## The Ion Temperature Gradient (ITG) Instability

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- Intuitive picture of the ITG instability

   based on analogy with
   Inverted pendulum / Rayleigh-Taylor
   instability
- 2. Rigorous derivation of ITG growth rate & threshold (in a simple limit) starting from the Gyrokinetic Eq.

(with sign errors in original lecture fixed.)



Candy, Waltz (General Atomics)

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(General Atomics, U. Maryland, LLNL, PPPL, U. Colorado, UCLA, U. Texas)

#### DOE Scientific Discovery Through Advanced Computing

#### http://fusion.gat.com/theory/pmp

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- J. Ongena (JET)

## The Plasma Microturbulence Project

- A DOE, Office of Fusion Energy Sciences, SciDAC (Scientific Discovery Through Advanced Computing) project (~2001-2004)
- devoted to studying plasma microturbulence through direct numerical sumulation
- National Team (& four codes):
  - GA (Waltz, Candy)
  - U. MD (Dorland)
  - U. CO (Parker, Chen)
  - UCLA (Lebeouf, Decyk)
  - LLNL (Nevins P.I., Cohen, Dimits)
  - PPPL (Lee, Lewandowski, Ethier, Rewoldt, Hammett, ...)
  - UCI (Lin)
- They've done all the hard work ...















# Part 1: Intuitive picture of the ITG instability -- based on analogy with Inverted pendulum / Rayleigh-Taylor instability



# "Bad Curvature" instability in plasmas≈ Inverted Pendulum / Rayleigh-Taylor Instability

Growth rate:

Top view of toroidal plasma:



The Secret for Stabilizing Bad-Curvature Instabilities

# Twist in **B** carries plasma from bad curvature region to good curvature region:



Similar to how twirling a honey dipper can prevent honey from dripping.

$$\begin{array}{rcl} & growth rate & propagation from bad-curvative \\ & region & bad-curvative \\ & region & to good curvative regions \\ \hline MHD works well to lowest order in plasmas, so RHS  $\Rightarrow$   
$$\begin{array}{rcl} & \frac{Vt}{VRL} & > & h_{ij} VA \sim \frac{VA}{qR} \\ \hline & \frac{Vt}{VRL} & > & h_{ij} VA \sim \frac{VA}{qR} \\ \hline & \frac{V_{e}}{V_{A}^{2} RL} & > & l \\ \hline & \frac{V_{e}^{2} q^{2} R^{2}}{V_{A}^{2} RL} & > & l \\ \hline & LHS = & \frac{\beta}{2} \frac{q^{2} R}{L} = \frac{1}{2} \frac{q^{2} R}{\partial r} \left[ \frac{\partial \beta}{\partial r} \right] = \frac{1}{2} \propto MHD \end{array}$$$$

While MHD works well to lowest order in plasmas,  
there are next-order FLR corrections that defrust  
the magnetic field 
$$\neq$$
 allow  $E_{11} \neq 0 \Rightarrow$  allow  
the plasma to more separately from  $\frac{D}{2}$ .  
Still have some waves that can connect good  $\neq$   
bad convaries region. Unstable if:  
 $\delta \gg connection rate$ 

















Higher energy porticles VB drift faster, creates charge separation à trus E field, causes EXB flow that further accentuates perturbation. Positive feedback => instability.





Similar bad convertere drive for trapped electron modes...

## Spherical Torus has improved confinement and pressure limits (but less room in center for coils)



# Understanding Turbulence That Affects the Performance of Fusion Device



(Candy & Waltz, GA 2003)

Central temp ~  $10 \text{ keV} \sim 10^8 \text{ K}$ 

Large temperature gradient
→ turbulent eddies
→ cools plasmas
→ determines plasma size
needed for fusion ignition

Major progress in last decade: detailed nonlinear simulations (first 3-D fluid approximations, now 5-D f( $\vec{x}, v_{\parallel}, v_{\perp}, t$ )) & detailed understanding



Comprehensive 5-D computer simulations of core plasma turbulence being developed by Plasma Microturbulence Project. Candy & Waltz (GA) movies shown: d3d.n16.2x\_0.6\_fly.mpg & supercyclone.mpg, from <u>http://fusion.gat.com/comp/parallel/gyro\_gallery.html</u> (also at <u>http://w3.pppl.gov/~hammett/refs/2004</u>).

