Discussion of Kinetic-MHD Formulation

J.D. Callen, in consultation with C.C. Hegna, C.R. Sovinec University of Wisconsin, Madison, WI 53706-1609

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Theses:

1) Key next step for extended MHD computational models is to add multicollisionality viscous forces that yield bootstrap current and poloidal flow.

2) A new approximate form for $\vec{\nabla} \cdot \overleftarrow{\pi}_{\parallel}$ that accomplishes this has been proposed — in UW-CPTC 09-6, available via http://www.cptc.wisc.edu.

3) Longer term we need a more exact kinetic-MHD hybrid model that obtains bootstrap current in neoclassical || Ohm's law & poloidal ion flow.

Outline:

Parallel viscous stress closure needed for bootstrap current, poloidal flow

New multi-collisionality parallel stress closure

What's needed in long term

Electron Parallel Force Balance Yields || Ohm's Law

- For times $t > 1/\nu_e \sim 10 \,\mu$ s, equilibrium electron || force balance becomes $0 = -n_e e \langle \vec{B} \cdot \vec{E}^A \rangle - \langle \vec{B} \cdot \vec{\nabla} \cdot \overleftarrow{\pi}_e \rangle + \langle \vec{B} \cdot \vec{R}_e \rangle + \langle \vec{B} \cdot \vec{S}_{em} \rangle - m_e n_{e0} \langle \vec{B} \cdot \overline{\vec{V}_e} \cdot \vec{\nabla} \overline{\vec{V}_e} \rangle - n_{e0} e \langle \vec{B} \cdot \overline{\vec{V}_e} \times \overline{\vec{B}_\perp} \rangle.$
- Using the collisional friction relation $\vec{B}_0 \cdot \vec{R}_e = -\vec{B}_0 \cdot \vec{R}_i \simeq n_{e0} e \vec{B}_0 \cdot \vec{J} / \sigma_{\parallel}$ and neoclassical closure $\langle \vec{B}_0 \cdot \vec{\nabla} \cdot \overleftarrow{\pi}_{e\parallel} \rangle \simeq m_e n_{e0} \langle B_0^2 \rangle (\mu_{e00} U_{e\theta} + \mu_{e01} Q_{e\theta})$, this equation yields an extended neoclassical-based parallel Ohm's law:¹

$$\underbrace{\langle \vec{B}_0 \cdot \bar{\vec{E}}^A \rangle}_{\bar{E}_{\parallel}^A \text{ field }} = \eta_{\parallel}^{\text{nc}} \underbrace{\langle \vec{B}_0 \cdot \vec{J} \rangle}_{\text{ current }} - \frac{1}{\sigma_{\parallel}} [\underbrace{\langle \vec{B}_0 \cdot \vec{J}_{\text{bs}} \rangle}_{\text{ bootstrap }} + \underbrace{\langle \vec{B}_0 \cdot \vec{J}_{\text{CD}} \rangle}_{\text{ current drive }} + \underbrace{\langle \vec{B}_0 \cdot \vec{J}_{\text{dyn}} \rangle}_{\text{ dynamo}}], \qquad \eta_{\parallel}^{\text{nc}} \simeq \frac{1}{\sigma_{\parallel}} \left(1 + \frac{\sigma_{\parallel}}{\sigma_{\perp}} \frac{\mu_{e00}}{\nu_e} \right)$$

• \parallel currents are driven by $dP_0/d\psi_p, \parallel e$ momentum sources and fluctuations:

