

Disruption Simulations

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Disruption simulation is controversial

- It's claimed that
 - The slow timescale of disruptions relative to the Alfvén time requires a 3D equilibrium code
 - Present simulation codes (M3D, Nimrod) use incorrect velocity boundary conditions
 - Magnetic boundary conditions do not include “wetting” of the wall by plasma so that “Hiro current” can flow

Disruptions have many causes: need XMHD, not 3D equilibrium

- VDE and kink modes
 - VDE carries plasma to wall, where it is scraped off, and destabilizes kink / tearing mode
 - Probably causes the most sideways wall force
- Tearing mode / NTM
 - NTM can be excited by a sawtooth
 - Requires kinetic closure
- RWM
 - RWM extensively studied linearly, not nonlinearly
 - Kinetic closure needed for better model
 - wall force may be small because of small growth rate
- Pellet / piece of wall tile falling into plasma
 - Wall tile causes 1/3 of C – mod disruptions
 - Local cooling increases pressure gradient

Causes of disruptions 2

- Pressure driven modes
 - Important for thermal stress on wall
 - Could be caused by alpha heating in burning plasma
 - Mitigation - MGI
- In general need XMHD, kinetic effects
 - RWM
 - NTM
 - Can these modes saturate before disrupting?
 - Are they important for sideways wall force?
 - Runaway electrons
- Time – scale: will return to this later
- A 3D equilibrium is inadequate to deal with disruption physics

Boundary conditions

- M3D and NIMROD assume no flow through boundary condition
- A possible boundary condition was used in DEBS (Schnack et al, JCP 70, 333, 1987)

$$v = \frac{E \times B}{B^2} \quad E = \eta_w J_w \quad J_w = \frac{B_{vac} - B_{plasma}}{\delta}$$

$$v_n = \frac{\eta_w F_w}{\delta B_w^2} \quad v_n = \frac{\eta_w (B_{vac}^2 - B_{plasma}^2)}{\delta B_w^2}$$

Boundary conditions 2

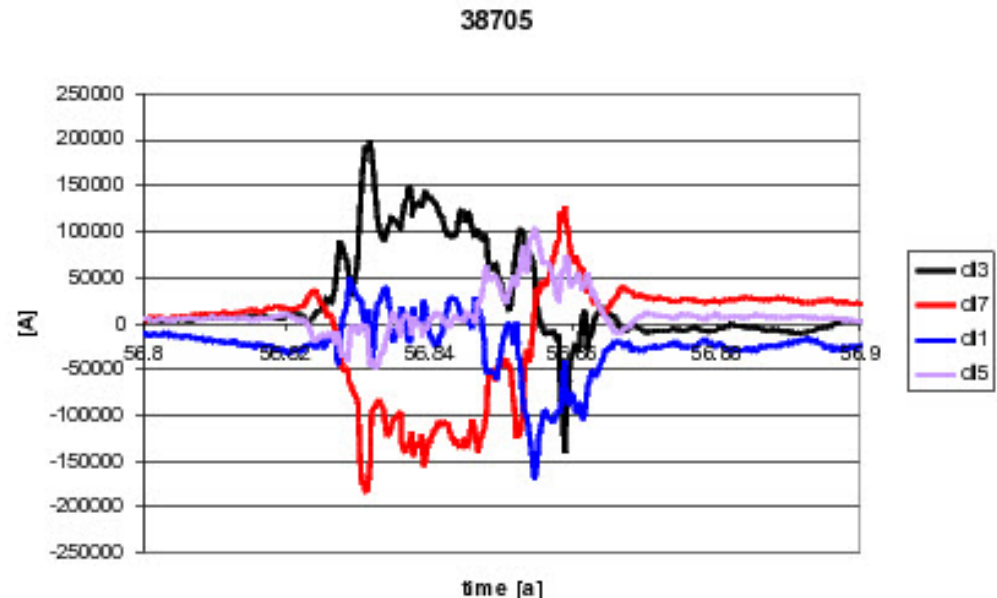
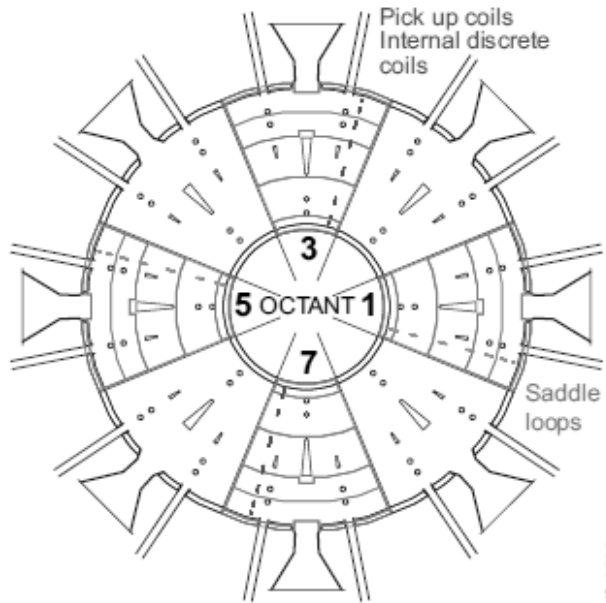
- DEBS boundary condition was tried in M3D
 - Made little difference
- Flow through boundary condition

