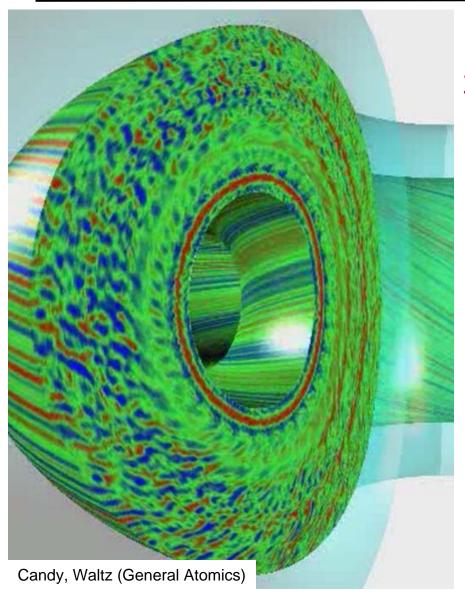
### Heat Transport in Tokamaks (I): The Bad-curvature ITG Instability



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CMPD/CMSO Winter School UCLA, Jan. 2009

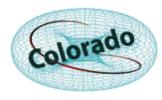
- I. Brief Fusion Status Report
- II. Physical picture of effective-gravity / bad-curvature instabilities in toroidal magnetic fields, based on invertedpendulum and Rayleigh-Taylor analogies.
- III. Detailed linear calculation of lon Temperature Gradient instability from drift/gyro-kinetic Eq.

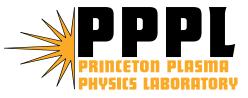
#### The Center For Plasma Microturbulence Studies

- A DOE, Office of Fusion Energy Sciences, SciDAC (Scientific Discovery Through Advanced Computing) project
- devoted to studying plasma microturbulence through direct numerical sumulation
- National Team (& 3 main codes):
  - GA (Waltz, Candy)
  - U. MD (Dorland)
  - U. CO (Parker, Chen)
  - LLNL (Nevins P.I.)
  - PPPL (Hammett, Mikkelsen, Rewoldt ...)
  - MIT
- They've done all the hard work ...







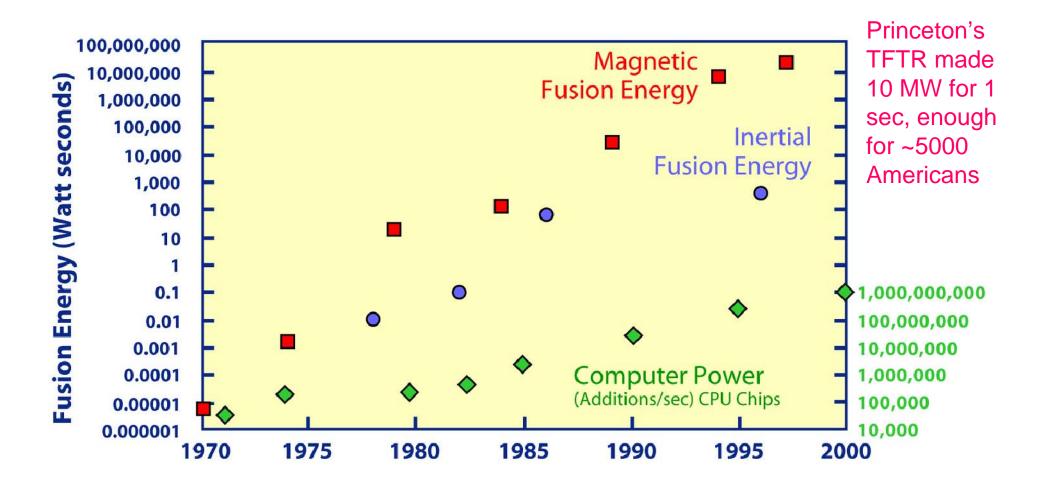






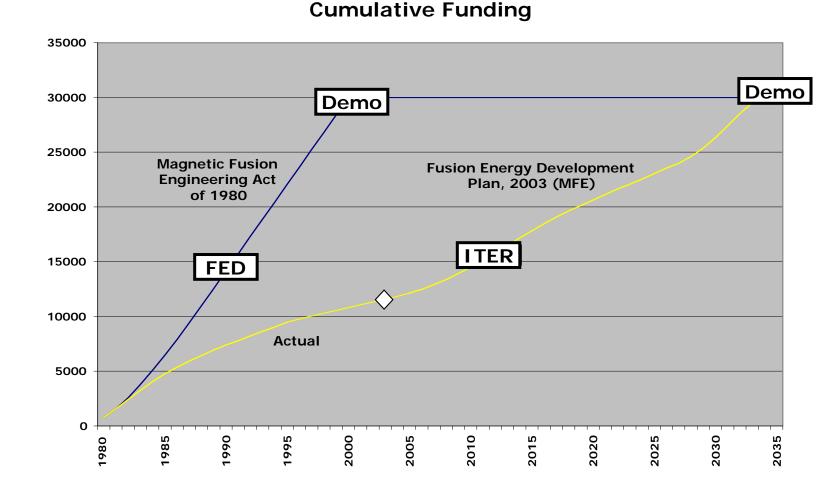
Massachusetts Institute of Technology

### Progress in Fusion Energy has Outpaced Computer Speed



Some of the progress in computer speed can be attributed to plasma science.

#### The Estimated Development Cost for Fusion Energy is Essentially Unchanged since 1980



On budget, if not on time.

\$M, FY02

\$30B development cost tiny compared to >\$100 Trillion energy needs of 21st century and potential costs of global warming. Still 40:1 payoff after discounting 50+ years.

# Need to aggressively pursue a portfolio of alternative energy in the near term (10-30 years)

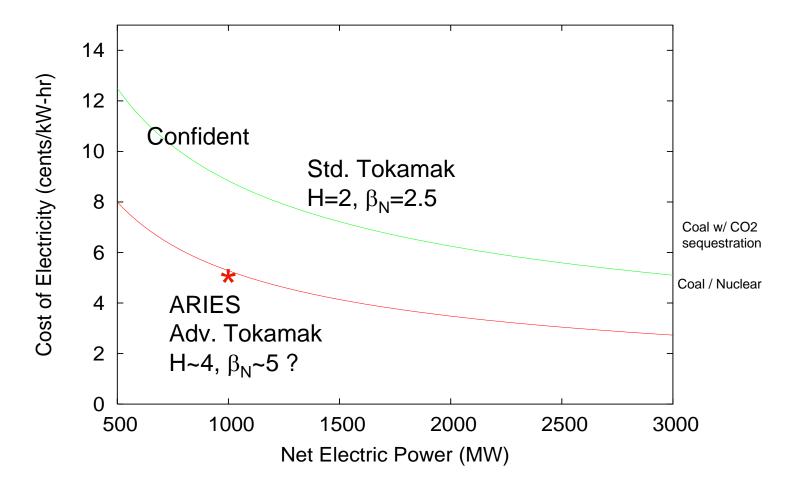
Needed to deal with global warming & energy independence economic issues

- improved building & transportation efficiency
- plug-in hybrid, CNG, vehicles
- wind power
- concentrated solar
- clean coal with CO2 sequestration
- synfuels+biomass with CO2 sequestration
- fission nuclear power plants
- ...

