

Present Status of M3D

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FDM3D Workshop
Princeton
March 19, 2007

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Capsule History of M3D

- Original **MH3D** (W.P., early 1980s) was a serial Fortran code in a single source file solving resistive MHD using finite differences on a radial mesh with spectral treatment of θ and ϕ .
- Over more than a decade, gradual refinements and enhancements of the physical model (hybrid [W.P.] and two-fluid [L.S.] models) and numerical scheme (finite elements [H.S.]) were accreted onto this program, forming the Multilevel 3D Code (**M3D**). This was eventually parallelized using OpenMP.
- Around 1999, X.T. set out to create an MPI version of the code. Doing a complete rewrite, he created a C code distributed over many files within two layers of directories, using linear triangular finite elements on a domain decomposed both poloidally and toroidally to solve MHD only, using the PETSc software library to handle communications and linear solves. This was **ParM3D**.
- In order to retain much of the physics and flexibility of the original version, H.S. undertook to couple the two codes together, using ParM3D for mesh generation, I/O, and linear solvers with the original Fortran “m1.F” as the physics driver. Data would be passed between the C and Fortran parts of the new code using a new set of Fortran and C interface routines. Much of the now-unused part of ParM3D was left in the distribution in vestigial form. This is **M3DP** (still referred to as **M3D**).
- A CVS repository for the modern M3D was started in 2001. Changes made since then are archived in `/p/m3d/README` on the PPPL Unix cluster. Highlights include refinement of the two-fluid options; improvement and parallelization of the hot particle treatment; addition of 2nd- and 3rd-order element options; and addition of vacuum region/resistive wall capability. The current version number is 3.5.12.

Platforms

M3D has been ported to the following computers at NERSC, NCCS, Princeton, and ANL:

	OpenMP	MPI
IBM SP (Seaborg)	Y	Y
Opteron cluster (Jacquard)		Y
IBM Power 5 (Bassi)	?	Y
Cray X1E (Phoenix)		Y*
Cray XT3, XT4 (Jaguar)		Y
SGI Origin 2000 (Hecate)	Y	
SGI Altix (MHD)	Y	Y
BlueGene/L, Argonne		Y*

*Not used for production runs.

Statistics

- Source code is divided into four directories (m3d, mhd, mesh, utility) with 34 subdirectories.
- There are approximately 264 C source files, 216 C header files, 33 Fortran source files, 16 Fortran header files, and 35 Makefiles.
- There are approximately 52,000 lines of C and 97,000 lines of Fortran source code.
- This includes a lot of code that is no longer executed (or, in many cases, compiled), but excludes standalone post-processing utilities and many trial routines that have not yet been committed to the repository.
- Libraries required include PETSc, parallel HDF5, and sometimes FFTW.
- Three standard input files (plus batch script), others optional; recently consolidated to a single Python script.
- Performance record: 240 Gflops on 10,240 XT3 cores (VN mode) during a 1D weak scaling test.

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Extended MHD Equations

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}_i) = 0$$

$$\rho \left[\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} + (\mathbf{v}_i^* \cdot \nabla) \mathbf{v}_\perp \right] = -\nabla p + \mathbf{J} \times \mathbf{B} + \mu \nabla^2 \mathbf{v}$$

$$\mathbf{E} + \mathbf{v} \times \mathbf{B} = \eta \mathbf{J} - \frac{\nabla_\parallel p_e}{ne}$$

$$\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times \mathbf{E}$$

$$\mathbf{J} = \nabla \times \mathbf{B}$$

$$\frac{\partial p}{\partial t} + \mathbf{v} \cdot \nabla p = -\gamma p \nabla \cdot \mathbf{v} + \nabla \cdot n \chi_\perp \nabla \left(\frac{p}{\rho} \right) - \mathbf{v}_i^* \cdot \nabla p - \gamma p \nabla \cdot \mathbf{v}_i^* + \frac{\mathbf{J} \cdot \nabla p_e}{ne} + \gamma p_e \mathbf{J} \cdot \nabla \left(\frac{1}{ne} \right)$$

$$\frac{\partial p_e}{\partial t} + \mathbf{v} \cdot \nabla p_e = -\gamma p_e \nabla \cdot \mathbf{v} + \nabla \cdot n \chi_{\perp e} \nabla \left(\frac{p_e}{\rho} \right) + \frac{\mathbf{J}_\parallel \cdot \nabla p_e}{ne} - \gamma p_e \nabla \cdot \left(\mathbf{v}_e^* - \frac{\mathbf{J}_\parallel}{ne} \right)$$

where

$$\mathbf{v}_e^* \equiv -\frac{\mathbf{B} \times \nabla p_e}{neB^2}, \quad \mathbf{v}_i^* \equiv \mathbf{v}_e^* + \frac{\mathbf{J}_\perp}{ne},$$

$$\mathbf{v} \equiv \mathbf{v}_i - \mathbf{v}_i^* = \mathbf{v}_e - \mathbf{v}_e^* + \frac{\mathbf{J}_\parallel}{ne}$$

Artificial sound wave model for κ_\parallel :

$$\frac{\partial T}{\partial t} = s \frac{\mathbf{B} \cdot \nabla u}{\rho}$$

$$\frac{\partial u}{\partial t} = s \mathbf{B} \cdot \nabla T + \nu \nabla^2 u$$

M3D Scalar Variables

Field Variables

Write

$$\vec{B} = \nabla \psi \times \nabla \phi + \frac{1}{R} \nabla_{\perp} F + (R_0 + \tilde{I}) \nabla \phi$$

where

$$\nabla_{\perp}^2 F = -\frac{1}{R} \frac{\partial \tilde{I}}{\partial \phi}$$

so that

$$\vec{J} = \left(\nabla \tilde{I} - \frac{1}{R} \nabla_{\perp} F' \right) \times \nabla \phi + \frac{1}{R^2} \nabla_{\perp} \psi' - C \nabla \phi$$

where primes denote derivatives with respect to ϕ and

$$C \equiv -R J_{\phi} = \Delta^* \psi + \frac{1}{R} \frac{\partial F}{\partial z}$$

Velocity Variables

Write

$$\vec{V} = \frac{R^2}{R_0} \nabla U \times \nabla \phi + \nabla_{\perp} \chi + V_{\phi} \hat{\phi}$$