$$\frac{\partial v_n}{\partial n} = -\frac{v_n}{d} \quad v_n = -dv_n' \cong 0$$

- If $d \ll a$, ($d = a/4$) verified that it makes little difference
- There is no theory of absorbing boundary condition for normal velocity, only parallel velocity
- sheath potential: if wall is an equipotential,
$$v = \frac{\partial \Phi}{\partial n} n \times B / B^2$$

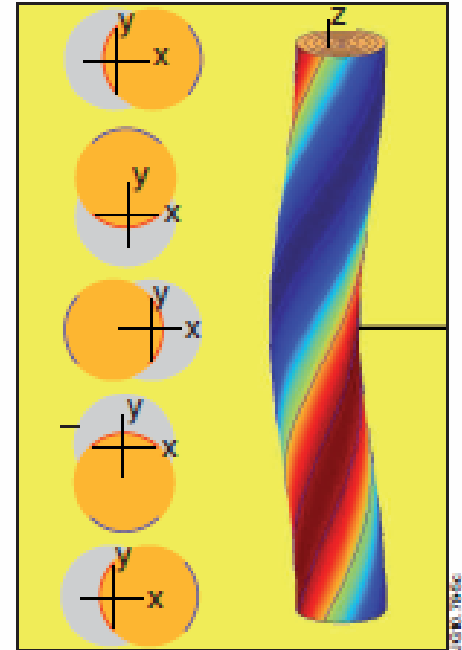
Hiro current

- In JET, the toroidal current varied as a function of toroidal angle
- This was correlated with toroidally varying vertical displacement
- From Gerasimov et al, JET 2009



Hiro current 2

- This was "explained" using the Hiro current theory (Zakharov, Phys. Plasmas 15, 062507 2008)
 - Plasma is unstable to $n = 1$ kink
 - Where the kinked plasma "wets" the wall, hiro current can flow into the wall
 - This causes remaining bulk plasma current to vary toroidally, in phase with the toroidally varying vertical plasma displacement
- The "hiro current" and "wetting" ideas caused a lot of confusion
 - Are codes like M3D and NIMROD able to produce hiro current effects?



Hiro current 3

- M3D and NIMROD allow halo current
- Hiro current is a component of halo current
 - It was confusing because in 2D studies of VDEs there is no hiro current
 - Hiro current is a 3D effect

• Hiro current is net normal current through the wall

$$I_{hiro} = \int J_n R dl$$

$$\nabla \cdot \mathbf{J} = 0 \quad \text{implies}$$

$$I_\varphi = \int J_\varphi dR dZ$$

Hiro current vanishes in 2D

$$J_n = \nabla I \times \nabla \varphi$$

$$\frac{dI_\varphi}{d\varphi} = -I_{hiro}$$

Toroidal variation of toroidal Current ~ hiro current

halo current

- Halo current is poloidal current that flows into the wall in a VDE or disruption
 - Net total halo current is hiro current
 - Net conventional (2D) halo current vanishes
 - Conventional halo current can be measured by $\frac{1}{2}$ absolute value

$$I_{halo} = \frac{1}{2} \int |J_n - J_{hiro}| R dl$$

$$J_{hiro} = \int J_n R dl / \int R dl$$

Where does Hiro current come from?