However, there are uncertainties about all of these energy sources: cost, quantity, intermittency, side-effects. How much CO2 can be stored underground long term, and at what cost? Energy demand in the developing world will continue to grow throughout this century.

Long term, still need something like fusion energy, or fission breeder reactors, or ?

#### $\downarrow$ turbulence & $\uparrow \beta$ could significantly improve fusion

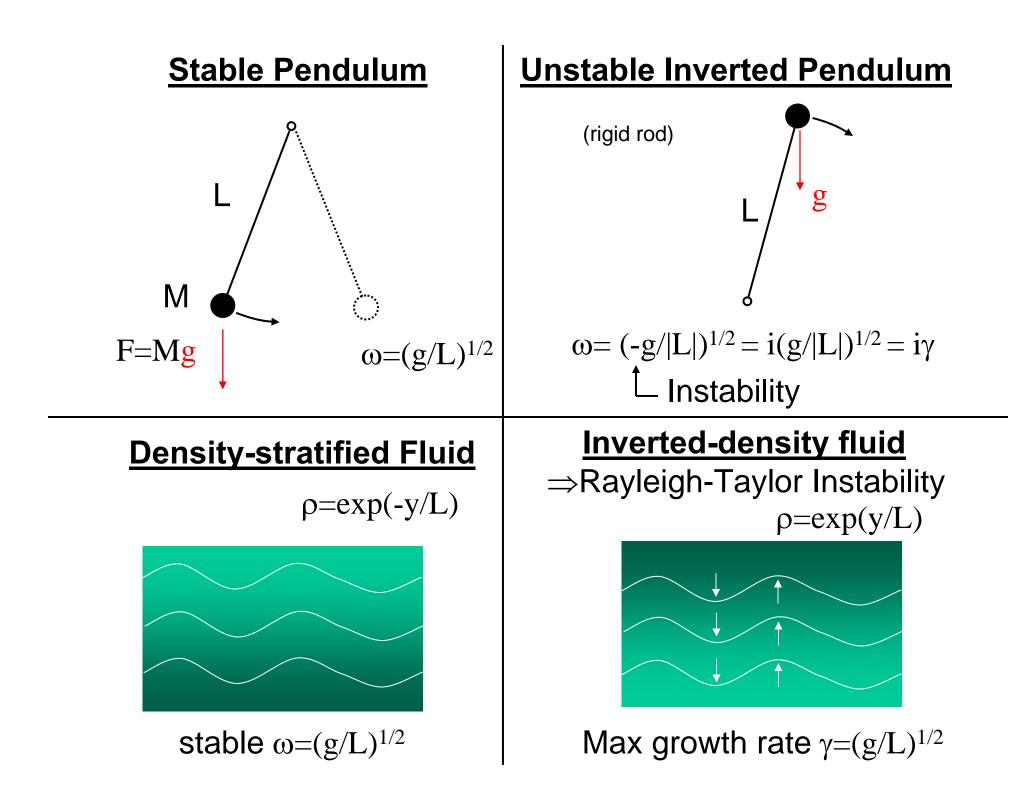


Can't just go to arbitrarily large reactor sizes: Heat flux to wall & Greenwald density limit get worse

(Relative Cost of Electricity (COE) estimates in this study, see ARIES reactor studies for more detailed & lower costs estimates.)

From Galambos, Perkins, Haney, & Mandrekas 1995 Nucl.Fus. (very good), scaled to match ARIES-AT reactor design study (2001), http://aries.ucsd.edu/ARIES/

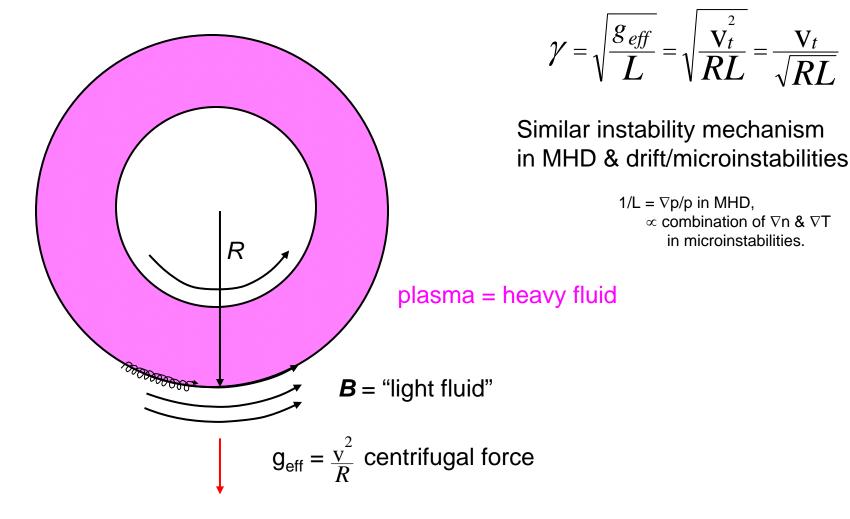
# Part 1: Intuitive picture of the ITG instability -- based on analogy with Inverted pendulum / Rayleigh-Taylor instability



## "Bad Curvature" instability in plasmas ≈ Inverted Pendulum / Rayleigh-Taylor Instability

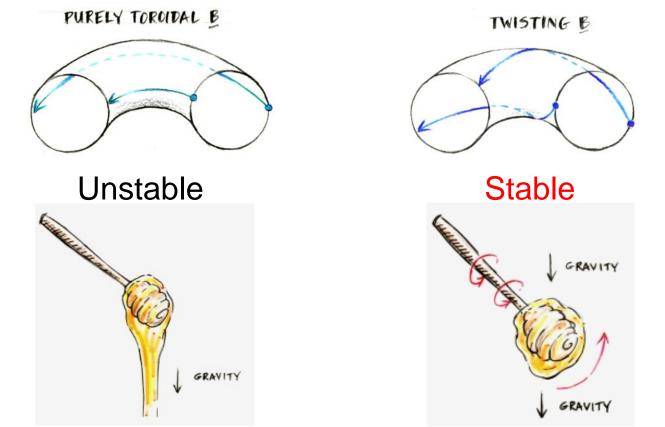
Growth rate:

Top view of toroidal plasma:



