

Modeling Three Dimensional Equilibria and ELM Suppression in DIII-D

by
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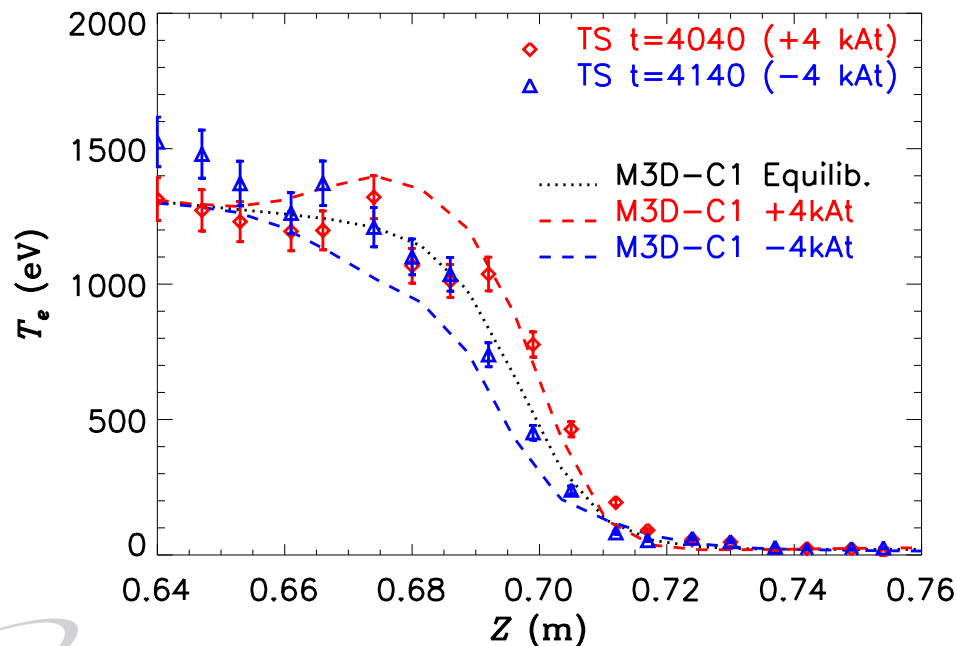
Outline

- **Modeling 3D equilibria**
 - Validation of linear M3D-C1 calculations
 - Nonlinear M3D-C1 calculations
 - Code comparisons
- **Developing and validating ELM suppression criteria**
- **Obtaining a predictive model for ELM suppression**

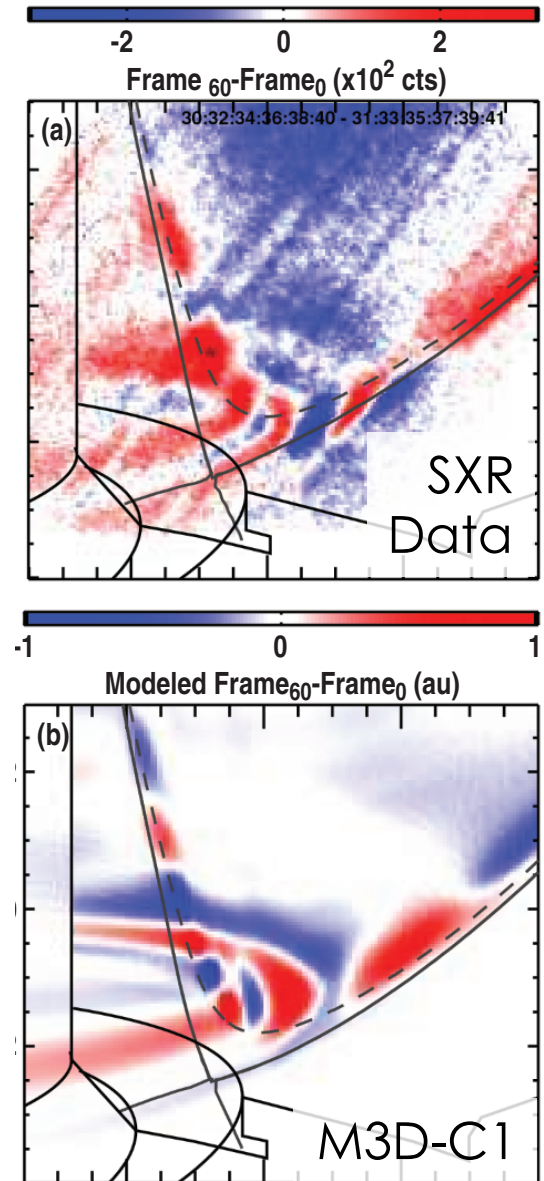
Modeling 3D Equilibria

Linear Calculations of Plasma Response Agree With Experimental Measurements of Profile Displacements

- Changing the phase of applied 3D fields “displaces” the temperature and density profiles up to ~4 cm on DIII-D
- Linear M3D-C1 calculations show helical distortions that agree well with observed displacements
 - Two-fluid effects and rotation affect agreement

