}{\partial t} + \nabla \cdot \left[ \rho \vec{v} \vec{v} - \vec{B} \vec{B} &- \rho \nu \nabla \vec{v} + \overleftarrow{I} \left( p + \frac{B^2}{2} \right) \right] = 0, \\ \frac{\partial T_e}{\partial t} + \vec{v} \cdot \nabla T_e &+ (\gamma - 1) T_e \nabla \cdot \vec{v} = 0, \end{split}$$

- Plasma is assumed polytropic  $p \propto n^{\gamma}$ .
- We assume cold ion limit:  $T_i \ll T_e \Rightarrow p \approx p_e$ .
- Generalized Ohm's law:

$$ec{E} = -ec{v} imes ec{B} + \eta 
abla imes ec{B} - rac{d_i}{
ho} (ec{j} imes ec{B} - 
abla p_e)$$



#### **Extended MHD Jacobian block structure**

• The linearized extended MHD model has the following couplings:

$$\begin{split} \delta \rho &= L_{\rho}(\delta \rho, \delta \vec{v}) \\ \delta T &= L_{T}(\delta T, \delta \vec{v}) \\ \delta \vec{B} &= L_{B}(\delta \vec{B}, \delta \vec{v}, \delta \rho, \delta T) \\ \delta \vec{v} &= L_{v}(\delta \vec{v}, \delta \vec{B}, \delta \rho, \delta T) \end{split}$$

• Jacobian coupling structure:

$$J\delta\vec{x} = \begin{bmatrix} D_{\rho} & 0 & 0 & U_{v\rho} \\ 0 & D_{T} & 0 & U_{vT} \\ L_{\rho B} & L_{TB} & D_{B} & U_{vB} \\ L_{\rho v} & L_{Tv} & L_{Bv} & D_{v} \end{bmatrix} \begin{pmatrix} \delta\rho \\ \delta T \\ \delta \vec{B} \\ \delta \vec{v} \end{pmatrix}$$

• We have added off-diagonal couplings.



#### **Extended MHD Jacobian block structure (cont.)**

• The coupling structure can be substantially simplified if we note  $(p \approx p_e)$ :

$$\frac{1}{\rho}(\vec{j} \times \vec{B} - \nabla p_e) \approx \frac{D\vec{v}}{Dt}$$

and therefore:

$$\vec{E} \approx -\vec{v} \times \vec{B} + \frac{\eta(T)}{\mu_0} \nabla \times \vec{B} - d_i \frac{D\vec{v}}{Dt}$$

• This transforms jacobian coupling structure to:

$$J\delta \vec{x} \approx \begin{bmatrix} D_{\rho} & 0 & 0 & U_{v\rho} \\ 0 & D_{T} & 0 & U_{vT} \\ 0 & 0 & D_{B} & U_{vB}^{R} + \boldsymbol{U}_{vB}^{H} \\ L_{\rho v} & L_{Tv} & L_{Bv} & D_{v} \end{bmatrix} \begin{pmatrix} \delta \rho \\ \delta T \\ \delta \vec{B} \\ \delta \vec{v} \end{pmatrix}$$

We can therefore reuse ALL resistive MHD PC framework!



## **Extended MHD preconditioner**

- Use same Schur complement approach.
- *M* block contains ion scales only! Approximation  $M^{-1} \approx \Delta t$  is very good in extended MHD (ion scales do NOT contribute to numerical stiffness).
- Additional block  $U_{vB}^{H}$  results, after the Schur complement treatment, in systems of the form:

$$\partial_t \delta \vec{v} - d_i \vec{B_0} \times (\nabla \times \nabla \times \delta \vec{v}) = rhs$$

- This system supports dispersive waves  $\omega \sim k^2!$
- We have shown analytically that damped JB is a smoother for these systems!

We can use classical MG!



#### **Preliminary efficiency results (2D tearing mode)**

 $d_i = 0.05$ 

1 time step,  $\Delta t = 1.0$ , V(3,3) cycles, mg\_tol=1e-2

Grid	Newton/ $\Delta t$	$GMRES/\Delta t$	<i>CPU</i> (s)	$CPU_{exp}/CPU$	$\Delta t/\Delta t_{exp}$
32x32	5	22	25	0.44	110
64x64	5	12	66	1.4	238
128x128	5	8	164	6.2	640
256x256	4	7	674	30	3012

Again, GMRES/ $\Delta t$  decreases with resolution!



## **Effect of spatial truncation error**



Residual history vs. GMRES it# with fixed time step Dt=1



## **GEM Challenge**

#### J. Birn et al., J. Geophys. Res., 106 (A3), p.3715-19 (2001)





## Parallel performance with PETSc Toolkit (unpreconditioned)





# **Implicit-AMR proof of principle**

B. Philip, M. Pernice, and L. Chacón, Lecture Notes in Computational Science and Engineering, accepted (2006).



#### **Current-Vorticity Formulation of Reduced Resistive MHD**<sup>1</sup>

$$(\partial_t + \mathbf{u} \cdot \nabla - \eta \Delta) J + \Delta E_0 = \mathbf{B} \cdot \nabla \omega + \{\Phi, \Psi\} (\partial_t + \mathbf{u} \cdot \nabla - \nu \Delta) \omega + S_\omega = \mathbf{B} \cdot \nabla J \Delta \Phi = \omega \Delta \Psi = J$$

$$\mathbf{u} = \vec{z} \times \nabla \Phi , \ \mathbf{B} = \vec{z} \times \nabla \Psi$$
$$\{\Phi, \Psi\} = 2[\Phi_{xy}(\Psi_{xx} - \Psi_{yy}) - \Psi_{xy}(\Phi_{xx} - \Phi_{yy})]$$

Preconditioner is developed as an extension of Chacón, Knoll and Finn, JCP, **178** (2002).

<sup>1</sup>Strauss and Lonacope. JCP, **147**, 1998



### **Structured Adaptive Mesh Refinement**

• *Structured* adaptive mesh refinement (SAMR) represents a locally refined mesh as a union of logically rectangular meshes.



- The mesh is organized as a hierarchy of nested refinement levels.
- Each refinement level defines a region of uniform resolution.
- Each refinement level is the union of logically rectangular patches.



#### **Hierarchical Structure of SAMR Grids**





## **Tearing Mode Results**









t = 50





t = 200



#### **Tearing Mode Performance**

	NNI						NLI			
Levels	1	2	3	4	5	1	2	3	4	5
$32 \times 32$	1.5	2.0	2.0	2.1	2.5	3.4	7.9	12.0	19.3	33.7
$64 \times 64$	1.8	2.0	2.0	2.4	_	6.5	11.7	19.1	33.2	_
$128 \times 128$	1.8	2.0	2.4	_	_	12.5	20.1	27.2	_	_
$\boxed{256 \times 256}$	1.9	2.0	_	_	_	19.9	27.5	_	_	—
$\boxed{512 \times 512}$	1.9	_	_	_	_	26.3	—	—	—	_

 $\eta_k = 0.1$ ,  $\epsilon_{rel} = \epsilon_{abs} = 10^{-7}$ , 2 SI iterations, V(3,3) cycles



#### Island Coalescence Results at t=8





# **Tilt Instability Results at t=7**