The Secret for Stabilizing Bad-Curvature Instabilities

## Twist in **B** carries plasma from bad curvature region to good curvature region:



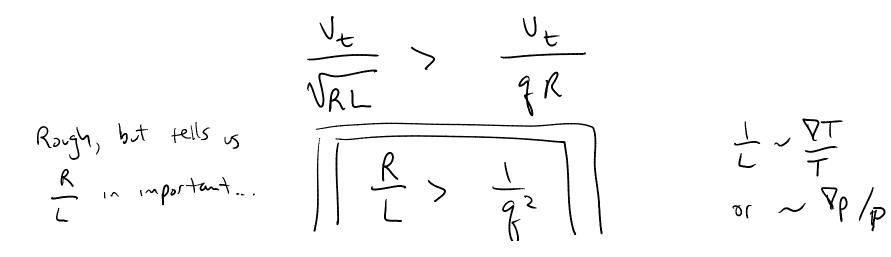
Similar to how twirling a honey dipper can prevent honey from dripping.

$$\begin{array}{rcl} & growth rate & propagation from bad-curvative \\ & n & bad-curvative & \\ & region & b & good curvative regions \\ \end{array}$$

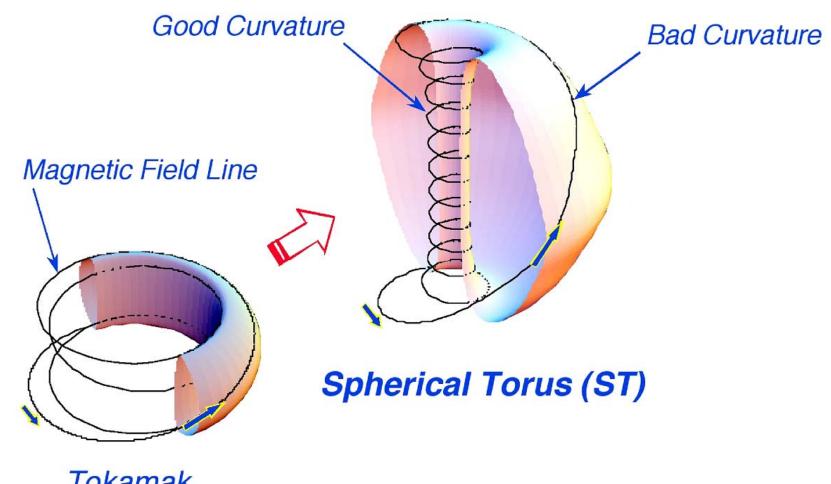
$$\begin{array}{rcl} MHD & workes & well & to & lowest & order & in & plasmas, so & RHS \Rightarrow \\ & \frac{Vt}{VRL} & > & h_{ij} VA \sim \frac{VA}{qR} \\ \end{array}$$

$$\begin{array}{rcl} Square: & \frac{V_{e}^{2} q^{2}R^{2}}{V_{A}^{2} RL} > & l \\ LHS = & \frac{B}{2} q^{2}R \\ L & = & \frac{1}{2} q^{2}R \\ \end{array}$$

While MHD works well to lowest order in plasmas,  
there are next-order FLR corrections that defrust  
the magnetic field 
$$\neq$$
 allow  $E_{11} \neq 0 \Rightarrow$  allow  
the plasma to more separately from  $\frac{D}{2}$ .  
Still have some waves that can connect good  $\neq$   
bad convaries region. Unstable if:  
 $\delta \geq connection rate$ 



#### **Spherical Torus has improved confinement and pressure** limits (but less room in center for coils)



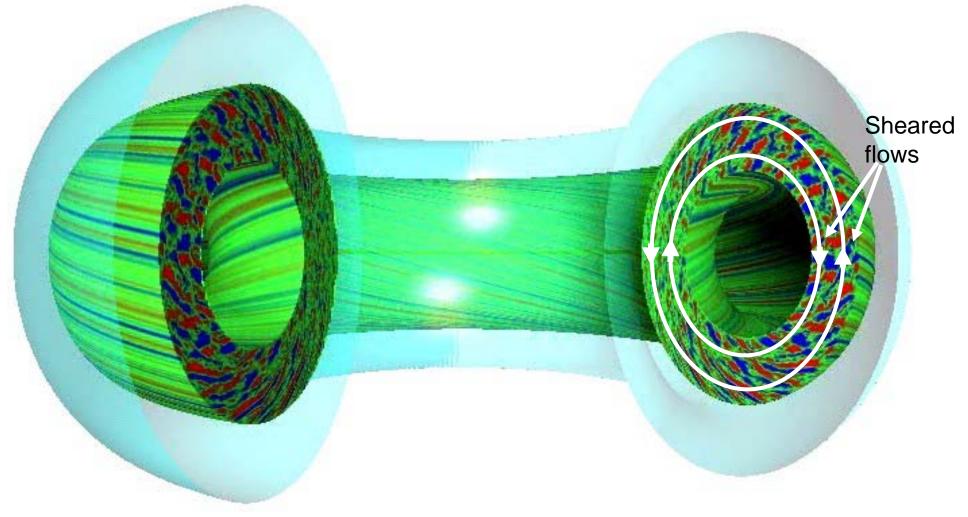
Tokamak

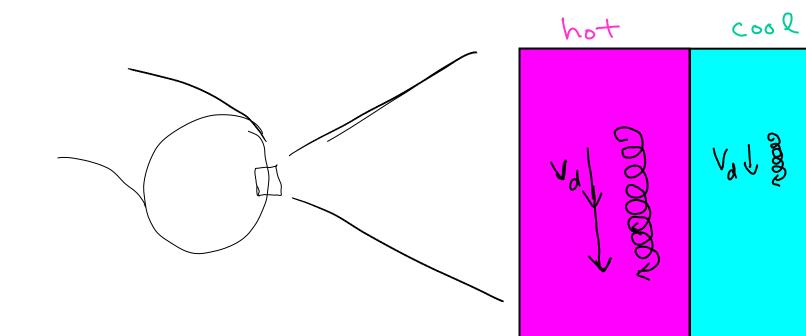
# These physical mechanisms can be seen in gyrokinetic simulations and movies

Stable side, smaller eddies Unstable bad-curvature side, eddies point out, direction of effective gravity