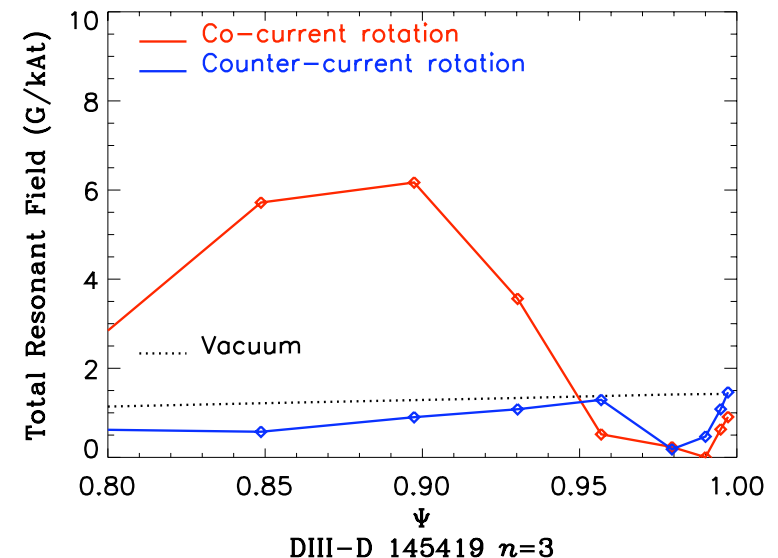
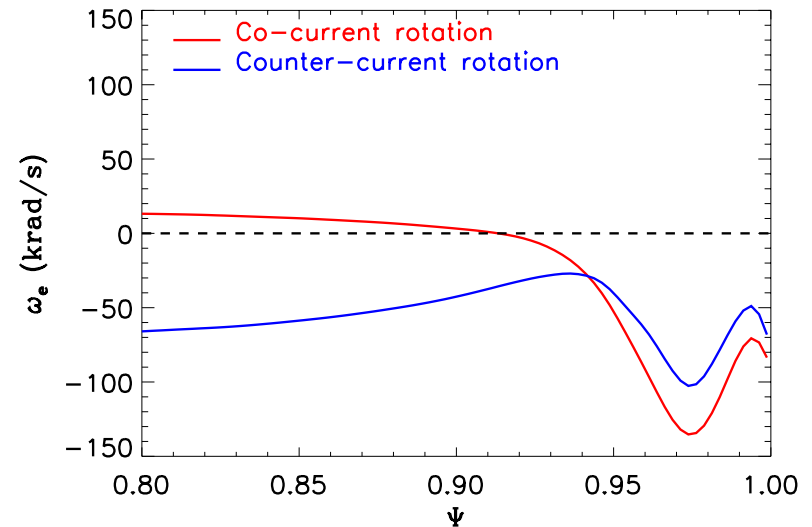


DIII-D 148712 $n=3$
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Plasma Response Calculations Predict Island Formation at Pedestal Top When Rotation is Co-Current

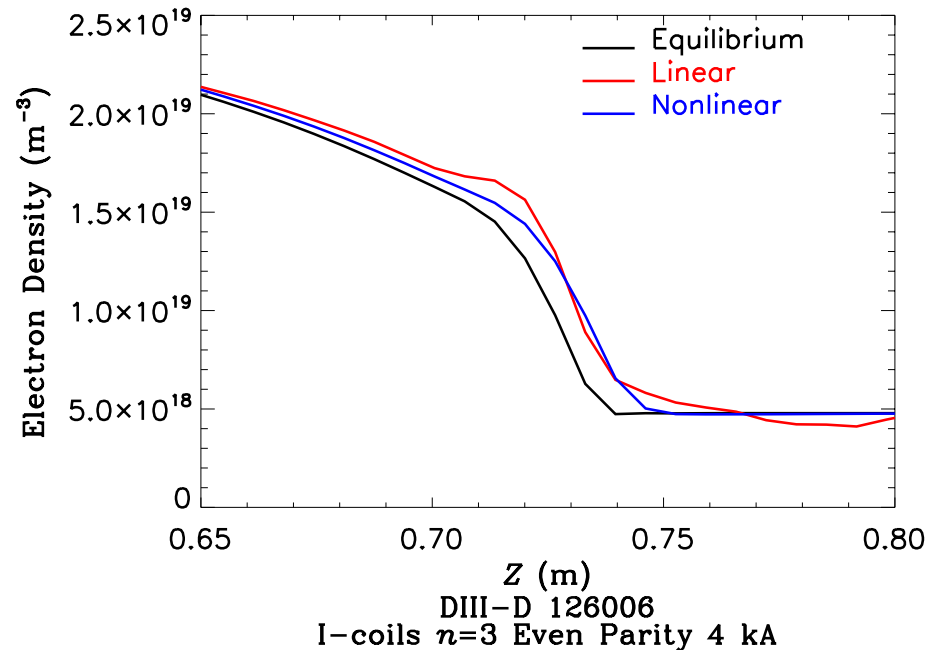
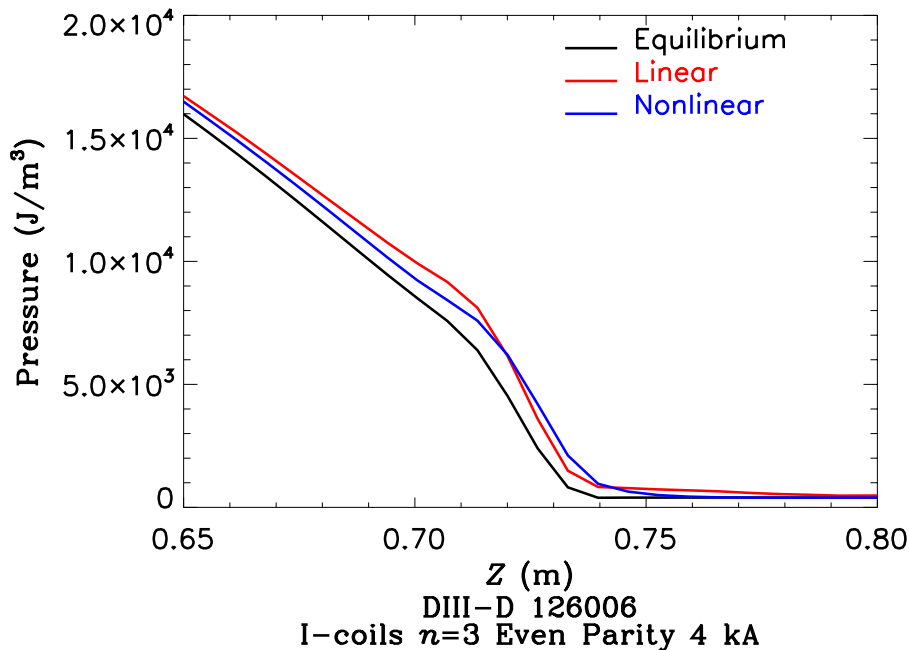
- Perpendicular electron rotation screens islands ($\omega_e = \omega_{\text{ExB}} + \omega_{*e}$)
- Diamagnetic term \rightarrow edge screening, reduced pedestal stochasticity
- In co-current rotating plasmas, $\omega_e = 0$ near top of pedestal
 - Islands can penetrate and be amplified here
- In counter-current rotation plasmas, ω_e never crosses zero
- Is this a mechanism for suppressing ELMs by limiting the pedestal?
 - Consistent with lack of counter-current ELM suppression