$$\begin{split} \langle \vec{B}_{0} \cdot \vec{J}_{\rm bs} \rangle &\simeq -\frac{\sigma_{\parallel}}{\sigma_{\perp}} \frac{\mu_{e00}}{\nu_{e}} \left(I \frac{dP_{0}}{d\psi_{p}} - n_{e0} e U_{i\theta} \langle B_{0}^{2} \rangle \right), & \text{bootstrap current,} \\ \langle \vec{B}_{0} \cdot \vec{J}_{\rm CD} \rangle &\equiv -\frac{\sigma_{\parallel}}{n_{e0}e} \langle \vec{B}_{0} \cdot \left(\bar{\vec{S}}_{em} - m_{e} \bar{\vec{V}}_{e} \bar{\vec{S}}_{en} \right) \rangle, & \text{non-inductive current drive,} \\ \langle \vec{B}_{0} \cdot \vec{J}_{\rm dyn} \rangle &= \underbrace{\frac{\sigma_{\parallel}}{n_{e0}e} \langle \vec{B}_{0} \cdot \left(m_{e} n_{e0} \overline{\vec{V}}_{e} \cdot \vec{\nabla} \overline{\vec{V}}_{e} + \overline{\nabla} \cdot \overline{\vec{\pi}}_{e\wedge} \right) \rangle}_{\parallel \text{Reynolds stress}} + \underbrace{\frac{\sigma_{\parallel} \langle \vec{B}_{0} \cdot \overline{\vec{V}}_{e} \times \overline{\vec{B}}_{\perp} \rangle}_{\parallel \text{Maxwell stress}}, & \text{dynamo.} \end{split}$$

¹For illustrative purposes the equations here are simplified versions where the effects of the poloidal electron heat flow $Q_{e\theta}$ have been neglected.

Poloidal Flow Is Obtained From Plasma || Force Balance

- Summing the parallel force balances over species yields (for $\bar{S}_n = 0$) $m_i n_{i0} \frac{\partial \langle B_0 V_{i\parallel} \rangle}{\partial t} \simeq -\langle \vec{B}_0 \cdot \vec{\nabla} \cdot \dot{\vec{\pi}}_i \rangle - m_i n_0 \langle \vec{B}_0 \cdot \overline{\vec{V}_i} \cdot \vec{\nabla} \overline{\vec{V}_i} \rangle + \langle \vec{B}_0 \cdot \overline{\vec{J}_{\wedge}} \times \overline{\vec{B}_{\perp}} \rangle + \langle \vec{B}_0 \cdot \sum_s \bar{\vec{S}}_{sm} \rangle.$
- The poloidal flow is determined mainly by the parallel ion viscous force: $(\vec{R} \vec{\nabla} \vec{r}) > 2 (m m \left[u - U + u \right]^{-2} O + \left[(R^2) - u - u - U - U \right]^{-2} O$

$$egin{aligned} &\langle ec{B} \cdot ec{
abla} \cdot ec{\pi}_{i\parallel}
angle \simeq m_i n_{i0} \left[\mu_{i00} U_{i heta} + \mu_{i01} rac{-2}{5 n_i T_i} Q_{i heta} + \cdots
ight] \langle B^2
angle, \qquad \mu_{i00}, \mu_{i01} \sim \sqrt{\epsilon} \,
u_i. \end{aligned}$$

- For $t > 1/\nu_i \sim 1$ ms, poloidal flow from NCLASS, or $\langle \vec{B} \cdot \vec{\nabla} \cdot \overleftarrow{\pi}_{i\parallel} \rangle \simeq 0$ is: $U^0_{i\theta}(\psi_p) \equiv \frac{\vec{V} \cdot \vec{\nabla} \theta}{\vec{B} \cdot \vec{\nabla} \theta} \simeq -\frac{\mu_{i01}}{\mu_{i00}} \frac{-2}{5n_i T_i} Q_{i\theta} \simeq \frac{c_p I}{q_i \langle B^2 \rangle} \frac{dT_{i0}}{d\psi_p} \implies V_p \simeq \frac{1.17}{q_i B} \frac{dT_{i0}}{dr} + \mathcal{O}\{\delta^2\}.$
- Including all the drives in the parallel plasma force balance above yields

$$egin{aligned} U_{i heta}(\psi_p) &\simeq \underbrace{U^0_{i heta}(\psi_p)}_{ ext{neoclassical}} - & rac{\langle ec{B}_0 \cdot (m_i n_{i0} \overline{ec{V}_i} \cdot ec{
abla} ec{ar{V}_i} + \overline{ec{
abla} \cdot ec{ar{m}_i} n_{i\wedge}}) \,
angle}{m_i n_{i0} \mu_{i00} \langle B_0^2
angle} &+ & rac{\langle ec{B}_0 \cdot ec{ar{J}_i} imes ec{ar{B}_\perp}
angle + \langle ec{B}_0 \cdot \sum_s ec{ar{S}}_{sm}
angle}{m_i n_{i0} \mu_{i00} \langle B_0^2
angle} \, . \ & \parallel \underbrace{ ext{Maxwell stress}} + ext{flow sources} \ \end{aligned}$$