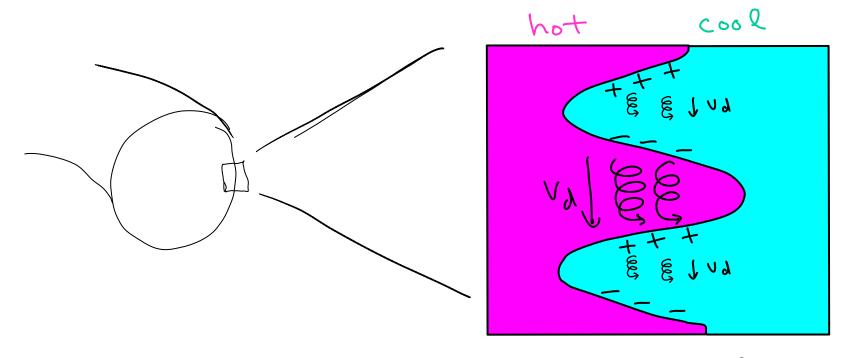
particles quickly move along field lines, so density perturbations are very extended along fields lines, which twist to connect unstable to stable side Movie <u>http://fusion.gat.com/THEORY/images/3/35/D3d.n16.2x\_0.6\_fly.mpg</u> from <u>http://fusion.gat.com/theory/Gyromovies</u> shows contour plots of density fluctuations in a cut-away view of a GYRO simulation (Candy & Waltz, GA). This movie illustrates the physical mechanisms described in the last few slides. It also illustrates the important effect of sheared flows in breaking up and limiting the turbulent

eddies. Long-wavelength equilibrium sheared flows in this case are driven primarily by external toroidal beam injection. (The movie is made in the frame of reference rotating with the plasma in the middle of the simulation. Barber pole effect makes the dominantly-toroidal rotation appear poloidal..) Short-wavelength, turbulent-driven flows also play important role in nonlinear saturation.





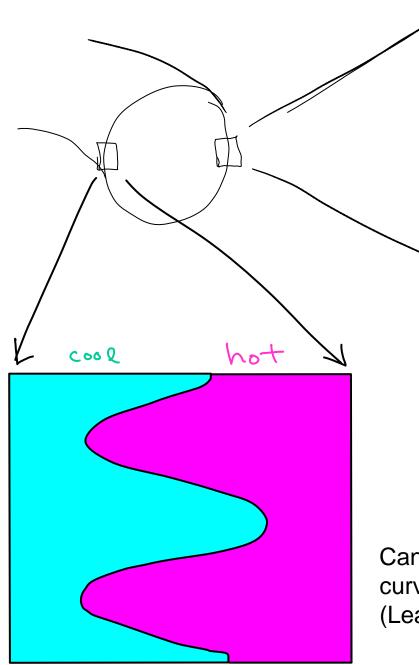
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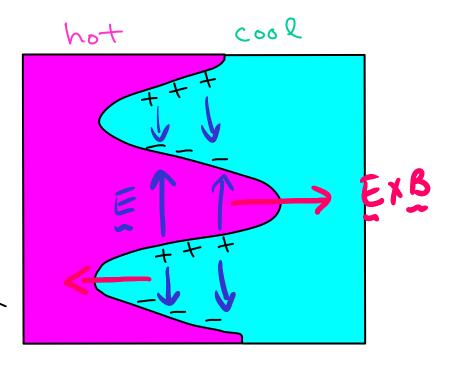


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perturbation. Positive feedback => instability.

Rosenbluth-Longmire picture





G ∇ß

Can repeat this analysis on the good curvature side & find it is stable. (Leave as exercise.)

Rosenbluth-Longmire picture

# Simple picture of reducing turbulence by negative magnetic shear

- Particles that produce an eddy tend to follow field lines.
- Reversed magnetic shear twists eddy in a short distance to point in the ``good curvature direction".
- Locally reversed magnetic shear naturally produced by squeezing magnetic fields at high plasma pressure: ``Second stability'' Advanced Tokamak or Spherical Torus.
- Shaping the plasma (elongation and triangularity) can also change local shear

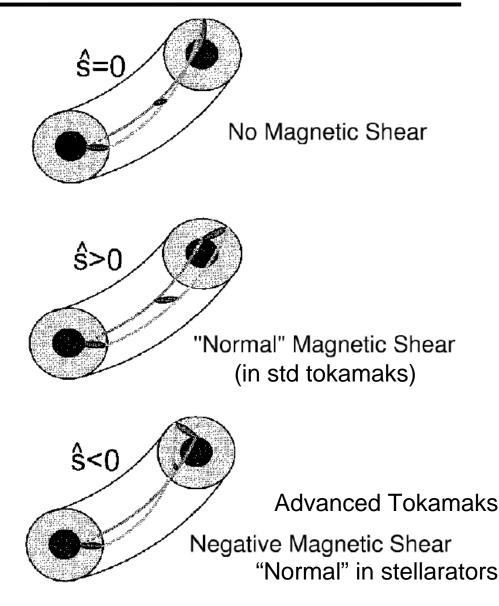
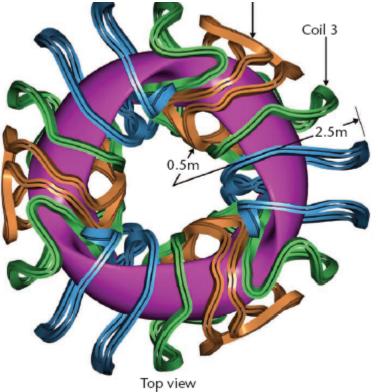
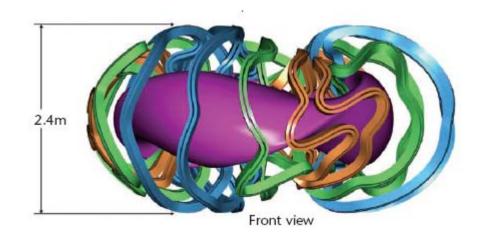


Fig. from Antonsen, Drake, Guzdar et al. Phys. Plasmas 96 Kessel, Manickam, Rewoldt, Tang Phys. Rev. Lett. 94

### **Improved Stellarators Being Studied**

- Originally invented by Spitzer ('51), the unique idea when fusion declassified ('57)
- Mostly abandoned for tokamaks in '69. But computer optimized designs now much better than slide rules. Now studying cost reductions.
- Quasi-symmetry discovered in late 90's: don't need vector *B* exactly symmetric toroidally, |*B*| symmetric in field-aligned coordinates sufficient to be as good as tokamak.
- Magnetic field twist & shear provided by external coils, not plasma currents, inherently steady-state. Stellarator expts. find they don't have Greenwald density limit or hard beta limit & don't disrupt. Quasi-symmetry allows plasma spin to reduce turbulence?





Part 2: Rigorous derivation of ITG growth rate & threshold (in a simple limit) starting from the Gyrokinetic Eq.