DIII-D 145419 $n=3$

Linear and Nonlinear Calculations of Displacement are in Reasonable Agreement for 126006 at 4kA n=3

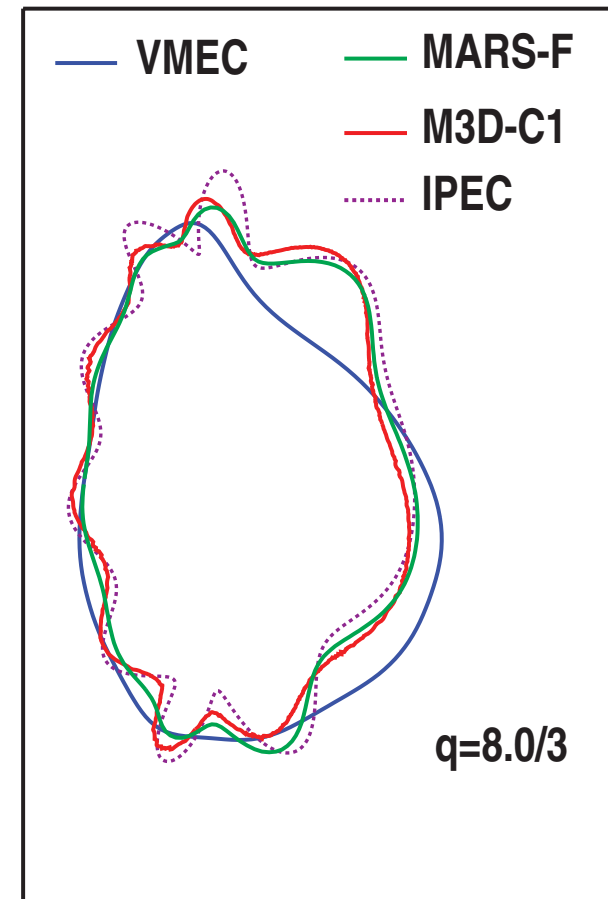
- Nonlinear, one-fluid calculations with Spitzer resistivity and realistic dissipation ($\sim 5 \text{ m}^2/\text{s}$) have been carried out
- Displacements are similar to linear results, in this case



- $|d\xi/dr|$ never exceeds ~ 0.3 in this case, so we expect the linear result to be valid

2012 Theory Milestone Compared 3D Equilibrium Calculations From IPEC, MARS, M3D-C1, and VMEC

- VMEC results were qualitatively different from results of linear codes (IPEC, MARS, M3D-C1)
- Nonlinear M3D-C1 calculations agreed well with linear M3D-C1 calculations (although linear validity was questionable at edge)
- VMEC was found to converge very slowly to analytic result in circular, large aspect-ratio test case as radial resolution was increased (S. Lazerson)
- My conclusion: VMEC struggles to resolve resonant currents in perturbed tokamaks



Turnbull, *et al.* Submitted to *Phys. Plasmas*

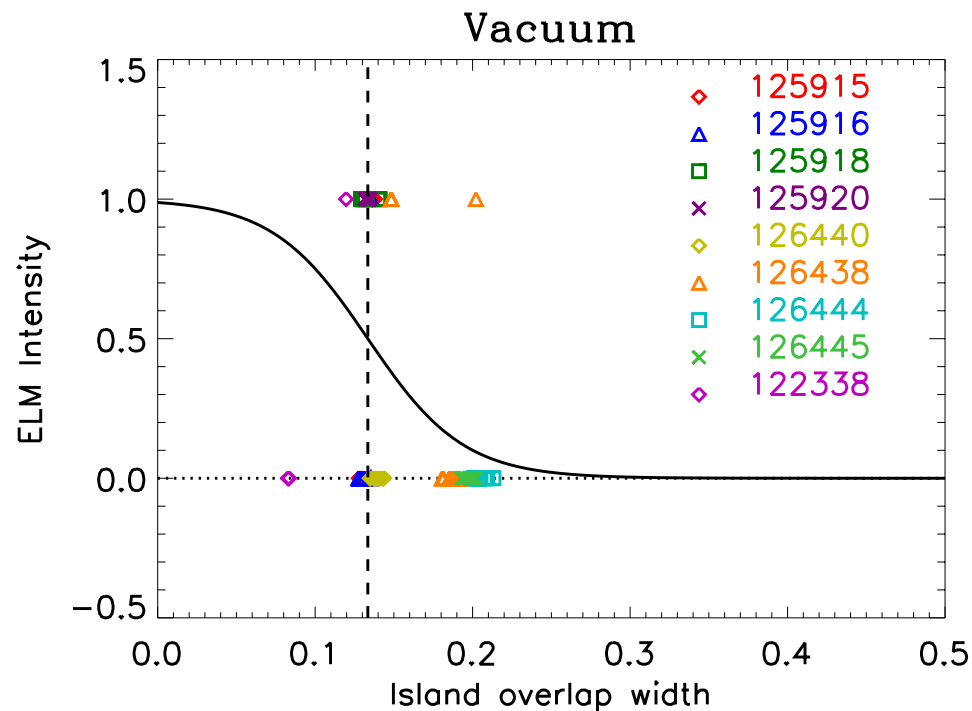
Developing and Validating ELM Suppression Criteria

ELM Suppression Criteria Are Tested on DIII-D Discharges Taking Plasma Response Into Account

- **“Island Overlap Width” criterion was found to correlate with RMP ELM Suppression**
 - Considered only the “vacuum” fields
 - Predicted level of stochasticity is
 - *This metric was not intended to describe the actual physical situation, but rather to find a characteristic of the coil spectrum that correlates with ELM suppression*
- **To develop a better ELM suppression criterion:**
 - Take into account the plasma response
 - Explore metrics related to our ELM suppression hypothesis
- **We can evaluate various criteria on a database of discharges with RMP applied (some are ELM suppressed, others aren't)**