Microinstabilities are small-amplitude  
but still nonlinear  

$$n(r)$$
  
 $n(r)$   
 $n = n_0(r) + \tilde{n}(x,t)$   
 $n_0 >> \tilde{n}$   
but  $\nabla n_0 \sim \nabla \tilde{n}$   
 $\int C_{on} locally flatten
or reverse total gradient
that was driving instability.
* Turbulence causes loss of plasma to the wall,
but confinement still x10S better than without B.
If no B, loss time  $\sim \frac{a}{V_{\rm E}} \sim 1$  psec  
with B, expts. measure  $\sim 0.1$ -10 sec.$ 

# Simple picture of reducing turbulence by negative magnetic shear

- Particles that produce an eddy tend to follow field lines.
- Reversed magnetic shear twists eddy in a short distance to point in the ``good curvature direction".
- Locally reversed magnetic shear naturally produced by squeezing magnetic fields at high plasma pressure: ``Second stability'' Advanced Tokamak or Spherical Torus.
- Shaping the plasma (elongation and triangularity) can also change local shear



### Sheared flows can suppress or reduce turbulence



### Sheared ExB Flows can regulate or completely suppress turbulence (analogous to twisting honey on a fork)



Dominant nonlinear interaction between turbulent eddies and  $\pm \theta$ -directed zonal flows.

Additional large scale sheared zonal flow (driven by beams, neoclassical) can completely suppress turbulence

#### Fascinating Diversity of Regimes in Fusion Plasmas. What Triggers Change? What Regulates Confinement?



R. Nazikian et al.

# All major tokamaks show turbulence can be suppressed w/ sheared flows & negative magnetic shear / Shafranov shift



Internal transport barrier forms when the flow shearing rate  $dv_{\theta}/dr > \sim$  the max linear growth rate  $\gamma_{lin}^{max}$  of the instabilities that usually drive the turbulence.

Shafranov shift  $\Delta$ ' effects (self-induced negative magnetic shear at high plasma pressure) also help reduce the linear growth rate.

Advanced Tokamak goal: Plasma pressure ~ x 2,  $P_{fusion} \propto pressure^2 ~ x 4$ 

### Transition to Enhanced Confinement Regime is Correlated with Suppression of Core Fluctuations in TFTR



 Similar suppression observed on JET (X-mode reflectometer) and DIII-D (FIR Scattering)

Hahm, Burrell, Phys. Plas. 1995, E. Mazzucato et al., PRL 1996.



R. Nazikian et al.

## **Improved Stellarators Being Built**

- Magnetic field twist and shear provided by external coils, not plasma currents. More stable?
- Computer optimized designs much better than 1950-60 slide rules?
- Quasi-toroidal symmetry allows plasma to spin toroidally: shear flow stabilization?





Part 2: Rigorous derivation of ITG growth rate & threshold (in a simple limit) starting from the Gyrokinetic Eq.

Our starting point will be the electrostatic Gyrotemetic  
Eq. written in a Drift-Kinetic-like form for the  
full, gyro-averaged, guiding center density 
$$f(R, v_n, \mu, t)$$
:

$$\frac{\partial \widetilde{f}}{\partial t} + (v_{\parallel} \mathbf{\hat{b}} + \mathbf{v}_E + \mathbf{v}_d) \cdot \nabla \widetilde{f} + \left(\frac{q}{m} E_{\parallel} - \mu \nabla_{\parallel} B + v_{\parallel} (\mathbf{\hat{b}} \cdot \nabla \mathbf{\hat{b}}) \cdot \mathbf{v}_E\right) \frac{\partial \widetilde{f}}{\partial v_{\parallel}} = 0$$