- In 2D, toroidally averaged case, there is no Hiro current, only halo current
- M3D magnetic field and current

$$B = \nabla \psi \times \nabla \varphi + I \nabla \varphi + \frac{\nabla_{\perp} F}{R}$$

$$J = -\Delta^* \psi \nabla \hat{\varphi} + \nabla I \times \nabla \varphi + \frac{1}{R^2} \nabla_{\perp} \frac{\partial \psi}{\partial \varphi} + \dots$$

Toroidal
current

Halo term
gives halo
at wall

Hiro term

Hiro current calculation

- In Strauss et al, Phys. Plasma 17, 082506 (2010) it was shown in a model calculation and verified in simulations that, as in JET

$$\frac{dI_{\phi}}{d\phi} = \frac{\xi_{VDE}}{a^2} \frac{dM_{IZ}}{d\phi}$$

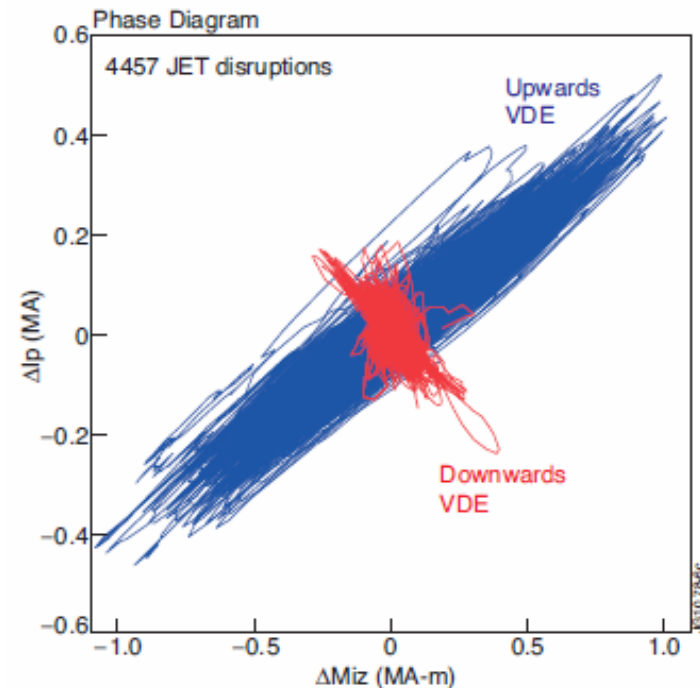
Hiro current is given by

$$I_{hiro} = -\frac{\xi_{VDE}}{a^2} \frac{dM_{IZ}}{d\phi}$$

Where the vertical
Current moment is

$$M_{IZ} = \int ZJ_{\phi} dRdZ$$

Hiro current can be calculated directly



From Gerasimov. EPS 2009

TPF and halo current fraction

- Can relate TPFxHalo current fraction to toroidal current perturbation
- It appears that the varying part of halo current is mostly hiro current, while the average part is halo current, and they have comparable magnitude