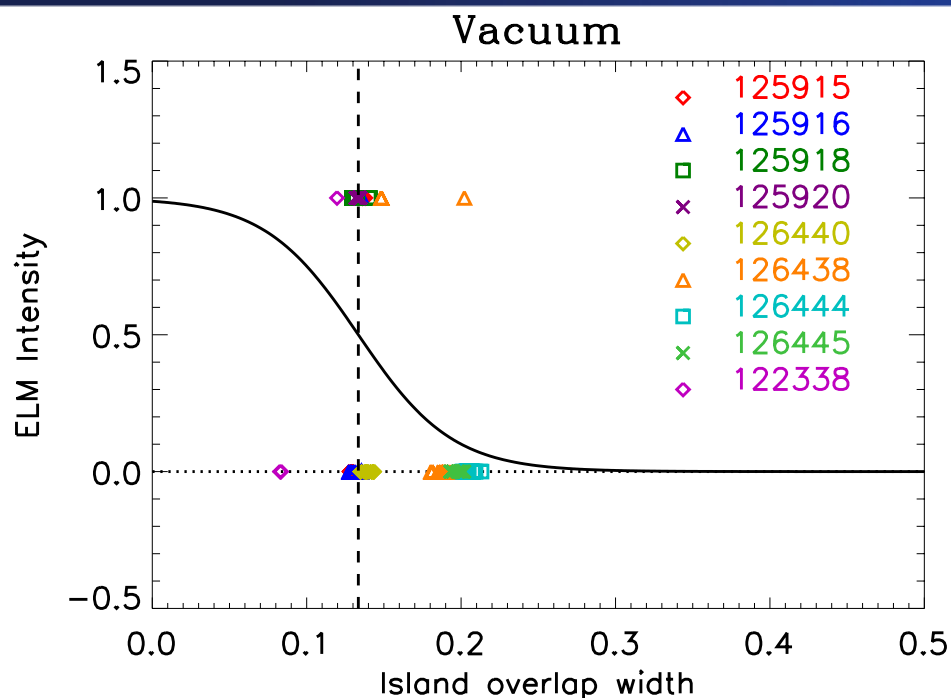
Features of Plasma Response Are Correlated With ELM Suppression For a Set of DIII-D Discharges

- For each discharge/timeslice, an axisymmetric equilibrium is reconstructed with EFIT
- **ELM Intensity** at each timeslice
 - 1 if plasma was ELMing
 - 0 if plasma was suppressed
- Each criterion is evaluated by tanh fit to ELM intensity
- **Threshold** = center of tanh fit
- **Accuracy** =
$$\frac{\text{\# of correctly classified timeslices}}{\text{\# of timeslices}}$$



Vacuum island overlap width
 Threshold = 0.133 (Ψ_N)
 Accuracy = 60%

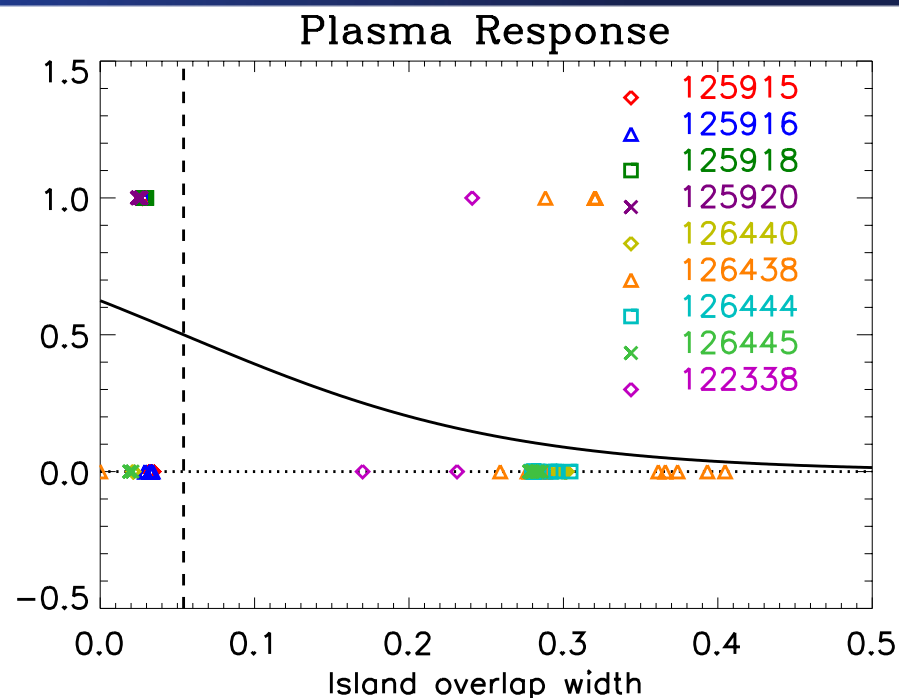
Island Overlap Criterion is Improved by Including Plasma Response



Vacuum island overlap width

Threshold = 0.133 (Ψ_N)