Others

$$\rho, p_{(e,i)} \text{ or } T_{(e,i)}$$

Note that

$$\nabla_{\perp}^2 \psi \equiv \frac{\partial^2 \psi}{\partial R^2} + \frac{\partial^2 \psi}{\partial z^2},$$

$$\Delta^* \psi \equiv \nabla_{\perp}^2 \psi - \frac{1}{R} \frac{\partial \psi}{\partial R} = \frac{\partial^2 \psi}{\partial R^2} - \frac{1}{R} \frac{\partial \psi}{\partial R} + \frac{\partial^2 \psi}{\partial z^2},$$

and

$$\Delta^{\dagger} \psi \equiv \nabla_{\perp}^2 \psi + \frac{1}{R} \frac{\partial \psi}{\partial R} = \frac{\partial^2 \psi}{\partial R^2} + \frac{1}{R} \frac{\partial \psi}{\partial R} + \frac{\partial^2 \psi}{\partial z^2}.$$

M3D Form of the Resistive MHD Equations

Define Poisson Bracket $[A, B] \equiv \nabla_{\perp} A \times \nabla_{\perp} B \cdot \hat{\phi} = \frac{\partial A}{\partial R} \frac{\partial B}{\partial z} - \frac{\partial A}{\partial z} \frac{\partial B}{\partial R}$

and $(A, B) \equiv \nabla_{\perp} A \cdot \nabla_{\perp} B = \frac{\partial A}{\partial R} \frac{\partial B}{\partial R} + \frac{\partial A}{\partial z} \frac{\partial B}{\partial z}$

Continuity:

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \vec{V}) = -\rho \left(\Delta^{\dagger} \chi + \frac{2}{R_0} \frac{\partial U}{\partial z} + \frac{1}{R} \frac{\partial V_{\phi}}{\partial \phi} \right) - \frac{R}{R_0} [\rho, U] - (\rho, \chi) - \frac{V_{\phi}}{R} \frac{\partial \rho}{\partial \phi} \quad (1)$$

Operate on the momentum equation with $-R_0 \hat{\phi} \cdot \nabla \times$ to get an equation for the evolution of $\Delta^{\dagger} U \equiv \nabla_{\perp}^2 U + \frac{1}{R} \frac{\partial U}{\partial R}$ (called “w” in the code):

$$\begin{aligned} \frac{\partial}{\partial t} \Delta^{\dagger} U &= \frac{R}{R_0} [U, \Delta^{\dagger} U] - (\chi, \Delta^{\dagger} U) - \Delta^{\dagger} U \left(\Delta^{\dagger} \chi + \frac{2}{R_0} \frac{\partial U}{\partial z} \right) - \frac{V_{\phi}}{R} \frac{\partial}{\partial \phi} \Delta^{\dagger} U - \left(\frac{V_{\phi}}{R}, \frac{\partial U}{\partial \phi} \right) \\ &+ 2R_0 \frac{V_{\phi}}{R} \frac{\partial}{\partial z} \frac{V_{\phi}}{R} + \frac{R_0}{R} \left[\frac{V_{\phi}}{R}, \frac{\partial \chi}{\partial \phi} \right] + R_0 \left\{ \vec{B} \cdot \nabla \left(\frac{C}{R^2 \rho} \right) + \vec{J} \cdot \nabla \left(\frac{1 + \tilde{I} / R_0}{R^2 \rho} \right) \right\} + \frac{2}{R^2 \rho} \frac{\partial p}{\partial z} \\ &+ R \left[\frac{1}{R^2 \rho}, p \right] - R_0 \nabla \phi \cdot \nabla \times \left(\frac{\mu \nabla^2 \vec{V}}{\rho} \right) \end{aligned} \quad (2a)$$

Evolution of the Compressible Velocity

From the definition of the velocity, it is clear that

$$\frac{\partial \chi}{\partial R} = \hat{R} \cdot \vec{V} - \frac{R}{R_0} \frac{\partial U}{\partial z} \quad \text{and} \quad \frac{\partial \chi}{\partial z} = \hat{z} \cdot \vec{V} + \frac{R}{R_0} \frac{\partial U}{\partial R}$$

so that, again using the momentum equation,

$$\begin{aligned} \frac{\partial}{\partial t} \left(\frac{\partial \chi}{\partial R} \right) &= -\frac{R}{R_0} \frac{\partial}{\partial z} \left(\frac{\partial U}{\partial t} \right) - \vec{V}_\perp \cdot \nabla_\perp \left(\frac{\partial \chi}{\partial R} + \frac{R}{R_0} \frac{\partial U}{\partial z} \right) - \frac{V_\phi}{R_0} \frac{\partial U'}{\partial z} - \frac{V_\phi}{R} \frac{\partial \chi'}{\partial R} + \frac{V_\phi^2}{R} - \frac{1}{\rho} \frac{\partial p}{\partial R} \\ &+ \frac{1}{R^2 \rho} (R_0 + \tilde{I}) \left[\frac{1}{R} \left(\frac{\partial F'}{\partial R} + \frac{\partial \psi'}{\partial z} \right) - \frac{\partial \tilde{I}}{\partial R} \right] + \frac{C}{R^2 \rho} \left(\frac{\partial F}{\partial z} - \frac{\partial \psi}{\partial R} \right) + \frac{\mu}{\rho} \hat{R} \cdot \nabla^2 \vec{V} \end{aligned} \quad (2b)$$

and

$$\begin{aligned} \frac{\partial}{\partial t} \left(\frac{\partial \chi}{\partial z} \right) &= \frac{R}{R_0} \frac{\partial}{\partial R} \left(\frac{\partial U}{\partial t} \right) - \vec{V}_\perp \cdot \nabla_\perp \left(\frac{\partial \chi}{\partial z} - \frac{R}{R_0} \frac{\partial U}{\partial R} \right) + \frac{V_\phi}{R_0} \frac{\partial U'}{\partial R} - \frac{V_\phi}{R} \frac{\partial \chi'}{\partial z} - \frac{1}{\rho} \frac{\partial p}{\partial z} \\ &+ \frac{1}{R^2 \rho} (R_0 + \tilde{I}) \left[\frac{1}{R} \left(\frac{\partial F'}{\partial z} - \frac{\partial \psi'}{\partial R} \right) - \frac{\partial \tilde{I}}{\partial z} \right] - \frac{C}{R^2 \rho} \left(\frac{\partial F}{\partial R} + \frac{\partial \psi}{\partial z} \right) + \frac{\mu}{\rho} \hat{z} \cdot \nabla^2 \vec{V} \end{aligned} \quad (2c)$$