$$I_{hiro} \approx I_{halo}$$

$$TPF = \frac{I_{hiro-max} - I_{hiro-min}}{\langle I_{halo} \rangle} \approx 2$$

$\langle .. \rangle$ is toroidal average

Halo current fraction is ratio of average halo current to toroidal current

$$H_f = \frac{\langle I_{halo} \rangle}{\langle I_{\varphi} \rangle}$$

TPF and halo fraction 2

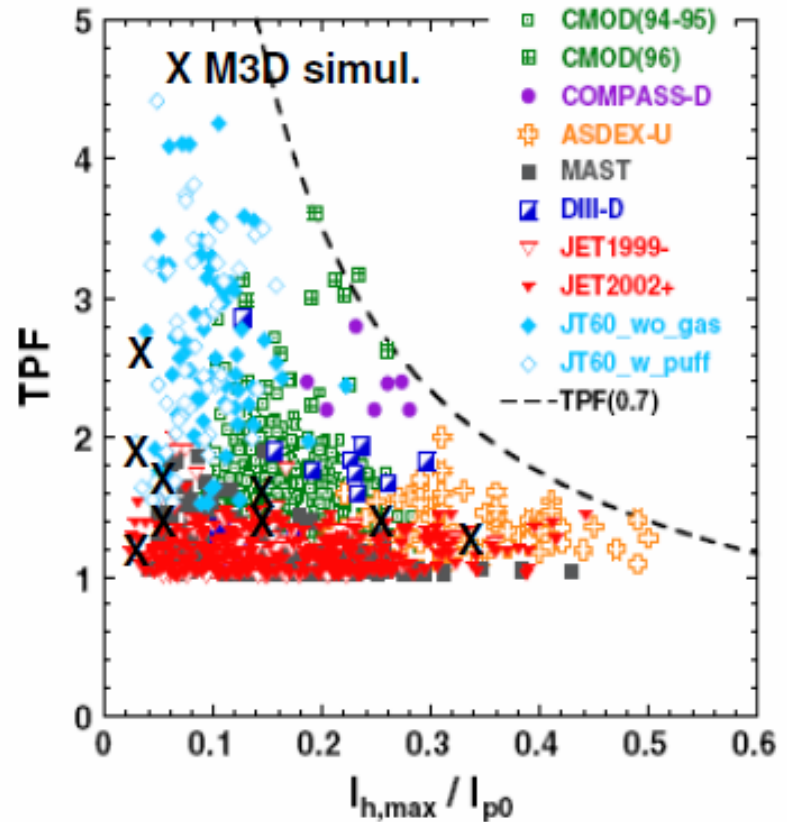
- Simulational results and ITER database

$$TPF \times H_f = 2 \frac{I_{hiro}}{\langle I_\varphi \rangle}$$

$$= \frac{2}{\langle I_\varphi \rangle} \frac{dI_\varphi}{d\varphi} = 2 \frac{\Delta I_\varphi}{I_\varphi} < 0.7$$

$$\frac{\Delta I_\varphi}{I_\varphi} < 0.35$$

M3D simulations have current perturbation ~ 0.2



“Wetting” and halo model

- If plasma is surrounded by a real vacuum, wetting is a problem
- In M3D and NIMROD the “vacuum” is represented by cold plasma
 - Current can flow from the plasma to the wall
 - No need for plasma to penetrate the wall
 - Halo plasma = SOL
- Halo width is time dependent, it gets bigger in a disruption
- Wall force is only weakly dependent on halo resistivity

Halo resistivity model

- Halo (SOL) resistivity model used in TSC (Sayer et al. Nucl. Fusion 33, 969, 1993) : 3 regions