Accuracy = 60%



Plasma island overlap width

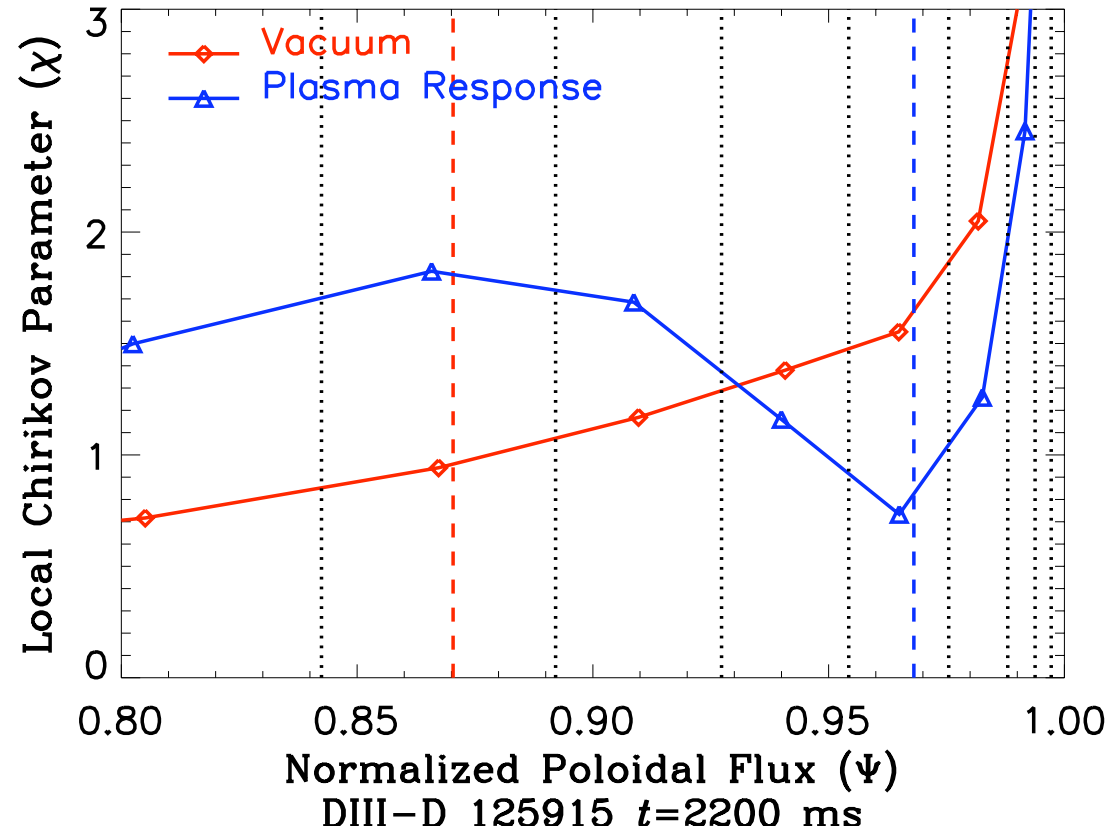
Threshold = 0.059 (Ψ_N)

Accuracy = 72.6%

- Plasma response reduces island overlap width threshold
- This criterion yields many false negatives (ELM suppressed despite not meeting threshold)

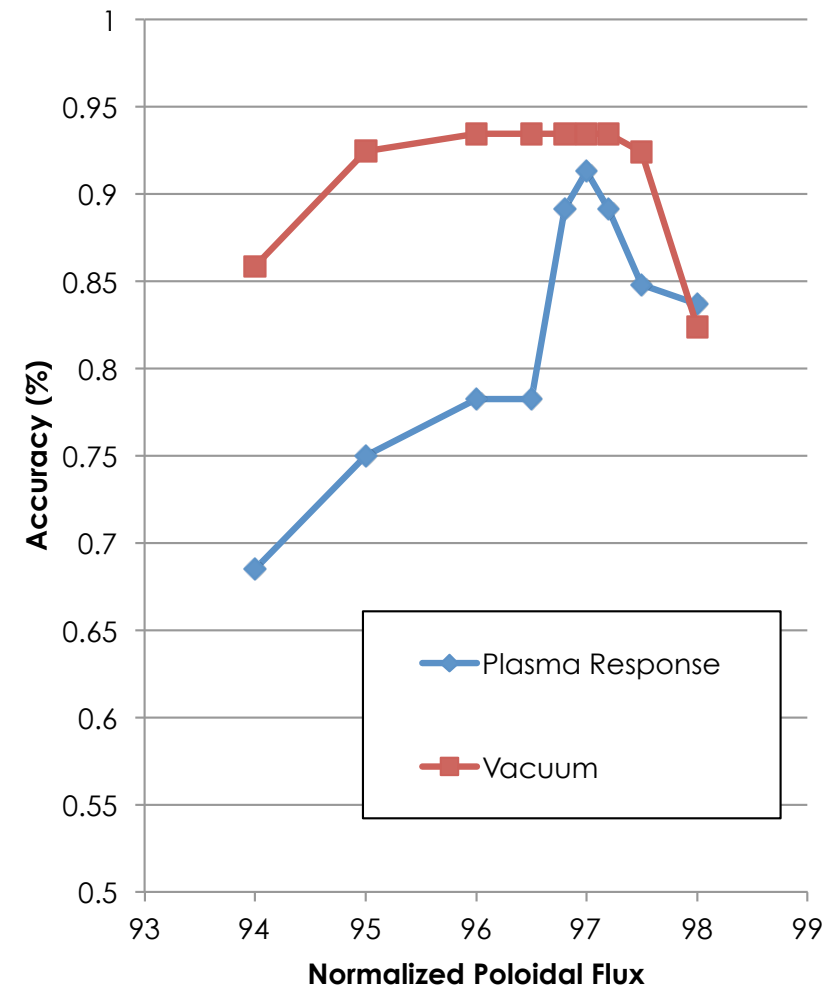
Local Chirikov Parameter $\chi(\Psi)$ Characterizes Local Stochasticity

- Island Overlap Width requires stochasticity across entire pedestal
- “Local Chirikov Parameter” evaluates stochasticity at particular location
- Chirikov parameter (symbols) is evaluated for each pair of adjacent rational surfaces (dotted lines)
- $\chi(\Psi)$ (solid lines) is defined by linear interpolation of Chirikov parameters