Evolution of the Toroidal Velocity

Dot the momentum equation with $\hat{\phi}$ to find

$$\begin{aligned} \frac{\partial V_\phi}{\partial t} &= \frac{R}{R_0} [U, V_\phi] - (\chi, V_\phi) - \frac{V_\phi}{R} \left(V_\phi' + \frac{\partial \chi}{\partial R} \right) - \frac{V_\phi}{R_0} \frac{\partial U}{\partial z} - \frac{1}{R\rho} \frac{\partial p}{\partial \phi} \\ &+ \frac{1}{R^2 \rho} [\tilde{I}, \psi] + \frac{1}{R^2 \rho} (\tilde{I}, F) + \frac{1}{R^3 \rho} \frac{\partial}{\partial \phi} [\psi, F] - \frac{1}{2R^3 \rho} \frac{\partial}{\partial \phi} (|\nabla_\perp \psi|^2 + |\nabla_\perp F|^2) \\ &+ \frac{\mu}{\rho} \left[\nabla^2 V_\phi - \frac{V_\phi}{R^2} + \frac{2}{R^2} \frac{\partial}{\partial \phi} \left(\frac{R}{R_0} \frac{\partial U}{\partial z} + \frac{\partial \chi}{\partial R} \right) \right] \end{aligned} \quad (2d)$$

Electrostatic Potential

If $\vec{B} = \nabla \times \vec{A}$ and $\frac{\partial \vec{B}}{\partial t} = -\nabla \times \vec{E}$ then $\frac{\partial \vec{A}}{\partial t} = -\vec{E} + \nabla \Phi$ where, if we choose the gauge

$\nabla_{\perp} \cdot \vec{A} = 0$, we find $\nabla_{\perp}^2 \Phi = \nabla_{\perp} \cdot \vec{E}$.

For the resistive MHD Ohm's law, that means

$$\begin{aligned} \nabla_{\perp}^2 \Phi = & \frac{1}{R_0} (\tilde{I}, U) + \left(1 + \frac{\tilde{I}}{R_0}\right) \nabla_{\perp}^2 U - \frac{V_{\phi}}{R} \Delta^* \psi + \frac{R_0}{R^2} \frac{\partial \chi}{\partial z} + \left[\chi, \frac{\tilde{I}}{R}\right] - \left[F, \frac{V_{\phi}}{R}\right] - \frac{1}{R} (V_{\phi}, \psi) \\ & + \frac{\eta}{R^2} \left[\frac{1}{R} \left(\frac{\partial F'}{\partial z} - \frac{\partial \psi'}{\partial R} \right) - \frac{\partial \tilde{I}}{\partial z} + \frac{\partial C}{\partial \phi} \right] + \frac{1}{R} [\eta, \tilde{I}] - \frac{1}{R^2} [\eta, F'] + \frac{1}{R^2} (\eta, \psi') \end{aligned} \quad (3)$$

Evolution of the Poloidal Field

The time derivative of ψ (called “a” in the code) is simply $R\hat{\phi} \cdot \frac{\partial \vec{A}}{\partial t}$,

$$\frac{\partial \psi}{\partial t} = \frac{R}{R_0} [U, \psi] + \frac{R}{R_0} (U, F) - (\chi, \psi) + [\chi, F] + \eta C + \frac{\partial \Phi}{\partial \phi}. \quad (4)$$

but for numerical stability, the quantity we generally choose to evolve is instead

$C_a \equiv \Delta^* \psi$:

$$\begin{aligned} \frac{\partial C_a}{\partial t} = & \frac{R}{R_0} \left\{ [U, C_a] + [\Delta^\dagger U, \psi] + 2 \left[\frac{\partial U}{\partial R}, \frac{\partial \psi}{\partial R} \right] + 2 \left[\frac{\partial U}{\partial z}, \frac{\partial \psi}{\partial z} \right] \right\} + \frac{2}{R_0} \left[U, \frac{\partial \psi}{\partial R} \right] + \frac{2}{R_0 R} \frac{\partial U}{\partial z} \frac{\partial \psi}{\partial R} \\ & + \frac{R}{R_0} \left\{ (U, \nabla_\perp^2 F) + (\Delta^\dagger U, F) + 2 \left(\frac{\partial U}{\partial R}, \frac{\partial F}{\partial R} \right) + 2 \left(\frac{\partial U}{\partial z}, \frac{\partial F}{\partial z} \right) \right\} + \frac{1}{R_0} \left(\frac{\partial F}{\partial R}, U \right) - \frac{1}{R_0 R} \frac{\partial F}{\partial z} \frac{\partial U}{\partial z} \\ & - \left\{ (\psi, \nabla_\perp^2 \chi) + (C_a, \chi) + 2 \left(\frac{\partial \psi}{\partial R}, \frac{\partial \chi}{\partial R} \right) + 2 \left(\frac{\partial \psi}{\partial z}, \frac{\partial \chi}{\partial z} \right) \right\} + \frac{1}{R} \left(\frac{\partial \chi}{\partial R}, \psi \right) + \frac{1}{R^2} \frac{\partial \psi}{\partial R} \frac{\partial \chi}{\partial R} \\ & + \left\{ [\nabla_\perp^2 \chi, F] + [\chi, \nabla_\perp^2 F] + 2 \left[\frac{\partial \chi}{\partial R}, \frac{\partial F}{\partial R} \right] + 2 \left[\frac{\partial \chi}{\partial z}, \frac{\partial F}{\partial z} \right] \right\} - \frac{1}{R} \left\{ \left[\frac{\partial \chi}{\partial R}, F \right] + \left[\chi, \frac{\partial F}{\partial R} \right] \right\} \\ & + \frac{\partial}{\partial \phi} (\nabla_\perp^2 \Phi) - \frac{1}{R} \frac{\partial^2 \Phi}{\partial \phi \partial R} \end{aligned} \quad (4')$$

Evolution of the Toroidal Field

The magnetic field is completely specified by two scalar functions; the auxiliary variable F is related to the non-vacuum toroidal field \tilde{I}/R by the elliptic equation given earlier. The evolution of \tilde{I} can be found from the toroidal component of the field equation:

$$\begin{aligned} \frac{\partial \tilde{I}}{\partial t} = & \frac{R}{R_0} [U, \tilde{I}] - (\chi, \tilde{I}) + R \left[\frac{V_\phi}{R}, \psi \right] + R \left(\frac{V_\phi}{R}, F \right) - (R_0 + \tilde{I}) \Delta^* \chi - \frac{V_\phi}{R} \frac{\partial \tilde{I}}{\partial \phi} \\ & + \eta \left[\Delta^* \tilde{I} - \frac{1}{R} \nabla_\perp^2 F' + \frac{2}{R^2} \left(\frac{\partial \psi'}{\partial z} + \frac{\partial F'}{\partial R} \right) \right] - \frac{1}{R} [\eta, \psi'] + (\eta, \tilde{I}) - \frac{1}{R} (\eta, F') \end{aligned} \quad (5)$$