-

$$\frac{details:}{K} = \frac{details:}{W} = \frac{details}{W} = \frac{d$$

even though 
$$\frac{V_E}{V_t} \sim \frac{P_R}{R} \sim \mathcal{E}$$
,  $\frac{V_E \cdot V_l}{V_{ll} \cdot \delta \cdot \nabla} \sim \frac{V_t \frac{P_R}{R} h_{ll}}{V_t \cdot h_{ll}} \sim \frac{h_l P}{h_{ll} \cdot R}$   
~ 1

$$\frac{\partial \overline{f}}{\partial t} + (v_{\parallel}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m}E_{\parallel} - \mu\nabla_{\parallel}B + v_{\parallel}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \overline{f}}{\partial v_{\parallel}} = 0$$
Linearize:  $\overline{f} = F_{o} + \widetilde{f}$ , where  $F_{o}$  satisfies Equilibrium Eq.  
 $\frac{\partial}{\partial t} = \partial \quad \underline{E} = 0$ 
 $\left(V_{\parallel}\stackrel{h}{\mathbf{b}} + \underline{V}_{d}\right) \cdot \nabla F_{o} - \mu \nabla_{\parallel} \beta \frac{\partial F_{o}}{\partial V_{\parallel}} = 0$ 
General Equilibrium solution could be an arbitrary function of the constants banana orbits or passing of the motion  $(E, \mu, P_{\phi})$  where  $E = \frac{1}{2}mv_{\parallel}^{2} + \mu \beta$ .  
 $E = \frac{1}{2}mv_{\parallel}^{2} + \mu \beta$ 
 $d \quad P_{\phi} = \text{ canonical angular momentum}$ 
 $\beta_{v}t$  if we neglect  $\frac{|V_{h}|}{V_{h}} \sim \frac{f}{R}$  get simpler Eq.:

$$V_{II} \hat{b} \cdot \nabla F_{0} - \mu (\hat{b} \cdot \nabla B) \frac{\partial F_{0}}{\partial V_{II}} = 0$$
  
Will consider Equilibrium of the form:  

$$F_{0} (R, V_{II}, \mu) \propto \frac{n_{0}(Y)}{T_{0}^{3/2}(Y)} e^{-\frac{m(\frac{1}{2}V_{II}^{2} + \mu B(X))}{T(Y)}} \propto e^{-\frac{E}{T}}$$
  
Exercise: Plug this in to the previous Eq. + show it is  
a solution.

$$\begin{split} \frac{\partial \tilde{f}}{\partial t} + (v_{\parallel}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \tilde{f} + \left(\frac{q}{m}E_{\parallel} - \mu \nabla_{\parallel}B + v_{\parallel}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right) \frac{\partial \tilde{f}}{\partial v_{\parallel}} &= 0 \\ \\ \text{Lmearize:} \quad \tilde{f} = F_{o} + \tilde{f}, \text{ where } F_{o} \text{ satisfies Equilibrium Eq.} \\ \text{Next order Eq:} \\ \frac{\partial \tilde{f}}{\partial t} + \left(v_{\parallel}\hat{\mathbf{b}} + v_{d}\right) \cdot \nabla \tilde{f} - \mu \nabla_{\mu}\beta \frac{\partial \tilde{f}}{\partial v_{\parallel}} &= - \bigvee_{E} \cdot \nabla F_{o} \\ - \left(\frac{q}{m}E_{\mu} + v_{\parallel}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot v_{E}\right) \frac{\partial F}{\partial v_{\parallel}} \end{split}$$

$$\left( -\lambda \omega + \lambda v_{\mu} h_{\mu} + \lambda v_{\theta} \cdot h_{\mu} \right) \widetilde{f} = - v_{E} \cdot \nabla F_{o} - \left( \frac{q}{m} E_{\mu} + v_{\mu} \left( b \cdot \nabla b \right) \cdot v_{E} \right) \frac{\partial F_{o}}{\partial v_{\mu}}$$