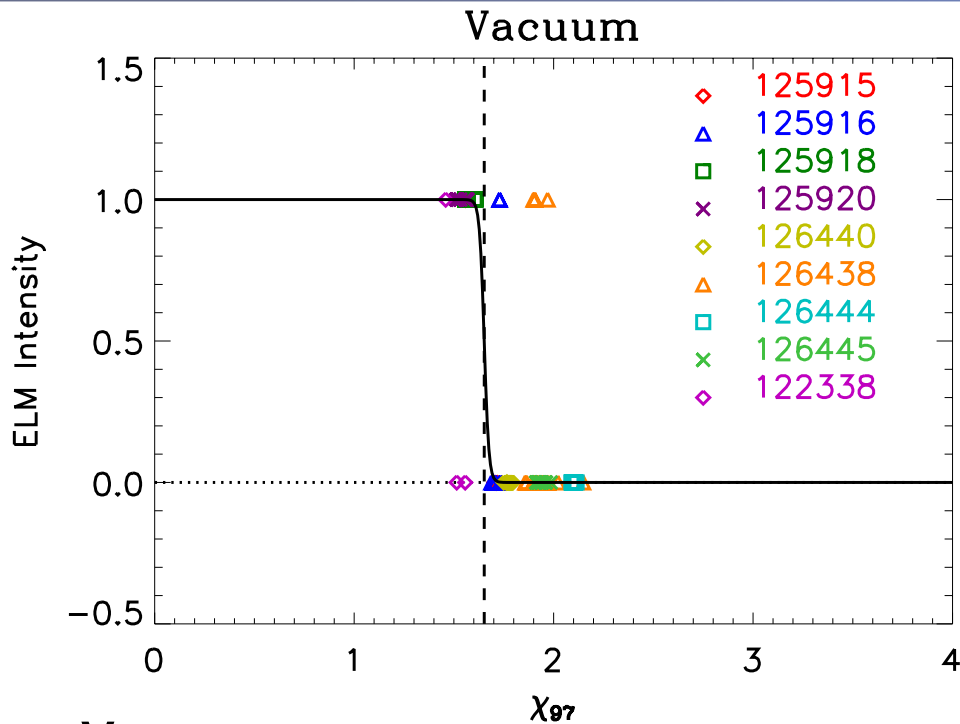


χ_{97} : Correlation of $\chi(\Psi)$ with ELM Suppression is Best at $\Psi=0.97$

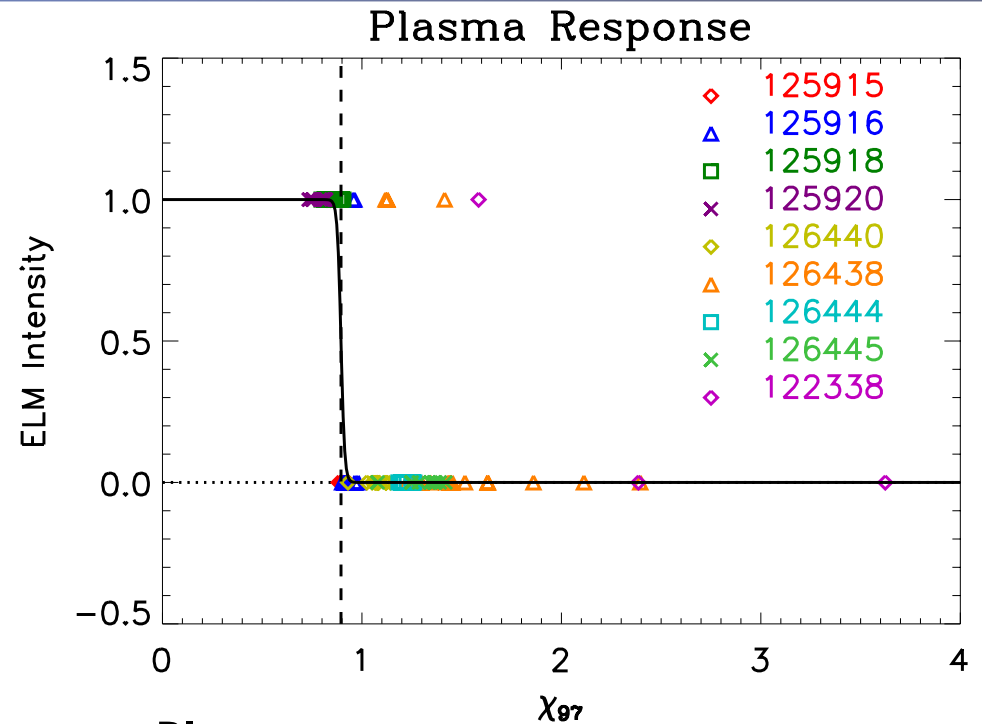
- $\chi(\Psi)$ with plasma response has sharp increase in accuracy near $\Psi=0.97$
- $\chi(\Psi)$ without plasma response is actually more accurate than with plasma response
 - Vacuum calculation is more robust
 - Little variation with Ψ
- $\chi(\Psi=0.97)$ is much more accurate than island overlap width



ELM Suppression More Strongly Correlates With χ_{97} Than With Island Overlap Width