The Energy Equation

The energy equation in the resistive MHD version M3D is normally solved in terms of the plasma pressure; simple substitution of the code variables into the pressure equation gives

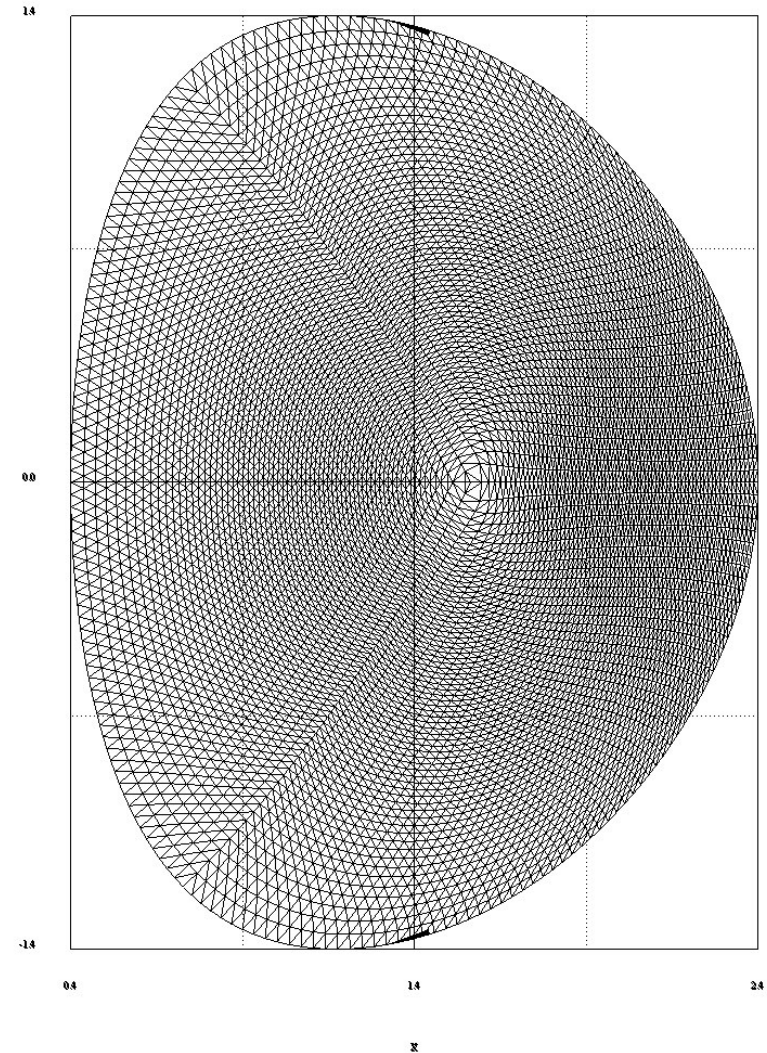
$$\frac{\partial p}{\partial t} = \frac{R}{R_0} [U, p] - (\chi, p) - \frac{V_\phi}{R} \frac{\partial p}{\partial \phi} - \gamma p \left(\frac{2}{R_0} \frac{\partial U}{\partial z} + \Delta^\dagger \chi + \frac{1}{R} \frac{\partial V_\phi}{\partial \phi} \right) + \rho \nabla \cdot \left[\kappa_\perp \nabla \left(\frac{p}{\rho} \right) \right] \quad (6)$$

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The M3D Mesh

- Uses linear basis functions on **unstructured triangular finite element** mesh in each constant- ϕ plane.
- 3 parameters control mesh resolution: # of planes, # of radial grids, # of theta sections.
- Mesh has same topology in all planes. In the tokamak case, it has the same geometry in all planes as well.
- Mesh is aligned with equilibrium flux surfaces (from VMEC-generated input files) but does not follow field lines.
- Uses either 4th-order finite differences or pseudo-spectral derivatives between planes.



Packing the Mesh at a Flux Surface

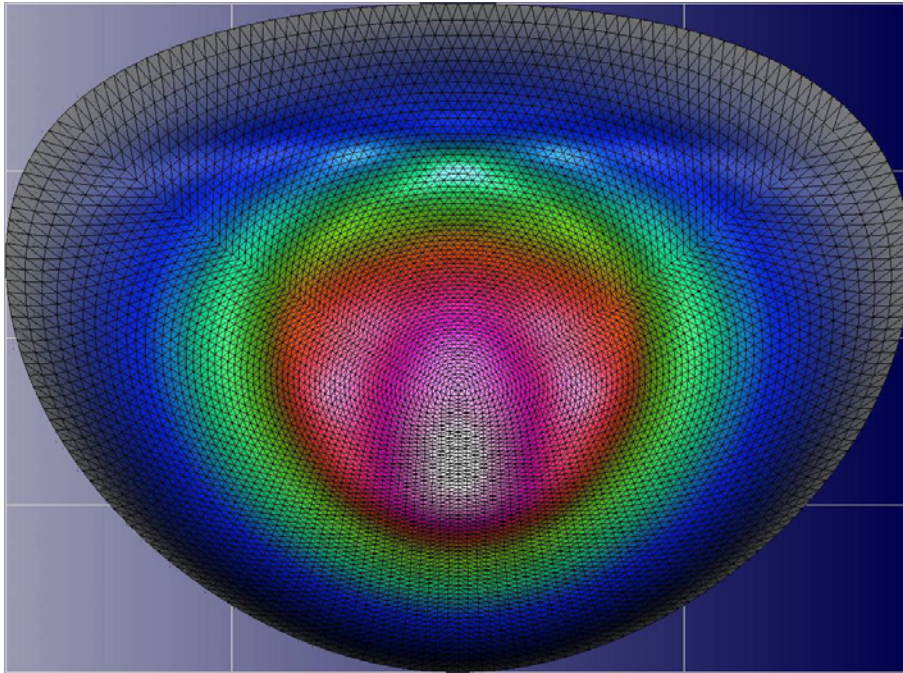
In order to resolve fine structures at a particular surface, the option exists to concentrate zones of the M3D mesh about a given minor radius (1D packing).