Our starting point will be the electrostatic Gyrotanetic  
Eq. written in a Drift-Kinetic-like form for the  
full, gyro-averaged, guiding center density 
$$f(R, v_{ii}, \mu, t)$$
:

$$\frac{\partial \widetilde{f}}{\partial t} + (v_{\parallel} \mathbf{\hat{b}} + \mathbf{v}_E + \mathbf{v}_d) \cdot \nabla \widetilde{f} + \left(\frac{q}{m} E_{\parallel} - \mu \nabla_{\parallel} B + v_{\parallel} (\mathbf{\hat{b}} \cdot \nabla \mathbf{\hat{b}}) \cdot \mathbf{v}_E\right) \frac{\partial \widetilde{f}}{\partial v_{\parallel}} = 0$$

$$\frac{details:}{K} = \frac{details:}{W} = \frac{details}{W} = \frac{d$$

even though 
$$\frac{V_E}{V_t} \sim f_R \sim E$$
,  $\frac{V_E \cdot V}{V_{l_l} \cdot b \cdot V} \sim \frac{V_t f_R h_L}{V_t \cdot h_{l_l}} \sim \frac{h_L f_R}{h_{l_l} \cdot R}$   
~ 1

$$\frac{Gyrukhetic tq. for full guding-center density f(k, v_{ii}, y, t):}{\frac{\partial \overline{f}}{\partial t} + (v_{ii}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m}E_{||} - \mu \nabla_{||}B + v_{||}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \overline{f}}{\partial v_{||}} = 0$$

$$\frac{\partial \overline{f}}{\partial t} + (v_{||}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m}E_{||} - \mu \nabla_{||}B + v_{||}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \overline{f}}{\partial v_{||}} = 0$$

$$\frac{\partial \overline{f}}{\partial t} + (v_{||}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m}E_{||} - \mu \nabla_{||}B + v_{||}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \overline{f}}{\partial v_{||}} = 0$$

$$\frac{\partial \overline{f}}{\partial t} + (v_{||}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m}E_{||} - \mu \nabla_{||}B + v_{||}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \overline{f}}{\partial v_{||}} = 0$$

$$\frac{\partial \overline{f}}{\partial t} + (v_{||}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + (v_{||}\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}} + v_{||}\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}} + v_{|}\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}} + v$$

$$\frac{\partial \overline{f}}{\partial t} + (v_{\parallel}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m}E_{\parallel} - \mu\nabla_{\parallel}B + v_{\parallel}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \overline{f}}{\partial v_{\parallel}} = 0$$
Linearize:  $\overline{f} = F_{o} + \widetilde{f}$ , where  $F_{o}$  satisfies Equilibrium Eq.  
 $\frac{\partial}{\partial t} = \partial \quad \underline{E} = 0$ 
 $\left(V_{\parallel}\stackrel{h}{\mathbf{b}} + \underline{V}_{d}\right) \cdot \nabla F_{o} - \mu \nabla_{\parallel} \beta \frac{\partial F_{o}}{\partial V_{\parallel}} = 0$ 
General Equilibrium solution could be an arbitrary function of the constants banana orbits or passing of the motion  $(E, \mu, P_{\phi})$  where  $E = \frac{1}{2}mv_{\parallel}^{2} + \mu \beta$ .  
 $E = \frac{1}{2}mv_{\parallel}^{2} + \mu \beta$ 
 $d \quad P_{\phi} = \text{ canonical angular momentum}$ 
 $\beta_{v}t$  if we neglect  $\frac{|V_{h}|}{V_{h}} \sim \frac{f}{R}$  get simpler Eq.:

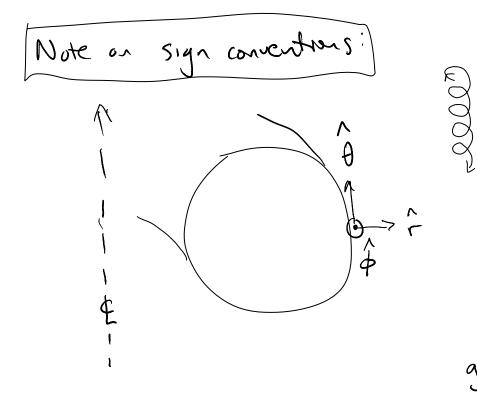
$$V_{II} \hat{b} \cdot \nabla F_{0} - \mu (\hat{b} \cdot \nabla B) \frac{\partial F_{0}}{\partial V_{II}} = 0$$
  
Will consider Equilibrium of the form:  

$$F_{0} (R, V_{II}, \mu) \propto \frac{n_{0}(Y)}{T_{0}^{3/2}(Y)} e^{-\frac{m(\frac{1}{2}V_{II}^{2} + \mu B(X))}{T(Y)}} \propto e^{-\frac{E}{T}}$$
  
Exercise: Plug this in to the previous Eq. + show it is  
a solution.

$$\begin{split} \frac{\partial \tilde{f}}{\partial t} + (v_{\parallel}\hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \tilde{f} + \left(\frac{q}{m}E_{\parallel} - \mu \nabla_{\parallel}B + v_{\parallel}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right)\frac{\partial \tilde{f}}{\partial v_{\parallel}} &= 0 \\ \\ \text{Lmearize:} \quad \tilde{f} = F_{o} + \tilde{f}, \text{ where } F_{o} \text{ satisfies Equilibrium Eq.} \\ \text{Next order Eq:} \\ \frac{\partial \tilde{f}}{\partial t} + \left(v_{\parallel}\hat{\mathbf{b}} + v_{d}\right) \cdot \nabla \tilde{f} - \mu \nabla_{\mu}\beta\frac{\partial \tilde{f}}{\partial v_{\parallel}} &= -\bigvee_{e} \cdot \nabla F_{o} \\ - \left(\frac{q}{m}E_{\mu} + v_{\parallel}(\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot v_{e}\right)\frac{\partial F}{\partial v_{\parallel}} \end{split}$$

$$\left( -\lambda \omega + \lambda v_{\mu} h_{\mu} + \lambda v_{d} \cdot h_{\perp} \right) \widetilde{f} = - v_{E} \cdot \nabla F_{o} - \left( \frac{q}{m} E_{\mu} + v_{\mu} \left( b \cdot \nabla b \right) \cdot v_{E} \right) \frac{\partial F_{o}}{\partial v_{\mu}}$$

$$\frac{\operatorname{Important Subtlety}: F(\underline{R}, \underline{V}_{n}, \underline{P}, \underline{t}) \quad so}{-\underline{V}_{\underline{C}} \cdot \nabla F_{o} = -\underline{V}_{\underline{C}} \cdot \nabla \Big| F_{o} \quad V_{\underline{n}, \underline{P}, \underline{t}} \\ \quad usny \quad F_{o} \propto \frac{n_{o}(r)}{T_{o}^{3/2}} e^{-\frac{(\underline{t} - mv_{u} + mp \cdot B(\underline{X}))}{T_{o}(r)}} \\ \quad w_{ill give terms proportional to } \nabla h_{o} \nabla T_{o}, \underline{d} = \underline{P} \cdot \nabla B \\ \nabla n, terms: -\underline{V}_{\underline{C}} \cdot \nabla F_{o} \Rightarrow + \frac{c}{B} \left( \nabla \underline{P} \times \widehat{b} \cdot \underline{\nabla} \underline{n}_{o} \right) F_{o} \\ p_{o}^{10,idal} = -\frac{c}{B} \cdot \nabla E \cdot \widehat{b} \cdot \widehat{r} \cdot \frac{1}{L_{n}} F_{o} \\ = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} = -\frac{c}{B} \cdot A \widehat{b} \cdot \widehat{F} \cdot \frac{1}{L_{n}} F_{o} \\ \frac{d}{d} \cdot \widehat{F} \cdot \widehat{F$$