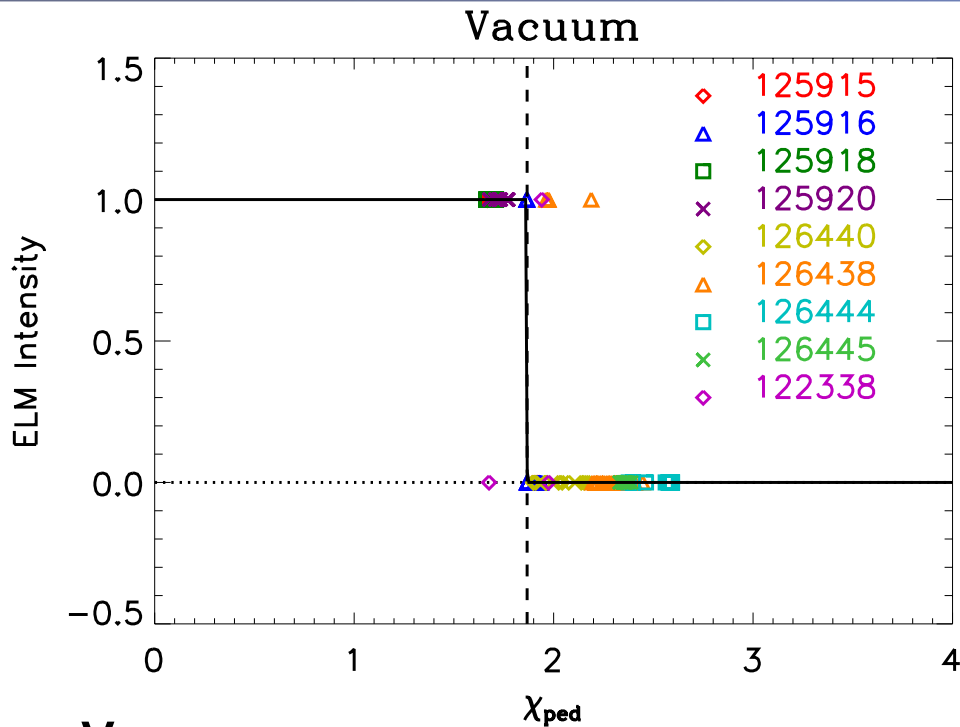


Vacuum χ_{97}
 Threshold = 1.65
 Accuracy = 93.5%

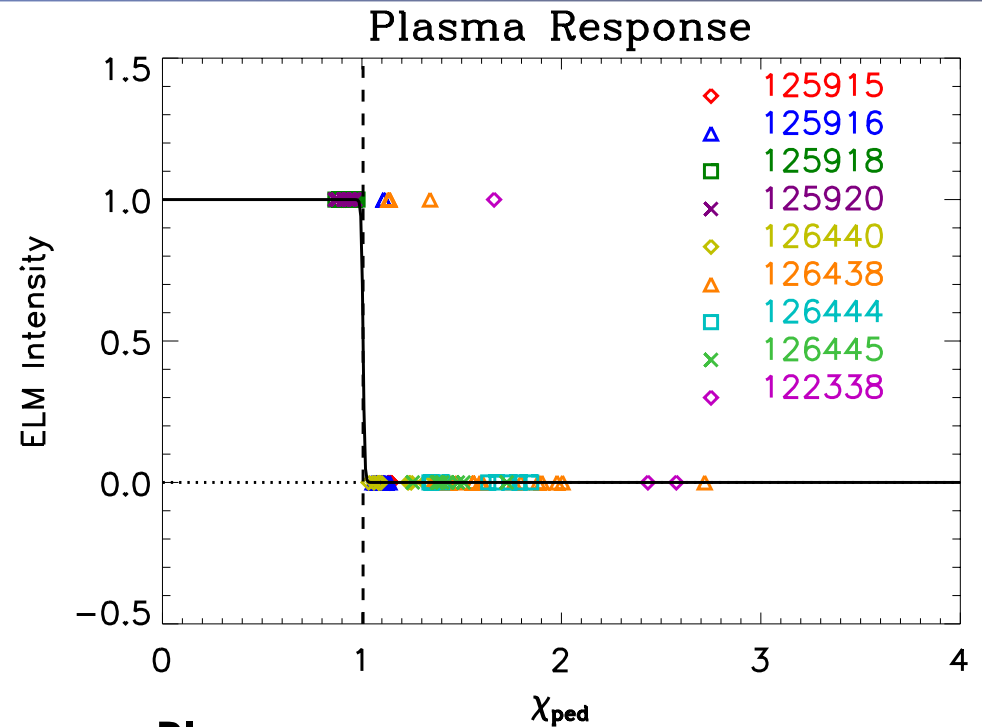


Plasma χ_{97}
 Threshold = 0.895
 Accuracy = 91.3%

χ_{ped} : Local Chirikov Parameter is Further Improved By Evaluating χ at Pedestal Top



Vacuum χ_{ped}
 Threshold = 1.867
 Accuracy = 91.6%

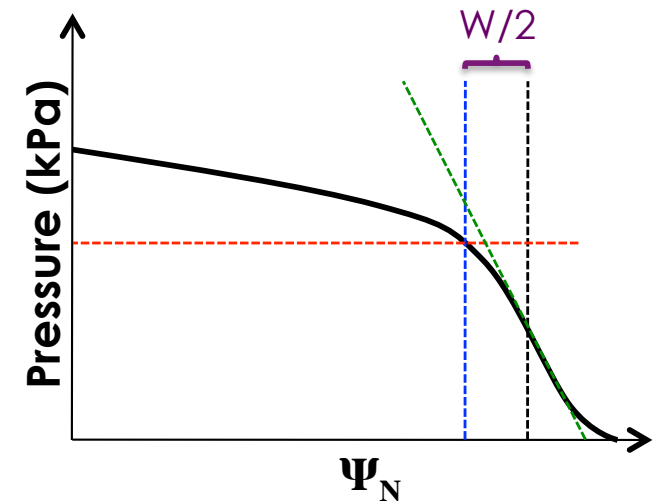


Plasma χ_{ped}
 Threshold = 1.01
 Accuracy = 92.6%

- Choosing “ Ψ =pedestal top” replaces arbitrary $\Psi=0.97$
- Accuracy of χ_{ped} with plasma response exceeds $\chi(\Psi)$ for any fixed Ψ

ELM Suppression Correlates Best With Position of Pedestal Center

	Threshold	Accuracy
Pedestal Gradient	$> 1,305 \text{ kPa}/\Psi_N$	66.3%
Pedestal Height	$> 38.4 \text{ kPa}$	68.4%
Pedestal Width	$> 0.0201 \Psi_N$	77.9%
Pedestal Top	$< 0.966 \Psi_N$	91.5%
Pedestal Center	$< 0.976 \Psi_N$	95.8%



- These are purely measures of the axisymmetric equilibrium
- Correlation with “Pedestal Center” is not a physically intuitive result
 - Pedestal width, height, or gradient would seem more natural
- ***A predictive model of ELM suppression must be able to predict the response of the axisymmetric pedestal profiles to 3D fields***

Obtaining a Predictive Model of ELM Suppression

Ultimate Goal Is To Understand RMP ELM Suppression

- **Need to know:**
 - Will coils suppress ELMs?
 - What is the associated loss of confinement?
 - What are the resulting heat/particle fluxes to the walls?
- **This will require:**
 - Calculating 3D MHD response
 - Calculating 2D transport response
 - (Maybe) calculating 3D peeling-ballooning stability
- **Efforts to calculate transport in 3D fields are underway**
 - Gyrokinetics (GENE)
 - Fast ion transport (SPIRAL)
 - Ballooning mode stability (T. Bird)
- **Maybe 3D effects on turbulence can be integrated into EPED**