$$\eta = \eta(T) \quad \psi < \psi_{core}$$

$$\eta = \eta_{halo} \quad \psi_{core} < \psi < \psi_{vacuum}$$

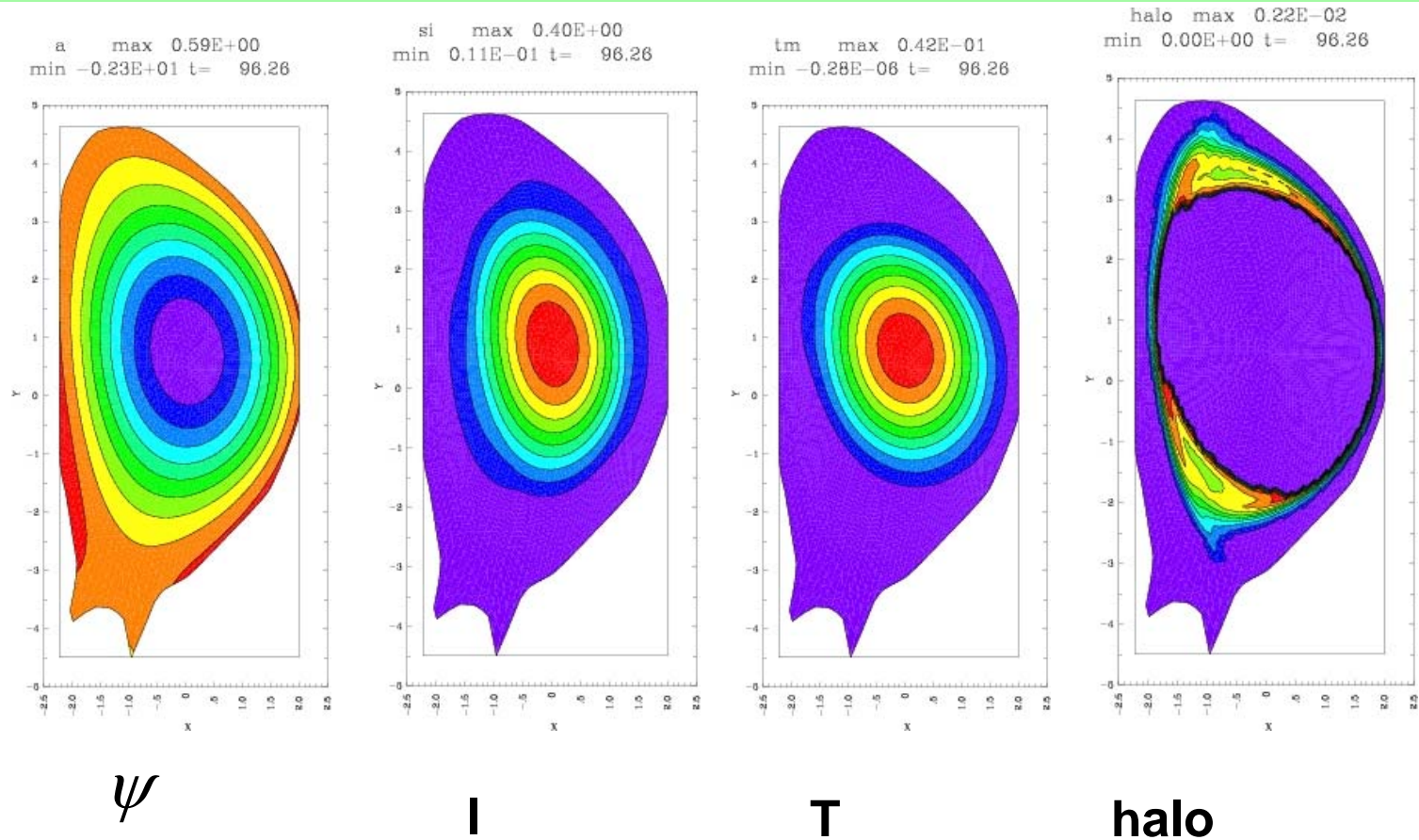
$$\eta = \eta_{vacuum} \quad \psi_{vacuum} < \psi$$

- in 3D this does not work because flux surfaces might not exist

replace $\psi_{core}, \psi_{vacuum}$ with T_{core}, T_{vacuum}

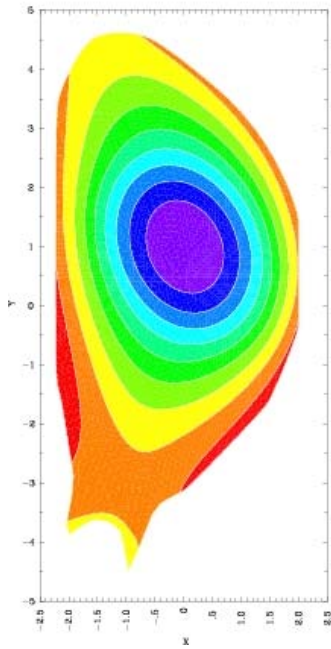
- want to determine effect of these parameters on wall force, etc.
- halo width increases during disruption