$$\frac{\operatorname{Important Subtlety}: F(\underline{R}, \underline{V}_{u}, \underline{P}, \underline{t}) \quad so}{-\underline{V}_{\underline{C}} \cdot \nabla F_{o} = -\underline{V}_{\underline{C}} \cdot \nabla \Big| F_{o} \quad V_{u, \underline{P}, \underline{t}} \\ \quad using \quad F_{o} \propto \frac{n_{o}(r)}{T_{o}^{3/2}} e^{-\frac{(\underline{t} - m_{u} + m_{\underline{P}} \cdot \underline{B}(\underline{x}))}{T_{o}(r)}} \\ \quad w_{ull give terms proportional to } \nabla n_{o}, \nabla T_{o}, \underline{t} = \underline{P} \cdot \nabla B \\ \nabla n_{o} terms: -\underline{V}_{\underline{C}} \cdot \nabla F_{o} \Rightarrow t \frac{c}{B} \left( \nabla \underline{\Psi} \times \widehat{b} \cdot \underline{\nabla} \underline{n}_{o} \right) F_{o} \\ p_{o}^{10udal} = -\frac{c}{B} \quad \nabla \underline{F} \times \widehat{b} \cdot \widehat{r} \cdot \underline{L}_{u} \quad F_{o} \qquad \frac{\nabla n_{o}}{n_{o}} = -\frac{\widehat{r}}{L_{u}} \\ \theta = -\frac{c}{B} \cdot A_{\theta} \cdot \underline{E} \cdot \underline{L}_{u} \quad F_{o} \qquad \frac{\nabla n_{o}}{n_{o}} = -\frac{\widehat{r}}{L_{u}} \\ \theta = -\frac{c}{B} \cdot A_{\theta} \cdot \underline{E} \cdot \underline{F}_{o} \qquad \frac{\omega_{x,\overline{x}}}{T_{o}} = -\frac{c}{R} \cdot A_{\theta} \cdot \underline{L}_{u} \\ \theta = -\frac{c}{R} \cdot A_{\theta} \cdot \underline{F}_{v} \quad F_{o} \qquad \frac{\omega_{x,\overline{x}}}{T_{o}} = -\frac{c}{R} \cdot A_{\theta} \cdot \underline{L}_{u} \\ \theta = -h_{\theta} \rho_{s} \cdot \frac{c_{s}}{L_{u}} \\ \theta = -h_{\theta} \cdot \frac{c_{s}$$



With B field out of the page,  
the VB drift for ions is  
downward  

$$V_{\partial} \approx - \frac{\partial}{\partial V_{\pm}} f_{R} \quad (at \theta = 0)$$
  
 $V_{\partial} \approx - \frac{\partial}{\partial V_{\pm}} f_{R} \quad (at \theta = 0)$   
defining  $W_{dv} = h \cdot V_{d}$   
gives convention used in Beer's  
thesis:

$$\omega_{dv} = \omega_d (v_{\parallel}^2 + \mu B) / v_t^2$$
$$\omega_d = -k_{\theta} \rho v_t / R$$

More on Sign Convertions  

$$\sum_{i=1}^{n} \sum_{i=1}^{n} \sum_$$

$$= - \frac{h}{eB} \frac{h}{L_{r}}$$

(Back to RHS of Incarized GK Eq., 4 slides back)  $-\underbrace{v}_{E}\cdot\nabla F_{o}-(\underbrace{\mathbf{q}}_{m}E_{n}+v_{n}(b\cdot\nabla b)\cdot v_{E})\frac{\partial F_{o}}{\partial v_{n}}$ RHS = $\propto + V_{\parallel} \begin{pmatrix} \wedge & & \\ b & \nabla & b \end{pmatrix} \cdot \begin{pmatrix} \wedge & & \\ b & \times \nabla & \overline{\phi} \end{pmatrix}$ part of this ~- c VExb. pVB  $\sim -\nabla \Psi \cdot \left[ p \hat{b} \times \nabla B + v_{ij} \hat{b} \times (\hat{b} \cdot \nabla \hat{b}) \right]$ + curvature drift 7B  $RHS = +i\left(\omega_{xv}^{T} - \omega_{dv} - h_{u}v_{u}\right) \frac{eF}{T} F_{o}$  $\omega_{dv} = \omega_d (v_{\scriptscriptstyle \parallel}^2 + \mu B) / v_t^2$  $\omega_*^T = \omega_* [1 + \eta (v_{\parallel}^2 / 2v_t^2 + \mu B / v_t^2 - 3/2)]$  $\omega_{a} \equiv -\frac{v_{t}}{p} p \left( h_{\theta} \cos \theta + h_{r} \sin \theta \right)$  $\omega_{\star} = h_{\theta} \rho \frac{V_{t}}{I}$   $\eta = \frac{L_{n}}{L_{\tau}}$ 

$$\int_{a}^{2} \int_{a}^{b} \int_{a$$

$$\left( -\kappa \omega + i v_{\parallel} h_{\parallel} + i v_{\vartheta} \cdot h_{\perp} \right) \widetilde{f} = - v_{\varepsilon} \cdot \nabla F_{o} - \left( \frac{q}{m} E_{\parallel} + v_{\parallel} \left( b \cdot \nabla b \right) \cdot v_{\varepsilon} \right) \frac{2F_{o}}{2v_{\parallel}}$$