Summary

- **Good progress on calculating 3D MHD response**
 - Various codes in relatively good agreement (except VMEC)
 - Quantitative agreement with experimental results
 - Linear response may be sufficient for some aspects of plasma response
 - Single-fluid nonlinear calculations with realistic parameters are feasible
- **We have obtained criteria that correlate with ELM suppression better than island overlap width does**
 - Fact that best correlation is with pedestal position implies that understanding transport in 3D is necessary for predictive model of ELM suppression

Extra Slides

M3D-C1 Solves Two-Fluid Equations

$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{u}) = 0$$

$$n_i m_i \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = \mathbf{J} \times \mathbf{B} - \nabla p - \nabla \cdot \Pi$$

$$\begin{aligned} \frac{\partial p}{\partial t} + \mathbf{u} \cdot \nabla p = & -\Gamma p \nabla \cdot \mathbf{u} - \frac{1}{n_e e} \mathbf{J} \cdot \left(\Gamma p_e \frac{\nabla n_e}{n_e} - \nabla p_e \right) \\ & + (\Gamma - 1) (\eta J^2 - \Pi : \nabla \mathbf{u} - \nabla \cdot \mathbf{q}) \end{aligned}$$

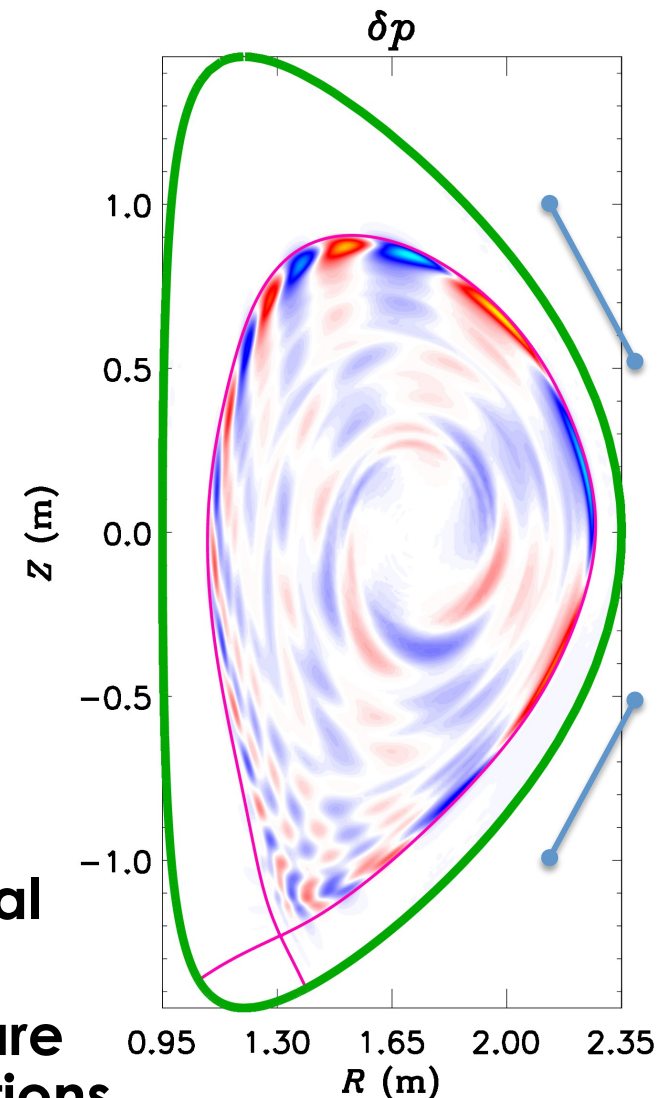
$$\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times \left[-\mathbf{u} \times \mathbf{B} + \eta \mathbf{J} + \frac{1}{n_e e} (\mathbf{J} \times \mathbf{B} - \nabla p_e) \right]$$

$$\mathbf{J} = \nabla \times \mathbf{B}$$

$$\Pi = -\mu \left[\nabla \mathbf{u} + (\nabla \mathbf{u})^T \right]$$

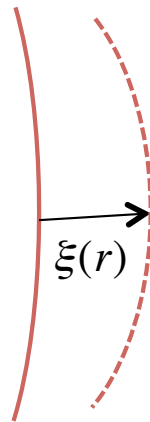
$$\mathbf{q} = -\kappa \nabla (T_e + T_i) - \kappa_{\parallel} \mathbf{b} \mathbf{b} \cdot \nabla T_e$$

- **Boundary conditions: normal B from external coils is held constant at boundary**
- **Here, linear, time-independent equations are solved directly, subject to boundary conditions**



The Validity of Linear Temperature Response Can Be Quantified

- “Displacement” may be defined by movement of isotherms:



$$T_0(r + \xi) + \delta T(r + \xi) = T_0(r)$$

$$\left[T_0(r) + \frac{dT_0}{dr} \xi \right] + \delta T(r) = T_0(r)$$

$$\xi = -\frac{\delta T}{dT_0/dr}$$

Criterion for validity of linear temperature response

- Overlap of adjacent isotherms is implied unless

$$\left| \frac{d\xi}{dr} \right| < 1$$

- In ideal MHD, violating this criterion implies that perturbed surfaces are no longer well described by ξ
- In M3D-C1, violating this criterion implies breakdown of linear approximation to $\mathbf{B} \cdot \nabla T = 0$

Linear Validity of Temperature Response Is Often Violated in the Pedestal for Typical DIII-D Cases

- For typical DIII-D parameters, linear validity is often exceeded in the pedestal region and near mode-rational surfaces
- Validity may also be exceeded near mode-rational surfaces
- Magnetic response is likely valid nearly everywhere since $\delta B/B$ is always small
 - Exception may be resonant field components