Halo in (2,1) tearing disruption



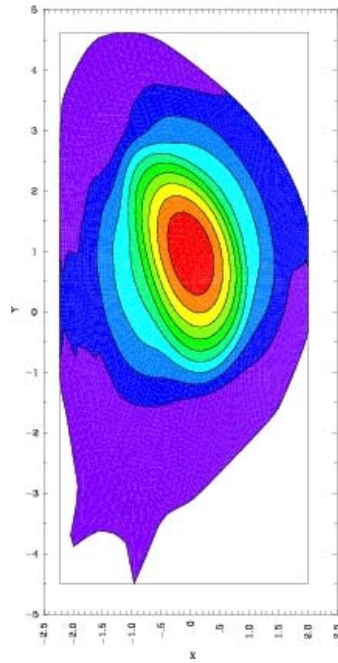
Halo in (2,1) tearing disruption

a max 0.79E+00
min -0.20E+01 t= 108.28



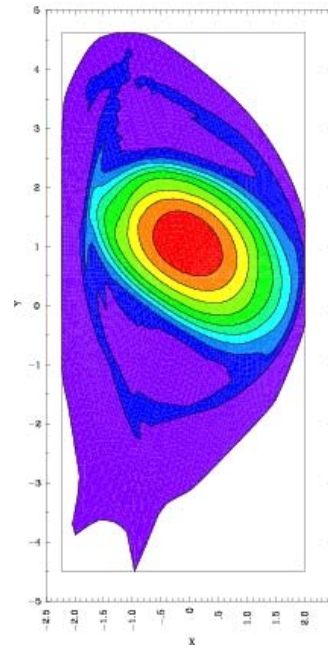
ψ

si max 0.38E+00
min 0.48E-01 t= 108.28



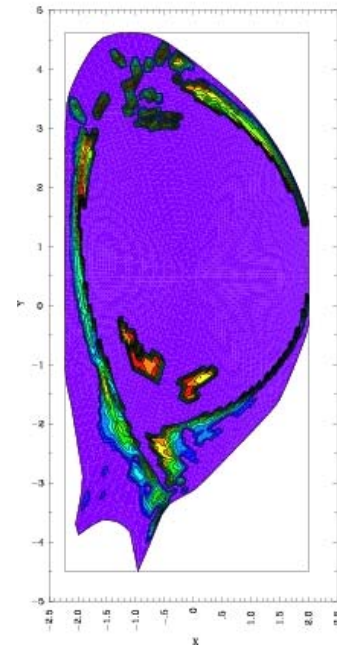
I

tm max 0.42E-01
min -0.49E-05 t= 108.28



T

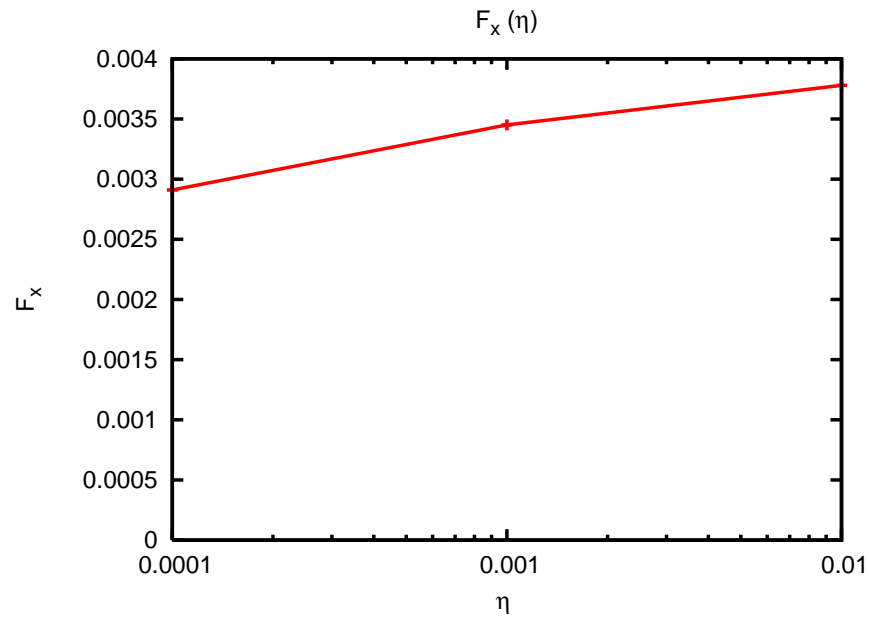
halo max 0.22E-02
min 0.00E+00 t= 108.28