subst. for RHS  

$$(-\omega + i v_{11}h_{11} + i \omega_{dv}) \tilde{f} = -i (-\omega_{xv}^{T} + \omega_{dv} + h_{11}v_{11}) \frac{e\bar{\Phi}}{T_{o}} F_{o}$$

$$(\bar{f} = -\omega_{xv}^{T} + (h_{11}v_{11} + \omega_{dv})) \frac{e\bar{\Phi}}{T_{o}} F_{o}$$

$$N_{o} + e^{i} recover Boltzmann response when h_{11}v_{11} + or \omega_{dv} large$$

$$\widetilde{f} = \frac{-\omega_{xv}^{T} + (h_{1v}v_{1v} + \omega_{dv})}{\omega - (h_{1v}v_{1v} + \omega_{dv})} \frac{e \Phi}{T_{o}} F_{v}$$

(slab "n;" version at ITG requires finite hill ti, but not toroidal version),

$$n_{eo} \frac{e\overline{P}}{T_e} = \int d^3 v \frac{-\omega_{\star v}^T + \omega_{av}}{\omega - \omega_{dv}} F_o \frac{e\overline{P}}{T_{vo}}$$

electrons (additional polarization

$$N_{o} \stackrel{e \neq}{=} = N_{o} \stackrel{e \neq}{=} \int d^{3}v \stackrel{F_{o}}{=} \frac{\omega_{dv} - \omega_{yT}}{\omega - \omega_{dv}}$$

$$"Cold plasma" or "fast wave" approx.  $\omega >> \omega_{dv}$ 

$$\frac{T_{no}}{T_{eo}} = \int d^{3}v \stackrel{F_{o}}{=} \frac{\omega_{dv} - \omega_{xT}}{\omega} \left(1 + \frac{\omega_{dv}}{\omega} + \cdots\right)$$$$

$$\frac{T_{no}}{T_{eo}} = \int d^{3}_{V} \frac{F_{o}}{h_{o}} \frac{\omega_{\partial v} - \omega_{*T}}{\omega} \left( 1 + \frac{\omega_{\partial v}}{\omega} + \cdots \right)$$

$$\omega_{dv} = \omega_{d} (v_{\parallel}^{2} + \mu B) / v_{t}^{2} \qquad \omega_{*}^{T} = \omega_{*} [1 + \eta (v_{\parallel}^{2} / 2v_{t}^{2} + \mu B / v_{t}^{2} - 3 / 2)]$$

$$\frac{\omega_{d}}{\omega_{d}} = -k_{\theta} \rho v_{t} / R \qquad \omega_{*} = -k_{\theta} \rho v_{t} / L_{n}$$

$$\int d^{3}_{V} \frac{F_{o}}{h_{o}} \omega_{\partial v} = \int d^{3}_{V} \frac{F_{o}}{h_{o}} \omega_{d} \left( v_{n}^{2} + \frac{1}{2} v_{\perp}^{2} \right) / v_{t}^{2}$$

$$= 2 \omega_{d}$$

$$\frac{T_{Ao}}{T_{eo}} = \int d^{3}_{V} \frac{F_{o}}{h_{o}} \frac{\omega_{dv} - \omega_{XT}}{\omega} \left( 1 + \frac{\omega_{dv}}{\omega} + \cdots \right) \\
\omega_{dv} = \omega_{d} (v_{\parallel}^{2} + \mu B) / v_{t}^{2} \qquad \omega_{*}^{T} = \omega_{*} [1 + \eta (v_{\parallel}^{2} / 2v_{t}^{2} + \mu B / v_{t}^{2} - 3/2)] \\
\omega_{d} = -k_{\theta} \rho v_{t} / R \qquad \omega_{*} = -k_{\theta} \rho v_{t} / L_{n} \qquad = \frac{1}{2} v_{\perp}^{2} = \frac{1}{2} \left( v_{X}^{2} + v_{Y}^{2} \right) \\
\int d^{3}_{V} \frac{F_{o}}{h_{o}} \omega_{X}^{T} = \omega_{*} \left( 1 + \eta \left( \frac{1}{2} + 1 - \frac{3}{2} \right) \right) = \omega_{X} \\
\int d^{3}_{V} \frac{F_{o}}{h_{o}} \omega_{dv}^{T} = \int d^{3}_{v} \frac{F_{o}}{h_{o}} \omega_{d}^{2} \left[ v_{u}^{H} + 2 v_{u}^{2} \frac{1}{2} v_{\perp}^{2} + \frac{1}{4} \left( v_{X}^{2} + v_{Y}^{2} \right)^{2} \right] \frac{1}{v_{t}^{4}} \\
= \omega_{d}^{2} \left[ 3 + 2 \cdot \frac{1}{2} \left( 1 + 1 \right) + \frac{1}{4} \left( \left( v_{X}^{4} + 2v_{X}^{2} + v_{Y}^{4} - v_{Y}^{4} \right) \right) \right] \\
= \omega_{d}^{2} \left[ 5 + \frac{1}{4} \left( 8 \right) \right] = 7 w_{d}^{2}$$