With B field out of the page,  
the VB drift for ions is  
downward  

$$V_{\partial} \approx - \frac{\partial}{\partial V_{\pm}} f_{R} \quad (at \theta = 0)$$
  
 $V_{\partial} \approx - \frac{\partial}{\partial V_{\pm}} f_{R} \quad (at \theta = 0)$   
defining  $W_{dv} = h \cdot V_{d}$   
gives convention used in Beer's  
thesis:

$$\omega_{dv} = \omega_d (v_{\parallel}^2 + \mu B) / v_t^2$$
$$\omega_d = -k_{\theta} \rho v_t / R$$

More on Sign Conventions  

$$\sum_{k=1}^{n} \sum_{k=1}^{n} \sum_$$

(Back to RHS of Incarized GK Eq., 4 slides back)  $-\underbrace{v}_{E}\cdot\nabla F_{o}-(\underbrace{\mathbf{q}}_{m}E_{n}+v_{n}(b\cdot\nabla b)\cdot v_{E})\frac{\partial F_{o}}{\partial v_{n}}$ RHS = $\propto + V_{\parallel} \begin{pmatrix} \wedge & & \\ b & \nabla & b \end{pmatrix} \cdot \begin{pmatrix} \wedge & & \\ b & \times \nabla & \overline{\phi} \end{pmatrix}$ part of this ~- c VExb. pVB  $\sim -\nabla \Psi \cdot \left[ p \hat{b} \times \nabla B + v_{ij} \hat{b} \times (\hat{b} \cdot \nabla \hat{b}) \right]$ + curvature drift 7B  $RHS = +i\left(\omega_{xv}^{T} - \omega_{dv} - h_{u}v_{u}\right) \frac{eF}{T} F_{o}$  $\omega_{dv} = \omega_d (v_{\scriptscriptstyle \parallel}^2 + \mu B) / v_t^2$  $\omega_*^T = \omega_* [1 + \eta (v_{\parallel}^2 / 2v_t^2 + \mu B / v_t^2 - 3/2)]$  $\omega_{a} \equiv -\frac{v_{t}}{p} p \left( h_{\theta} \cos \theta + h_{r} \sin \theta \right)$  $\omega_{\star} = h_{\theta} \rho \frac{V_{t}}{I}$   $\eta = \frac{L_{n}}{L_{\tau}}$ 

$$\int_{a}^{2} \int_{a}^{b} \int_{a$$

$$\left( -\kappa \omega + i v_{\parallel} h_{\parallel} + i v_{\vartheta} \cdot h_{\perp} \right) \widetilde{f} = - v_{\varepsilon} \cdot \nabla F_{o} - \left( \frac{q}{m} E_{\parallel} + v_{\parallel} \left( b \cdot \nabla b \right) \cdot v_{\varepsilon} \right) \frac{2F_{o}}{2v_{\parallel}}$$

subst. for RHS  

$$\left( -\omega + i v_{11}h_{11} + i \omega_{dv} \right) \widetilde{f} = -i \left( -\omega_{xv}^{T} + \omega_{dv} + h_{11}v_{11} \right) \frac{e\overline{\Phi}}{T_{o}} F_{o}$$

$$\left[ \widetilde{f} = \frac{-\omega_{xv}^{T} + (h_{11}v_{11} + \omega_{dv})}{\omega - (h_{11}v_{11} + \omega_{dv})} \frac{e\overline{\Phi}}{T_{o}} F_{o} \right]$$

$$N_{o} + e^{i} recover Boltzmann response when h_{11}v_{11} + or \omega_{dv} large$$

$$\widetilde{f} = \frac{-\omega_{xv}^{T} + (h_{1v}v_{1v} + \omega_{dv})}{\omega - (h_{1v}v_{1v} + \omega_{dv})} \frac{e \Phi}{T_{o}} F_{v}$$

(slab "y;" version of ITG requires finite hilver, but not tovordal version),

$$n_{eo} \frac{e\overline{\Psi}}{T_e} = \int d^3 v \frac{-\omega_{\star v}^T + \omega_{av}}{\omega - \omega_{dv}} F_o \frac{e\overline{\Psi}}{T_{vo}}$$

electrons (additional polarization contribution to density gives hip i corrections but not critical for basic ITE.)

$$N_{o} \stackrel{e \neq}{=} = N_{o} \stackrel{e \neq}{=} \int d^{3}v \stackrel{F_{o}}{=} \frac{\omega_{dv} - \omega_{yT}}{\omega - \omega_{dv}}$$

$$"Cold plasma" or "fast wave" approx.  $\omega \gg \omega_{dv}$ 

$$\frac{T_{no}}{T_{eo}} = \int d^{3}v \stackrel{F_{o}}{=} \frac{\omega_{dv} - \omega_{xT}}{\omega} \left(1 + \frac{\omega_{dv}}{\omega} + \cdots\right)$$$$

$$\frac{T_{no}}{T_{eo}} = \int d^{3}_{V} \frac{F_{o}}{h_{o}} \frac{\omega_{\partial v} - \omega_{*T}}{\omega} \left( 1 + \frac{\omega_{dv}}{\omega} + \cdots \right)$$

$$\omega_{dv} = \omega_{d} (v_{\parallel}^{2} + \mu B) / v_{t}^{2} \qquad \omega_{*}^{T} = \omega_{*} [1 + \eta (v_{\parallel}^{2} / 2v_{t}^{2} + \mu B / v_{t}^{2} - 3 / 2)]$$

$$\frac{\omega_{d}}{\omega_{d}} = -k_{\theta} \rho v_{t} / R \qquad \omega_{*} = -k_{\theta} \rho v_{t} / L_{n}$$

$$\int d^{3}_{V} \frac{F_{o}}{h_{o}} \omega_{dv} = \int d^{3}_{V} \frac{F_{o}}{h_{o}} \omega_{d} \left( v_{n}^{2} + \frac{1}{2} v_{\perp}^{2} \right) / v_{t}^{2}$$