• Given the poloidal flow $(\Omega_{*p} \equiv I U_{i\theta}/R^2)$, relation of toroidal flow to E_r is:

$$\Omega_t \equiv ec V \cdot ec
abla \zeta = -\left(rac{d\Phi}{d\psi_p} + rac{1}{n_i q_i} rac{dp_i}{d\psi_p}
ight) + \Omega_{*p} ~~ \Longrightarrow ~~ egin{array}{ll} V_t \simeq rac{E_r}{B_p} - rac{1}{n_i q_i B_p} rac{dp_i}{dr} + rac{1.17}{q_i B_p} rac{dT_i}{dr} \,.$$

How Can We Add These || Flow Damping Effects To Codes?

- Braginskii viscous force due to CGL form for parallel stresses is $\stackrel{\leftrightarrow}{\pi}_{\parallel} \equiv \pi_{\parallel} \left(\frac{\vec{B}\vec{B}}{B^2} - \frac{\stackrel{\leftrightarrow}{\mathbf{i}}}{3} \right), \quad \pi_{\parallel} \equiv -\frac{3}{2} \eta_0 \frac{\vec{B} \cdot \stackrel{\leftrightarrow}{\mathbf{W}} \cdot \vec{B}}{B^2}, \quad \stackrel{\leftrightarrow}{\mathbf{W}} \equiv \vec{\nabla}\vec{V} + (\vec{\nabla}\vec{V})^{\mathsf{T}} - \frac{2}{3} \stackrel{\leftrightarrow}{\mathbf{i}} (\vec{\nabla} \cdot \vec{V}).$
- Parallel component of parallel rate of strain has a couple of forms: $\vec{B} \cdot \vec{W} \cdot \vec{B}/2 = B(\vec{B} \cdot \vec{\nabla})(\vec{V} \cdot \vec{B}/B) + [\vec{B} \times (\vec{B} \times \vec{V})] \cdot \vec{\kappa} - (B^2/3)\vec{\nabla} \cdot \vec{V}$ $= B^2 \vec{V} \cdot \vec{\nabla} \ln B + \vec{B} \cdot \vec{\nabla} \times (\vec{V} \times \vec{B}) + (2B^2/3)\vec{\nabla} \cdot \vec{V} - (\vec{B} \cdot \vec{V})(\vec{\nabla} \cdot \vec{B}).$
- For $\vec{\nabla} \cdot \vec{B} = 0$, $\vec{\nabla} \cdot \vec{V} = 0$ and $\vec{V}_{\perp} = (1/B^2)\vec{B} \times \vec{\nabla}f$, the last form yields $\pi_{\parallel} = -3\eta_0 (\vec{V} \cdot \vec{\nabla} \ln B) + \Delta \pi_{\parallel}$, where $\Delta \pi_{\parallel} \equiv -(3\eta_0/B^3)(\vec{B} \cdot \vec{\nabla}f)[\vec{B} \cdot \vec{\nabla} \times (\vec{B}/B)]$ is small.
- Viscous force for the Braginskii viscous stress is $(\vec{\kappa} \text{ is curvature vector})$ $\vec{\nabla} \cdot \stackrel{\leftrightarrow}{\pi}_{\parallel} = \pi_{\parallel} [\vec{\kappa} - \vec{B} (\vec{B} \cdot \vec{\nabla} \ln B) / B^2] + (1/B^2) \vec{B} (\vec{B} \cdot \vec{\nabla}) \pi_{\parallel} - (1/3) \vec{\nabla} \pi_{\parallel}$ $\implies \vec{B}_0 \cdot \vec{\nabla} \cdot \stackrel{\leftrightarrow}{\pi}_{\parallel} = -\pi_{\parallel} (\vec{B}_0 \cdot \vec{\nabla} \ln B_0) + (2/3) (\vec{B}_0 \cdot \vec{\nabla}) \pi_{\parallel}.$
- FSA neglecting $\Delta \pi_{\parallel}$ & using $\vec{V} \cdot \vec{\nabla} \ln B_0 = (\vec{B}_0 \cdot \vec{\nabla} \ln B_0) U_{\theta}(\psi_p)$ yields $\langle \vec{B}_0 \cdot \vec{\nabla} \cdot \overleftrightarrow{\pi}_{\parallel} \rangle = 3\eta_0 \langle (\vec{B}_0 \cdot \vec{\nabla} \ln B_0)^2 \rangle U_{\theta},$ with $U_{\theta}(\psi) \equiv \frac{\vec{V} \cdot \vec{\nabla} \theta}{\vec{B}_0 \cdot \vec{\nabla} \theta}$ from $\vec{\nabla} \cdot \vec{V} = 0.$