$$\frac{T_{no}}{T_{eo}} = \int d^3 v \frac{F_o}{h_o} \frac{\omega_{dv} - \omega_{xT}}{\omega} \left( 1 + \frac{\omega_{dv}}{\omega} + \cdots \right)$$

$$\int d^{3}v \frac{F_{o}}{n_{o}} \omega_{dv} \omega_{\star}^{T} = \omega_{d} \omega_{\star} \begin{cases} 2 \\ + \eta \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{N_{o}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \\ + \eta \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \\ + \eta \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{t}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{V_{t}^{2}} \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \int d^{3}v \frac{F_{o}}{V_{t}^{2}} \left( \frac{1}{2}V_{1}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \frac{V_{t}^{2}}{V_{t}^{2}} \frac{V_{t}^{2}}{V_{t}^{2}} + \frac{1}{2}V_{t}^{2} + \frac{1}{2}V_{t}^$$

$$= \omega_{d}\omega_{*} \left\{ 2 + \eta \left[ \frac{1}{2} 3 + \frac{1}{2} 2 - \frac{3}{2} + \frac{1}{2} \cdot 2 \cdot \frac{1}{2} + \frac{1}{4} 8 - \frac{1}{2} \cdot 2 \cdot \frac{3}{2} \right] \right\}$$

$$\int d^{3}v \frac{F_{o}}{n_{o}} \omega_{dv} \omega_{\star}$$

$$= \omega_{d} \omega_{\star} \left\{ 2 + \eta \left[ \frac{1}{2} 3 + \frac{1}{2} 2 - \frac{3}{2} + \frac{1}{2} \cdot 2 \cdot \frac{1}{4} + \frac{1}{4} 8 - \frac{1}{2} \cdot 2 \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{2} \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{2} \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{2} \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{4$$

This defines a dispersion relation w us. h

$$\begin{bmatrix} \frac{T_{vo}}{T_{eo}} = 2 \frac{\omega J}{\omega} - \frac{\omega \star}{\omega} + 7 \frac{\omega J}{\omega^2} - 2 \frac{\omega J \omega_{\star}}{\omega^2} (1+\eta) \end{bmatrix}$$

Consider the flat density limit: 
$$\nabla n \rightarrow 0$$
, but  $\nabla T \neq 0$   
 $\omega_* = -h_{\theta} \rho \frac{V_t}{L_n} \rightarrow 0$ 
 $\eta = \frac{1}{T} \nabla T = \frac{L_n}{L_T} \rightarrow \infty$ 

$$\omega_{*}\eta = -h_{\theta}\rho \frac{V_{t}}{L_{n}} \frac{L_{n}}{L_{\tau}} \equiv \overline{\omega}_{*\tau}$$

$$\omega^{2} \frac{T_{iv}}{T_{e_{o}}} = 2 \omega_{d} \omega + 2 \omega_{d} \overline{\omega_{x_{T}}} - 7 \omega_{d}^{2} = 0$$

$$\omega = 2 \omega_{d} \pm \sqrt{4 \omega_{a}^{2}} - 4 \frac{T_{iv}}{T_{e_{o}}} \left(2 \omega_{d} \overline{\omega_{x_{T}}} - 7 \omega_{d}^{2}\right)$$

$$2 \left(T_{iv}/T_{e_{o}}\right)$$

From last page:  

$$W = 2W_{d} \pm \sqrt{4W_{a}^{2} - 4\frac{T_{iv}}{T_{e_{o}}}(2W_{d}W_{*T} - 7W_{d}^{2})}$$

$$2(T_{iv}/T_{e_{o}})$$

Consider large temperature gradient limit:  $\omega_{*T} \propto \nabla T$  f Growth rate:

$$Y = \frac{\sqrt{2} \omega_{d} \overline{\omega_{xT}}}{\sqrt{T_{x0}/T_{e0}}} = \frac{\sqrt{2} h_{\theta} \rho_{i}}{\sqrt{T_{x0}/T_{e0}}} \frac{V_{t,i}}{\sqrt{RL_{T}}}$$
  