$$= 2 \omega_{d}$$

$$\frac{T_{no}}{T_{eo}} = \int \partial_{v}^{3} \frac{F_{o}}{h_{o}} \frac{\omega_{dv} - \omega_{x\tau}}{\omega} \left( 1 + \frac{\omega_{dv}}{\omega} + \cdots \right) \\
\omega_{dv} = \omega_{d} (v_{\parallel}^{2} + \mu B) / v_{t}^{2} \qquad \omega_{*}^{T} = \omega_{*} [1 + \eta (v_{\parallel}^{2} / 2v_{t}^{2} + \mu B / v_{t}^{2} - 3 / 2)] \\
\omega_{d} = -k_{\theta} \rho v_{t} / R \qquad \omega_{*} = -k_{\theta} \rho v_{t} / L_{n} \qquad = \frac{1}{2} v_{\perp}^{2} = \frac{1}{2} \left( v_{x}^{2} + v_{y}^{2} \right) \\
\int \partial_{v}^{3} \frac{F_{o}}{h_{o}} \omega_{x}^{T} = \omega_{*} \left( 1 + \eta \left( \frac{1}{2} + 1 - \frac{3}{2} \right) \right) = \omega_{x} \\
\int \partial_{v}^{3} \frac{F_{o}}{h_{o}} \omega_{dv}^{2} = \int \partial_{v}^{3} \frac{F_{o}}{h_{o}} \omega_{d}^{2} \left[ v_{u}^{4} + 2v_{u}^{2} \frac{1}{2} v_{\perp}^{2} + \frac{1}{4} \left( v_{x}^{2} + v_{y}^{2} \right)^{2} \right] \frac{1}{v_{t}^{4}} \\
= \omega_{d}^{2} \left[ 3 + 2 \cdot \frac{1}{2} \left( 1 + 1 \right) + \frac{1}{4} \left( \left( v_{x}^{4} + 2v_{x}^{2} v_{y}^{2} + v_{y}^{4} \right) \right) \right] \\
v_{t}^{4}$$

$$\frac{T_{no}}{T_{eo}} = \int d^3 v \frac{F_o}{h_o} \frac{\omega_{dv} - \omega_{\star T}}{\omega} \left( 1 + \frac{\omega_{dv}}{\omega} + \cdots \right)$$

$$\omega_{dv} = \omega_d (v_{\parallel}^2 + \mu B) / v_t^2 \qquad \omega_*^T = \omega_* [1 + \eta (v_{\parallel}^2 / 2v_t^2 + \mu B / v_t^2 - 3/2)]$$
  
$$\omega_d = -k_{\theta} \rho v_t / R \qquad \omega_* = -k_{\theta} \rho v_t / L_n \qquad \qquad = \frac{1}{2} v_{\perp}^2 = \frac{1}{2} \left( v_{\chi}^2 + v_{\chi}^2 \right)$$

$$\int d^{3}v \frac{F_{o}}{n_{o}} \omega_{dv} \omega_{\star}^{T} = \omega_{d} \omega_{\star} \begin{cases} 2 \\ + \eta \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{N_{o}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \\ + \eta \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \\ + \eta \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{N_{o}} \left( \frac{V_{11}^{2} + \frac{1}{2}V_{1}^{2}}{V_{t}^{2}} \right) \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{t}^{2} - \frac{3}{2}V_{t}^{2} \right) \int d^{3}v \frac{F_{o}}{V_{t}^{2}} \left( \frac{1}{2}V_{11}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \int d^{3}v \frac{F_{o}}{V_{t}^{2}} \left( \frac{1}{2}V_{1}^{2} + \frac{1}{2}V_{1}^{2} - \frac{3}{2}V_{t}^{2} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \right) \frac{V_{t}^{2}}{V_{t}^{2}} \frac{V_{t}^{2}}{V_{t}^{2}} \frac{V_{t}^{2}}{V_{t}^{2}} + \frac{1}{2}V_{t}^{2} + \frac{1}{2}V_{t}^$$

$$= \omega_{d}\omega_{*} \left\{ 2 + \eta \left[ \frac{1}{2} 3 + \frac{1}{2} 2 - \frac{3}{2} + \frac{1}{2} \cdot 2 \cdot \frac{1}{2} + \frac{1}{4} 8 - \frac{1}{2} \cdot 2 \cdot \frac{3}{2} \right] \right\}$$

$$\int d^{3}v \frac{F_{o}}{n_{o}} \omega_{dv} \omega_{\star}$$

$$= \omega_{d} \omega_{\star} \left\{ 2 + \eta \left[ \frac{1}{2} \frac{3}{3} + \frac{1}{2} 2 - \frac{3}{2} + \frac{1}{2} \cdot 2 \cdot \frac{1}{4} + \frac{1}{4} 8 - \frac{1}{2} \cdot 2 \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{2} \cdot 2 \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{4} - \frac{1}{2} \cdot \frac{1}{2} \cdot \frac{1}{2} + \frac{1}{4} - \frac{1}{4$$

This defines a dispersion relation w us. h

$$\frac{T_{vo}}{T_{eo}} = 2 \frac{\omega J}{\omega} - \frac{\omega_{\star}}{\omega} + 7 \frac{\omega_{d}}{\omega^{2}} - 2 \frac{\omega_{d}\omega_{\star}(1+\eta)}{\omega^{2}}$$

Consider the flat density limit: 
$$\nabla n \rightarrow 0$$
, but  $\nabla T \neq 0$   
 $\omega_* = -h_{\theta} \rho \frac{V_t}{L_n} \rightarrow 0$ 
 $\eta = \frac{1}{T} \nabla T = \frac{L_n}{L_T} \rightarrow \infty$ 

$$\omega_{*}\eta = -h_{\theta}\rho \frac{V_{t}}{L_{n}} \frac{L_{n}}{L_{\tau}} \equiv \overline{\omega}_{*\tau}$$

$$\omega^{2} \frac{T_{iv}}{T_{e_{o}}} = 2 \omega_{d} \omega + 2 \omega_{d} \overline{\omega_{x_{T}}} - 7 \omega_{d}^{2} = 0$$

$$\omega = 2 \omega_{d} \pm \sqrt{4 \omega_{a}^{2}} - 4 \frac{T_{iv}}{T_{e_{o}}} \left(2 \omega_{d} \overline{\omega_{x_{T}}} - 7 \omega_{d}^{2}\right)$$

$$2 \left(T_{iv}/T_{e_{o}}\right)$$

From last page:  

$$W = 2W_{d} \pm \sqrt{4W_{a}^{2} - 4\frac{T_{iv}}{T_{e_{o}}}(2W_{d}W_{*T} - 7W_{d}^{2})}$$

$$2(T_{iv}/T_{e_{o}})$$

Consider large temperature gradient limit:  $\omega_{*T} \propto \nabla T$  f Growth rate:

$$Y = \frac{\sqrt{2} \omega_{d} \overline{\omega_{xT}}}{\sqrt{T_{x0}/T_{e0}}} = \frac{\sqrt{2} h_{\theta} \rho_{i}}{\sqrt{T_{x0}/T_{e0}}} \frac{V_{t,i}}{\sqrt{RL_{T}}}$$
  
Fundamental scaling of bad-curvature driven instabilities.