Command line options:

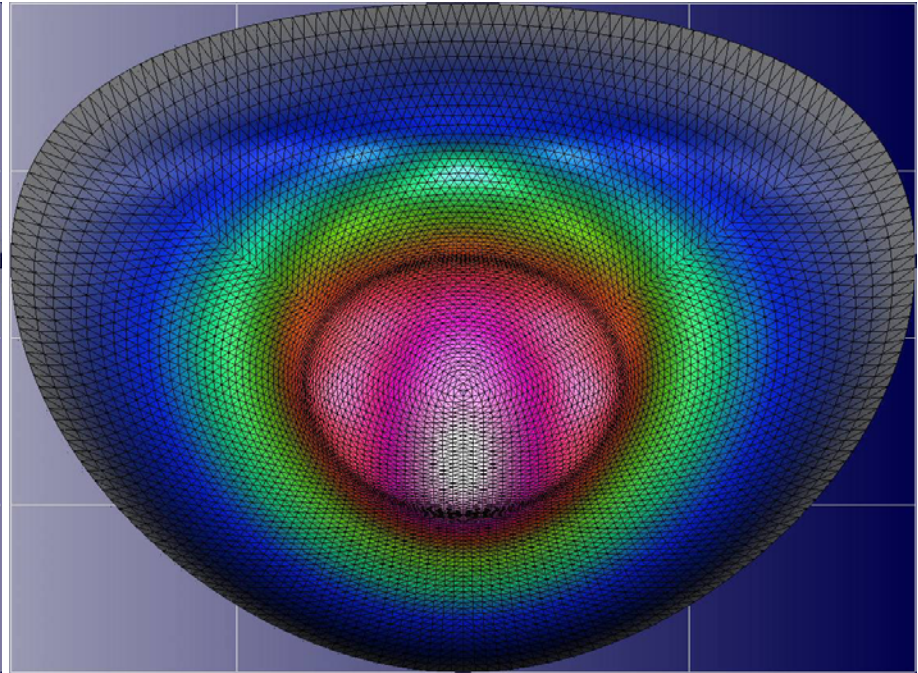
- packingFactor <pf> *Ratio of packed to unpacked mesh density.*
- packingRadius < x_0 > *Relative position of packing surface (from 0 to 1).*
- packingWidth <w> *Relative width of peak packing area (on 0 to 1 scale).*

Example: $pf=4.0$; $x_0=0.5$; $w=0.12$:

Before packing

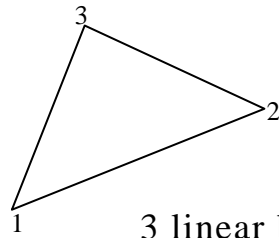


After packing



Linear Finite Elements

Linear basis functions on a triangle:



Side lengths $d\vec{r}_1 \equiv \vec{r}_2 - \vec{r}_3$, etc.

$$\text{Area } \Delta = \frac{1}{2} d\vec{r}_1 \times d\vec{r}_2 \cdot \hat{\phi}$$

3 linear basis functions $\lambda_\alpha(\vec{r}) = \frac{1}{4\Delta} \sum_{\beta \neq \alpha} (\vec{r} - \vec{r}_\beta) \times d\vec{r}_\alpha \cdot \hat{\phi}$

$$\lambda_\alpha(\vec{r}_\alpha) = 1; \lambda_\alpha(\vec{r}_{\beta \neq \alpha}) = 0$$

Galerkin method: integrate equations over each basis function to get “weak form” → linear algebraic equation.

$$f(R, z) = \sum_j f_j \lambda_j(R, z)$$

Mass matrix: $\iint \lambda_i f(R, z) d^2x = \sum_j f_j \iint \lambda_i \lambda_j d^2x \equiv \sum_j M_{i,j} f_j$

Stiffness matrix: $\iint \lambda_i \nabla_\perp^2 f(R, z) d^2x = \sum_j f_j \iint \lambda_i \nabla_\perp^2 \lambda_j d^2x = \sum_j f_j \left\{ \iint \nabla_\perp \cdot (\lambda_i \nabla \lambda_j) d^2x - \iint \nabla_\perp \lambda_i \cdot \nabla_\perp \lambda_j d^2x \right\} \equiv \sum_j S_{i,j} f_j$

"dRoverR" matrix: $\iint \frac{\lambda_i}{R} \frac{\partial}{\partial R} f(R, z) d^2x = \sum_j f_j \iint \frac{\lambda_i}{R} \frac{\partial \lambda_j}{\partial R} d^2x \equiv \sum_j R_{i,j} f_j$

Handy identity: $\iint_\Delta \lambda_1^\ell \lambda_2^m \lambda_3^n d^2x = 2\Delta \frac{\ell! m! n!}{(\ell + m + n + 2)!}$

Lumped mass matrix (diagonal): $\bar{M}_{i,j} \equiv \delta_{i,j} \sum_j M_{i,j}$

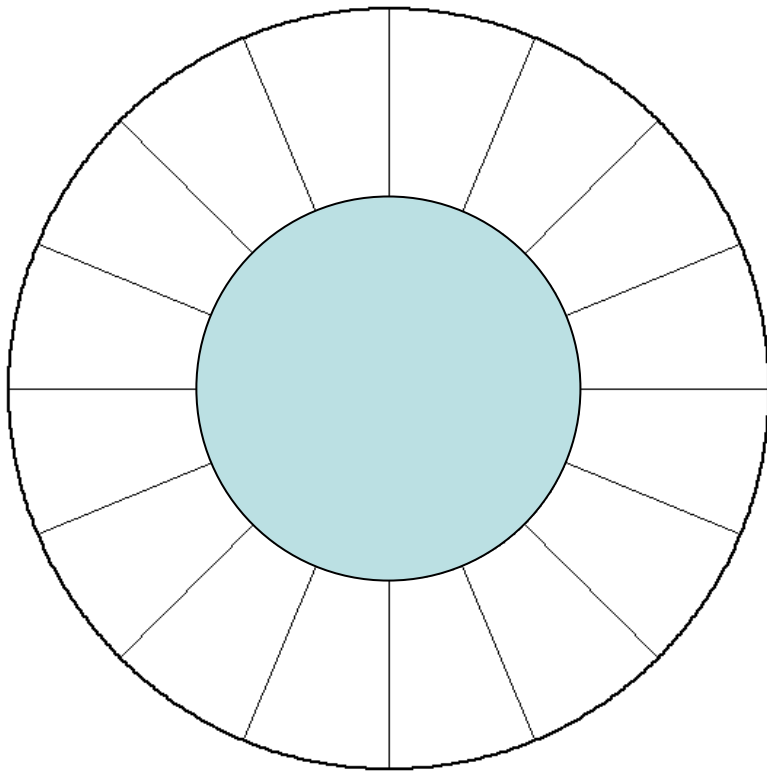
Boundary Conditions

- All calculations use a fixed boundary.
- Standard cases use perfectly conducting wall, with or without a “slot”.
- Slip or no-slip conditions may be imposed.
- Most of these are realized as Dirichlet b.c.s in linear solves. Exceptions: F , χ use Neumann.

Domain Decomposition

3 parameters control domain decomposition: # of toroidal PEs, # of radial PEs, # of theta PEs.