Fundamental scaling of bad-curvature driven instabilities.

Go back to general D.R.:  

$$\begin{aligned}
\omega &= \frac{2 \omega_{\theta} \pm \sqrt{4 \omega_{a}^{2} - 4 \frac{T_{iv}}{T_{e_{0}}} \left(2 \omega_{a} \overline{\omega}_{*\tau} - 7 \omega_{a}^{2}\right)}{2 \left(T_{iv} / T_{e_{0}}\right)} \\
&= 2 \omega_{a} \pm \sqrt{\left(4 + 28 \frac{T_{av}}{T_{e_{0}}}\right) \omega_{a}^{2} - 8 \frac{T_{ao}}{T_{e_{0}}} \omega_{a} \overline{\omega}_{*\tau}}}{2 \left(T_{ao} / T_{e_{0}}\right)} \\
\text{Instability exists if} \\
8 \frac{T_{ao}}{T_{e_{0}}} \omega_{\theta} \overline{\omega}_{*\tau} > \omega_{a}^{2} \left(4 + 28 \frac{T_{av}}{T_{e_{0}}}\right) \\
&= \frac{1}{R} \frac{1}{L_{T}} > \frac{1}{R^{2}} \left(\frac{1}{2} \frac{T_{e_{0}}}{T_{e_{0}}} + \frac{1}{2} 7\right) \\
&= \frac{1}{R} \frac{1}{L_{T}} > \frac{1}{2} \left(7 + \frac{T_{e_{0}}}{T_{e_{0}}}\right)
\end{aligned}$$

Compare w/ Romanelli 1990 (Eq. 12):  

$$\eta_{i} = (\frac{5}{3} + \tau/4)2\epsilon_{n}$$
or
$$\frac{L_{n}}{L_{\tau}} = (\frac{5}{3} + \frac{1}{4} + \frac{T_{e}}{T_{i}})^{2} \frac{L_{n}}{R}$$

$$\frac{R}{L_{\tau crit}} = \frac{10}{3} + \frac{1}{2} + \frac{T_{eo}}{T_{io}}$$

$$= 3.33 + 0.5 + \frac{T_{eo}}{T_{io}}$$
vs. my
$$\frac{R}{L_{\tau crit}} = 3.5 + 0.5 + \frac{T_{eo}}{T_{io}}$$





Why does this get the 
$$\frac{T_{io}}{T_{eo}}$$
 dependence of  
 $\frac{R}{L_{torit}}$  wrong? More accurate:  $\frac{R}{L_{t}} \cdot \frac{R}{L_{torit}} = \frac{4}{3}(1+\frac{T_{io}}{T_{eo}})$   
Because near marginal studielity, the expansion  
of the resumpt denomination  
 $\frac{1}{W-W_{dV}} \approx \frac{1}{W}(1+\frac{W_{dV}}{W}+...)$ 

breaks down, since waw a neur Morginal stability...

More general result for threshold for metability:  

$$\frac{R_{o}}{L_{torit}} = M_{ax} \left[ \left( 1 + \frac{T_{i}}{T_{e}} \right) \left( 1.33 + 1.91 \frac{s}{q} \right) \left( 1 - 1.5 \frac{r}{R} \right) \left( 1 + 0.3 \frac{rdk}{dr} \right) \right]$$

$$0.8 \frac{R_{o}}{L_{h}} \right]$$

# **ITG References**

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- Earlier history:
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  - Sheared-slab eta\_i mode: Coppi, Rosenbluth, and Sagdeev, Phys. Fluids 1967
  - Toroidal ITG mode: Coppi and Pegoraro 1977, Horton, Choi, Tang 1981, Terry et al. 1982, Guzdar et al. 1983... (See Beer's thesis)