Go back to general D.R.:  

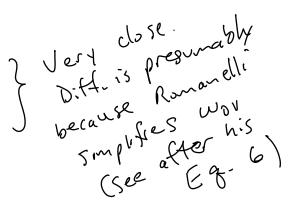
$$\begin{aligned}
\omega &= \frac{2 \omega_{\theta} \pm \sqrt{4 \omega_{a}^{2} - 4 \frac{T_{iv}}{T_{e_{0}}} \left(2 \omega_{a} \overline{\omega}_{*\tau} - 7 \omega_{a}^{2}\right)}{2 \left(T_{iv} / T_{e_{0}}\right)} \\
&= 2 \omega_{a} \pm \sqrt{\left(4 + 28 \frac{T_{av}}{T_{e_{0}}}\right) \omega_{a}^{2} - 8 \frac{T_{ao}}{T_{e_{0}}} \omega_{a} \overline{\omega}_{*\tau}}}{2 \left(T_{ao} / T_{e_{0}}\right)} \\
\text{Instability exists if} \\
8 \frac{T_{ao}}{T_{e_{0}}} \omega_{\theta} \overline{\omega}_{*\tau} > \omega_{a}^{2} \left(4 + 28 \frac{T_{av}}{T_{e_{0}}}\right) \\
&= \frac{1}{R} \frac{1}{L_{T}} > \frac{1}{R^{2}} \left(\frac{1}{2} \frac{T_{e_{0}}}{T_{e_{0}}} + \frac{1}{2} 7\right) \\
&= \frac{1}{R} \frac{1}{L_{T}} > \frac{1}{2} \left(7 + \frac{T_{e_{0}}}{T_{e_{0}}}\right)
\end{aligned}$$

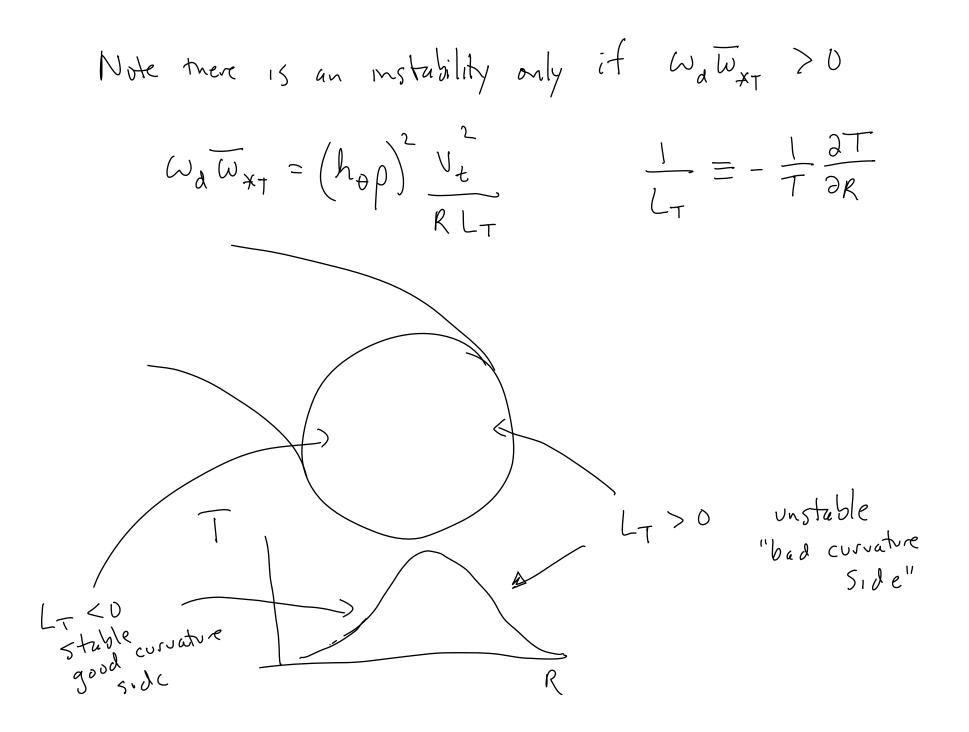
Compare w/ Romanelli 1990 (Eq. 12):  

$$\eta_{i} = (\frac{3}{3} + \tau/4)2\epsilon_{n}$$
or
$$\frac{L_{n}}{L_{t}} = (\frac{5}{3} + \frac{1}{4} + \frac{Te}{T_{i}})^{2} \frac{L_{n}}{R}$$

$$\frac{R}{L_{t}} = \frac{10}{3} + \frac{1}{2} + \frac{Teo}{T_{io}}$$

$$= 3.33 + 0.5 + \frac{Teo}{T_{io}}$$
vs. my
$$\frac{R}{L_{t}} = 3.5 + 0.5 + \frac{Teo}{T_{io}}$$





Why does this get the 
$$\frac{T_{io}}{T_{eo}}$$
 dependence of  
 $\frac{R}{L_{torit}}$  wrong? More accurate:  $\frac{R}{L_{t}} \cdot \frac{R}{L_{torit}} = \frac{4}{3}(1+\frac{T_{io}}{T_{eo}})$   
Because near marginal studielity, the expansion  
of the resumpt denomination  
 $\frac{1}{W-W_{dV}} \approx \frac{1}{W}(1+\frac{W_{dV}}{W}+...)$ 

breaks down, since waw a neur Morginal stability...

More general result for threshold for metability:  

$$\frac{R_{o}}{L_{torit}} = M_{ax} \left[ \left( 1 + \frac{T_{i}}{T_{e}} \right) \left( 1.33 + 1.91 \frac{s}{q} \right) \left( 1 - 1.5 \frac{r}{R} \right) \left( 1 + 0.3 \frac{rdk}{dr} \right) \right]$$

$$0.8 \frac{R_{o}}{L_{h}} \right]$$

## **ITG References**

- Mike Beer's Thesis 1995 http://w3.pppl.gov/~hammett/collaborators/mbeer/afs/thesis.html
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- Biglari, Diamond, Rosenbluth, Phys. Fluids B 1989
- Jenko, Dorland, Hammett, PoP 2001
- Candy & Waltz, PRL ...
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- ...
- Earlier history:
  - slab eta\_i mode: Rudakov and Sagdeev, 1961
  - Sheared-slab eta\_i mode: Coppi, Rosenbluth, and Sagdeev, Phys. Fluids 1967
  - Toroidal ITG mode: Coppi and Pegoraro 1977, Horton, Choi, Tang 1981, Terry et al. 1982, Guzdar et al. 1983... (See Beer's thesis)