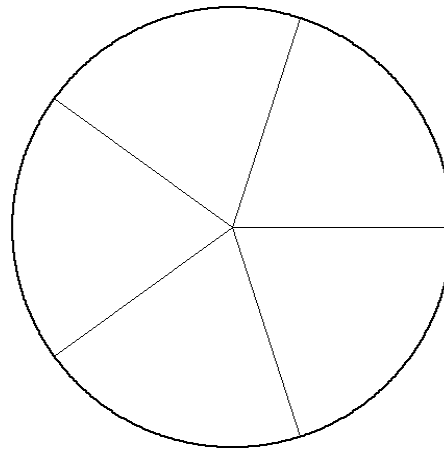
Toroidal
(overhead view)



$B = 16$

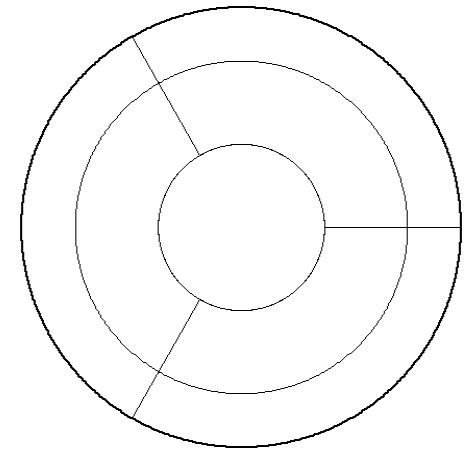
Linear solves are independent on each processor

Poloidal
(cross-section view)



$D = 1$
 $F = 5$

or



$D = 3$
 $F = 3$

Linear solves are parallel over processors

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Time Discretization, Overview

- Equations (1-6) are advanced explicitly, except for parabolic and fast wave terms.
- Time discretization is typically 1st order, forward-in-time. 2nd-order predictor-corrector is also an option.
- Artificial sound term, if selected, is advanced in subcycles of the main time step.
- **Code execution time is dominated by ~13 linear solves per time step**, each of size N , where N is the number of vertices in a single plane.
 - Elliptic solves are more expensive than Helmholtz.
 - Neumann b.c.s are more expensive than Dirichlet.

Schematic of Equation Solve

Generic mixed hyperbolic/parabolic equation:

$$\frac{\partial f}{\partial t} + u \frac{\partial f}{\partial x} = D \frac{\partial^2 f}{\partial x^2}$$

Galerkin F.E. method

1. Explicit solve: $f^* = f^n - (\delta t) u^n \left(\frac{\partial f}{\partial x} \right)^n$

2. Implicit solve:

$$\left[\frac{\partial^2}{\partial x^2} - \frac{1}{D\delta t} \right] (f^{n+1} - f_{source}) = - \frac{(f^* - f_{source})}{D\delta t}$$

Order of Operations in Main Loop

1. Recompute dt based on CFL condition for shear Alfvén wave.
2. Adjust resistivity profile to track temperature.
3. Compute $I = \varepsilon + \tilde{I}$, B^2
4. Advance particles if hybrid option is on.
5. Solve (2a) for vorticity $w = \Delta^\dagger U$; ideal terms explicitly, followed by implicit solve for viscous term and elliptic solve for U .
6. Simultaneously solve (5) for toroidal field, (2b-c) for $\nabla_\perp \chi$, and ideal part of (6) for pressure or temperature implicitly (in-plane) to step over fast wave time scale. Integrate to solve for χ . Many terms are still explicit; resistivity, viscosity and heat diffusion are still implicit, perpendicular to $\nabla\phi$.
7. Apply perpendicular (or isothermal) heat conduction.
8. Advance (1) for density ρ .
9. Advance artificial sound wave.
10. Advance (2d) for toroidal velocity.
11. Solve elliptic equation (3) for electrostatic potential.
12. Solve (4) for ψ or $\Delta^*(4)$ for C_a followed by an elliptic solve for ψ .
13. Solve elliptic equation for F .
14. Diagnostics, output, checkpointing.

Artificial Sound Wave Substep

$$\frac{\partial T}{\partial t} = s \frac{\mathbf{B} \cdot \nabla u}{\rho}$$

$$\frac{\partial u}{\partial t} = s \mathbf{B} \cdot \nabla T + \nu \nabla^2 u$$

Repeat `napmax` times:

- Solve T equation with reduced time step `rdtdp` explicitly.
- Solve hyperbolic part of u equation explicitly.
- Solve parabolic part of u equation implicitly.
- Check stability.

Linear vs. Nonlinear

By default, the time advance is fully nonlinear. However an option exists to search for linear toroidal eigenmodes.

- Begin by adding a perturbation with toroidal mode $#n$ to velocity variable U in equilibrium.
- With pseudospectral method, only three planes are needed to resolve the mode. (Use number of field periods = n).
- After each nonlinear advance of a variable, find the mode n component, add to the $n=0$ component from the original equilibrium to get advanced-time value.
- Fastest-growing mode will eventually dominate over others; growth rate determined from rate of change of total kinetic energy.
- Rescale perturbed quantities periodically to keep total kinetic energy below nonlinear level but above noise.

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PETSc

- Portable, Extensible Toolkit for Scientific Computation.
 - MPI-based suite of data structures & routines for parallel solution of PDEs.
 - Maintained by PETSc group, Mathematics and Computer Science Division, Argonne National Lab.
 - Latest version is 2.3.2.
- The MPI version of M3D is highly dependent on PETSc.
 - Uses versions 2.1.6, 2.3.0.
 - Parallel data structures, ghost exchanges
 - Vectors (variable fields)
 - Matrices (linear operators)
 - Linear solves – great flexibility in solver choices
 - Asymmetric operators: GMRES
 - Symmetric operators: CG
 - Direct solves (SuperLU), Multigrid
 - Most of M3D computation occurs in PETSc solves, so we rely on PETSc optimization for performance, scalability.

HDF5

- Hierarchical Data Format
 - Widely adopted and supported portable binary format
 - Allows self-describing data organized in file-system-like hierarchies.
 - Random access
- **M3D uses HDF5 as its primary output option.**
 - A subset of the fields in the checkpoint (12 scalar, 1 vector) is written every several time steps, in single precision.
 - Mesh is described as a set of triangular prisms.
 - Data values are given at vertices.
 - Checkpoint files can also be converted between native binary and HDF5 for intersystem portability.
 - UCD (text) output is another option; the OpenMP version can also produce NCAR graphics.