halo

Halo resistivity and wall force

- The wall force is insensitive to the halo resistivity

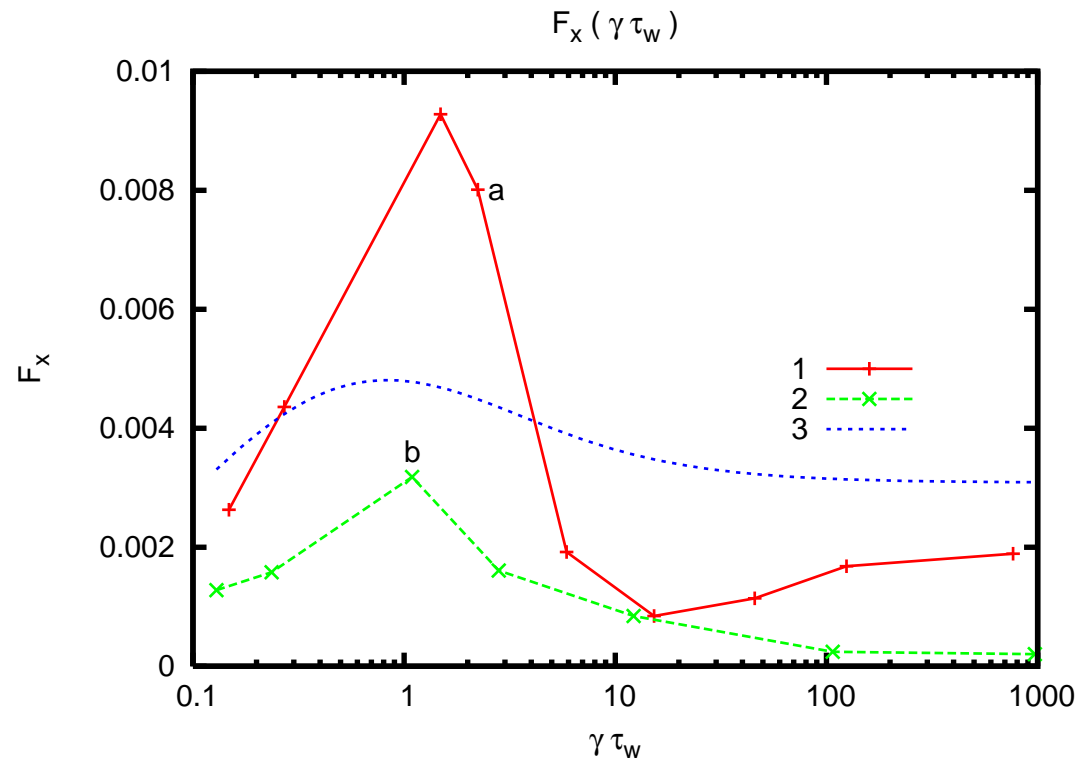


summary

- Many kinds of disruptions
 - Need X MHD physics
 - Even VDE/kink disruption involves scrape off at wall
 - 3D equilibrium code inadequate
- Velocity boundary condition
 - So far has not made much difference
- Hiro current
 - M3D contains “wetting”
 - Hiro current is the net halo current
 - Causes toroidal variation of toroidal current
- Halo modeling in progress
 - Region between plasma and “vacuum”
 - Halo resistivity had moderate effect on wall force

Time scale

- M3D simulations were criticized because the wall time in the simulations was short
 - In fact wall time was 10 – 10,000 Alfvén times
 - It was found that the largest wall force occurred when the mode nonlinear evolution time was comparable to the resistive wall penetration time
 - The modes studied so far had fast growth rates so wall time was chosen to be short for maximum effect



Time scale 2

- resistive wall mode (RWM) grows at wall penetration rate
 - Does wall force scale with growth rate as well as depending on “resonance” with wall time? If so, wall force will be small.

$$F_{wall} \propto \gamma I^2 f(\gamma \tau_{wall})$$

- **Plan RWM simulations in future**
- **Other “slow” modes - NTM**

Future plans

- Improve modeling of “vacuum” and halo region
- Scrape off of plasma by VDE
- Improve wall model
 - Two ITER walls with blanket structure in between
 - Two thin walls
 - Blanket will be modeled by spatially varying resistivity, $\nu = 0$
- Higher S, higher resolution
 - Study of RWM disruptions
 - Dependence of wall force on growth rate