# New Developments with M3D-C1

N.M. Ferraro, General Atomics M.S. Chance, J. Chen, S.C. Jardin, PPPL F. Delalondre, F. Zhang, RPI

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Resistive Wall Boundary Conditions

• Linear Non-Axisymmetric Response

• Nonlinear 3D





# Resistive Wall Boundary Conditions

• Linear Non-Axisymmetric Response

• Nonlinear 3D



#### **Thin-Shell Resistive Wall Boundary Conditions**

$$\mathbf{B} = \nabla \psi \times \nabla \varphi - \nabla_{\perp} f' + F \nabla \varphi$$
$$F = F_0 + R^2 \nabla_{\perp}^2 f$$

- M3D-C1 advances  $\psi$  and F
- Essential (Dirichlet) condition on  $\psi$  :

$$\frac{\partial \psi}{\partial t} = -\frac{\eta_W}{\delta} R \left( \hat{\mathbf{t}} \cdot \mathbf{B} - \hat{\mathbf{t}} \cdot \mathbf{B}^v \right) - \frac{V_L}{2\pi}$$

• Natural (Neumann) boundary condition on *F*:  $\int dV \frac{\mu}{R^2} \frac{\partial F}{\partial t} = -\oint dS \frac{\mu}{R} \frac{\eta_W}{\delta} \left( \frac{F}{R} - \hat{\varphi} \cdot \mathbf{B}^{\nu} \right) + \int dV \nabla \varphi \cdot \nabla \mu \times \mathbf{E}$ 



# Vacuum Response Depends on Plasma Response Non-Locally

$$\begin{pmatrix} \hat{\mathbf{n}} \cdot \mathbf{B}^{\nu} \end{pmatrix}_{i} = \begin{pmatrix} \hat{\mathbf{n}} \cdot \mathbf{B} \end{pmatrix}_{i}$$

$$\begin{pmatrix} \hat{\mathbf{t}} \cdot \mathbf{B}^{\nu} \end{pmatrix}_{i} = M_{ij}^{t} (\hat{\mathbf{n}} \cdot \mathbf{B})_{j}$$

$$\begin{pmatrix} \hat{\varphi} \cdot \mathbf{B}^{\nu} \end{pmatrix}_{i} = M_{ij}^{\varphi} (\hat{\mathbf{n}} \cdot \mathbf{B})_{j}$$

*i, j* range over all boundary nodes

- VACUUM\* calculates response matrices M in arbitrary geometry
- M is dense; all boundary nodes coupled to each other
  - Adds communication; hurts scalability
  - Not yet supported by SCOREC libraries in parallel

\* M.S. Chance, Phys. Plasmas 4, 2161 (1997)



#### **Resistive Wall Mode Test**

- Equilibrium is no-wall unstable
- Stable with conducting wall at b=1



- Growth rate should transition from ideal-wall limit to no-wall limit as  $\eta_w/\delta$  is increased.
- In the large-aspect limit, we know response matrix analytically





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# Linear Non-axisymmetric Field Response with M3D-C1

- $B(t) = B_0 + B_1(t)$ 
  - **B**<sub>0</sub> is the axisymmetric equilibrium field
  - B<sub>1</sub>(0) is the "vacuum field" from non-axisymmetric coils (I-coils).

### Conducting-wall boundary condition

- B held constant in time on simulation domain boundary (approximately vacuum vessel)
- Simulation is time-advanced until the steady-state is reached.
- Final B<sub>1</sub> is applied field + plasma response.



#### **Response Calculations Require Stable Equilibria**

- In practice, equilibria are almost always weakly unstable to "numerical tearing" modes
  - Due mainly to lack of resolution around rational surfaces
  - No steady-state  $\rightarrow$  This invalidates response
- With MARS, this is usually not a problem since the response frequency is chosen a priori
- With initial value code, the equilibrium must be made to be stable to these spurious modes
  - Change equations: thermal diffusion, viscosity
  - Change equilibrium: rotation



#### **Rotation & Dissipation Affect Stability & Screening**

- Dissipative terms inhibit screening response
  - Magnetic islands form
- Equilibrium rotation enhances screening



#### Rotation Improves Core Screening; But Stochasticizes Edge



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#### Summary of Non-Axisymmetric Results

- We are able to calculate response with Spitzer resistivity, rotation, and two-fluid terms
- Initial-value calculations require dissipation to ensure stability
  - Dissipation inhibits screening
- Rotation enhances screening
  - Direction of rotation is important even in single fluid MHD
- Poster Tuesday morning



# Unsplit Method Superior to Split Methods for Finding Linear Perturbed Equilibrium

- Split method has difficulty obtaining perturbed equilibrium
  - Persistent oscillations at low dissipation
  - More sensitive to  $\delta t$ Kinetic Energy 0.02 - Caramana method more 0.01 susceptible to  $( au_{A0}^{-1})$ numerical 0.00 instability in 2 (unsplit) -Implicit.  $\theta$ -Implicit (split) -0.01 under-resolved Caramana (split) cases -0.02

2000

4000

 $t (\tau_{AO})$ 

6000

0

8000

10000



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### M3D-C1 Uses Wedge-Shaped Elements in 3D

#### Tensor product

- Poloidal: reduced quintic  $(C^1)$
- Toroidal: reduced cubic polynomials (C<sup>1</sup>)
- Integration quadrature is also tensor product
- 6×2=12 DOFs/node
- 3D mesh is series of 2D planes
- Allows packing in toroidal direction





#### **3D Matrix Has Cyclic Block-Tridiagonal Form**

- Each plane corresponds to "block"
- Only nearest neighbor planes are coupled
- Presently this is solved without (further) preconditioning
- Typical problem: 10<sup>5</sup> DOFs/block





#### **3D Results: Alfven Wave**

• With just 2 toroidal planes,  $\omega$  is correct to 1 part in 10<sup>5</sup>





#### **3D Results: Anisotropic Diffusion in Helical Field**





#### Summary

- Resistive-wall boundary conditions are implemented
  - Not yet functional in parallel
- Linear 3D response successfully calculated with Spitzer resistivity, rotation, and two-fluid physics
- First fully-3D simulations have been run successfully
  - Much future work will involve solver strategies