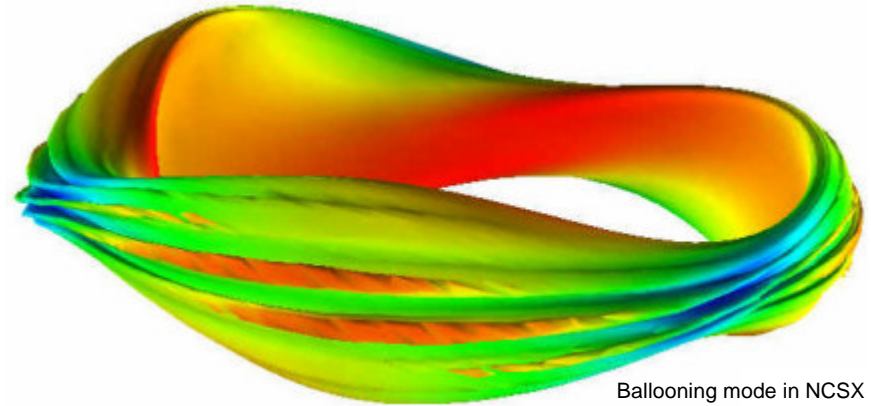
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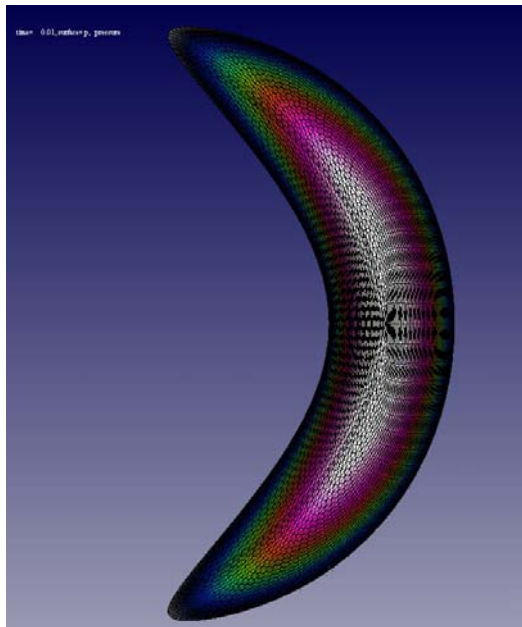
Stellarator

(H. Strauss)

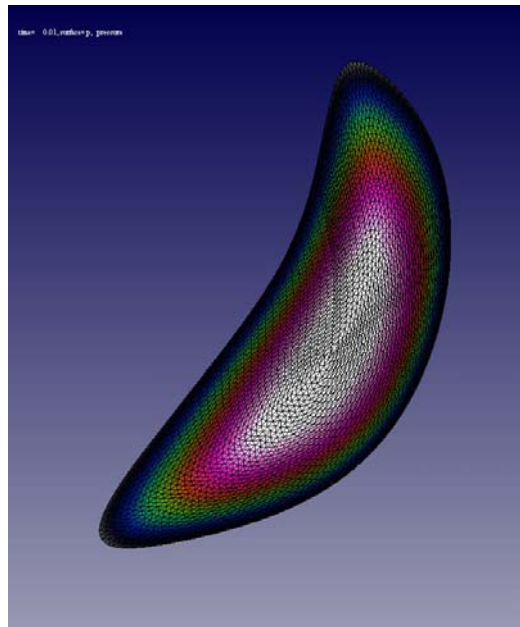
- By generating a mesh from a 3D equilibrium file, M3D can run stellarator cases.
- Planes can be made to span just one field period.
- Toroidal derivatives require extra terms for toroidal mesh variation, impacting speed and accuracy.



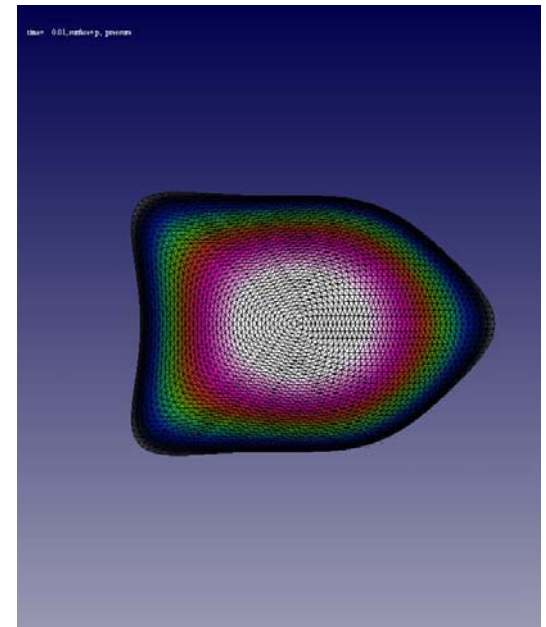
Ballooning mode in NCSX



$\varphi = 0$



$\varphi = \pi/6$



$\varphi = \pi/3$

Two Fluid

(L. Sugiyama)

- A hierarchy of extended MHD models exists in M3D.
- The simplest uses the drift ordering to approximate the ion gyroviscous stress tensor term in the momentum equation ($-\nabla \cdot \Pi_i^{gv}$) using the diamagnetic drift velocity:

$$\rho \left[\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} + (\mathbf{v}_i^* \cdot \nabla) \mathbf{v}_\perp \right] = -\nabla (\mathbf{p}_e + \mathbf{p}_i) + \mathbf{J} \times \mathbf{B} + \mu \nabla^2 \mathbf{v}$$

$$\mathbf{v}_i^* \equiv \mathbf{v}_e^* + \frac{\mathbf{J}_\perp}{ne}, \quad \mathbf{v}_e^* \equiv -\frac{\mathbf{B} \times \nabla p_e}{neB^2}, \quad \mathbf{v} \equiv \mathbf{v}_i - \mathbf{v}_i^* = \mathbf{v}_e - \mathbf{v}_e^* + \frac{\mathbf{J}_\parallel}{ne}$$

- The Hall term can also be added to Ohm's law, introducing the dispersive whistler wave, which is very difficult to stabilize.