Adding Parallel Flow Damping Effects To Codes (continued)

• A multi-collisionality parallel stress that yields the Braginskii and fluxsurface-averaged neoclassical closures has been proposed² ($\hat{\mathbf{b}} \equiv \vec{B}_0/B_0$):

$$egin{aligned} \pi_{\parallel} &= & -mn\,\mu\,\langle B_0^2
angle rac{\hat{\mathrm{b}}\cdotec{
abla}B_0}{\langle\,(\hat{\mathrm{b}}\cdotec{
abla}B_0)^2
angle}\,(U_ heta-U_ heta^0) \ & \ & -3\,\eta_0\left(rac{ec{B}\cdotec{
abla} imes(ec{N} imes(ec{N} imesec{B})}{B^2}+rac{2}{3}ec{
abla}\cdotec{V}-rac{(ec{B}\cdotec{V})(ec{
abla}\cdotec{B})}{B^2}
ight). \end{aligned}$$

- Electron neoclassical poloidal flow damping frequency μ is of the form $\mu_e \simeq \frac{2.3\sqrt{\epsilon}\,\nu_e}{(1+\nu_{*e}^{1/2}+\nu_{*e})(1+\epsilon^{3/2}\nu_{*e})},$ for collisionality parameter $\nu_{*e} \equiv \frac{\nu_e}{\epsilon^{3/2}\omega_{te}} = \frac{Rq}{\epsilon^{3/2}\lambda_e}$ \implies banana regime for $\nu_{*e} \ll 1$, plateau for $1 \ll \nu_{*e} \ll \epsilon^{-3/2}$, Braginskii for $\nu_{*e} \gg \epsilon^{-3/2}$.
- The "offset" poloidal flow velocity for electrons or ions is given by

$$U^0_{s heta}(\psi_p)\equiv k_s \, rac{I(\psi_p)}{q_s\langle B_0^2
angle} \, rac{dT_{s0}}{d\psi_p}, \qquad ext{in which } k_s ext{ has a form similar to } \mu_e.$$

²J.D. Callen, "Viscous Forces Due To Collisional Parallel Stress For Extended MHD Codes," UW-CPTC 09-6 (via http://www.cptc.wisc.edu).

Caveats And Long Term Needs

• PROPOSAL: Implement Braginskii operator with neoclassical viscous damping frequencies μ_e , μ_i and flow offsets $U_{e\theta}$, $U_{i\theta}$ in M3D and NIMROD³? Some issues for such a proposition:

Best form of π_{\parallel} to use? $\vec{V}_e \rightarrow -\vec{J}/n_e e \sim \nabla^2 \vec{B}$ yields 4th order operator in $\partial \vec{B}/\partial t$ eqn. Poloidal variation of viscous force for $\nu_* \ll 1$ not properly captured — but do we care? Long parallel scale variations should still be relaxed with Braginskii coefficient η_0 ? Need heat flow offsets (U^0_{θ}) to damp flows to nonzero values. Need $Z_{\rm eff}$ effects on μ for realistic tokamak plasma situations.

• Ultimate test of procedure is via more fundamental kinetic-based approach that solves drift-kinetic equation and uses result to obtain π_{\parallel} closure:

Held — finite element continuum solution of drift-kinetic equation, Ramos — ordered, closed fluid and electron formulation for slow-MHD.

• Challenge for kinetic-based approaches before it would be appropriate to implement them in M3D and NIMROD would be demonstration that they can obtain the axisymmetric neoclassical parallel Ohm's law including the bootstrap current and the neoclassical poloidal ion flow damping.

³C.R. Sovinec, www.cptc.wisc.edu/sovinec_research/notes/e_viscosity2.pdf; C.R. Sovinec et al., 2007 Sherwood Conf., Annapolis, MD.