Hybrid (Kinetic Hot Ions)

(G. Fu)

- Gyrokinetic particle push based on GTC group's formulation.
- Large ensemble of ions substepped through interpolated M3D \mathbf{B} field.
- Hot ions couple back to fluid model through pressure tensor:

$$\rho \frac{d\mathbf{v}}{dt} + \rho (\mathbf{v}_i^* \cdot \nabla) \mathbf{v}_\perp = -\nabla P - \nabla \cdot \mathbf{P}_h + \mathbf{J} \times \mathbf{B} - \mathbf{b}\mathbf{b} \cdot \nabla \cdot \Pi_i$$

where $\mathbf{P}_h = P_\perp \mathbf{I} + (P_\parallel - P_\perp) \mathbf{b}\mathbf{b}$

based on moments taken over the particle distribution function

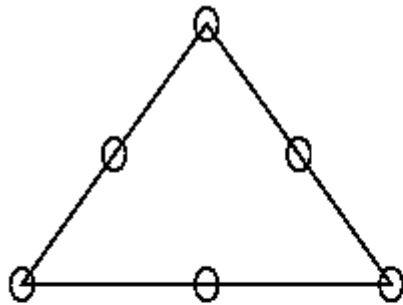
$$f = \sum_i \delta(\mathbf{R} - \mathbf{R}_i) \delta(v_\parallel - v_{\parallel,i}) \delta(\mu - \mu_i)$$

- MPI Parallelization follows domain decomposition of M3D mesh; particles can move between processors.
- Typical particle push time is comparable to fluid advance time.
- Fully kinetic ion model (with fluid electrons) also exists.

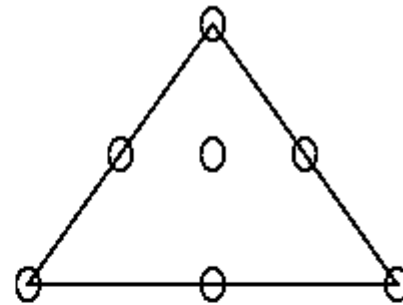
Higher-Order Elements

(H. Strauss, J. Chen)

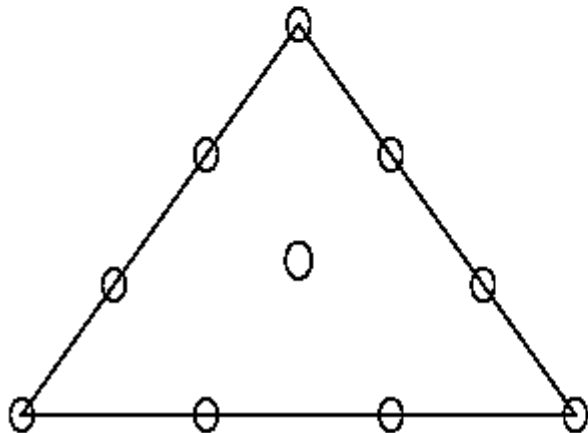
- 2nd and 3rd-order polynomial elements are available.
- Formed by adding nodes to existing mesh triangles.
- In “lumped” elements, nodes are placed at quadrature points of integral, resulting in a diagonal mass matrix for much faster evaluation, at a cost of more vertices.



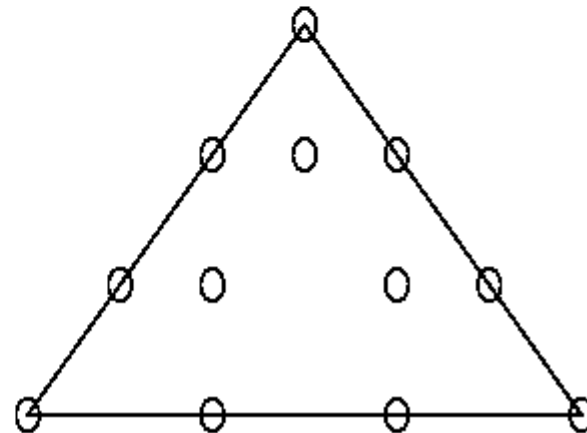
2nd-order Lagrange



2nd-order lumped



3rd-order Lagrange

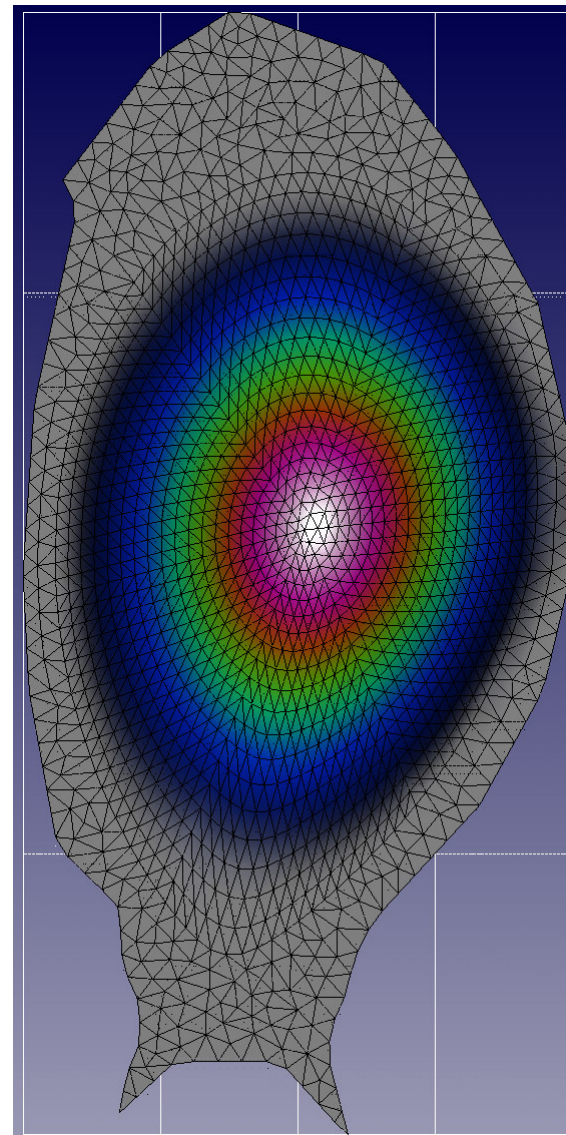


3rd-order lumped

Resistive Wall

(H. Strauss, J. Breslau)

- OpenMP code uses external package to generate vacuum-region mesh extending M3D mesh out to wall.
- Mesh may exclude axis region (not shown) with internal boundary condition.
- MPI version can initialize from mesh+data file generated by OMP version.
- Vacuum region treated as low density, low temperature (high η) plasma.
- Boundary conditions on fields at wall are applied using Green's functions precomputed by GRIN for each toroidal mode based on boundary geometry.



VDE in ASDEX (early time).

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Concluding Thoughts

- The proliferation of new physics modules, options, and numerical techniques has made M3D very versatile and flexible but also very complex and challenging to maintain.
- A set of thorough standard tests for validation is badly needed.
- The code has been very productive on present machines, producing results few other MHD codes are capable of.
- But it could be a lot more efficient, and scaling up usefully to petascale runs remains a formidable hurdle.
 - Need more implicitness.
 - Need higher order elements.
 - Need efficient, scalable solvers.