

# NSTX Research Highlights and Progress Toward NSTX Upgrade\*

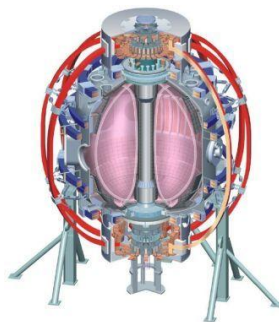
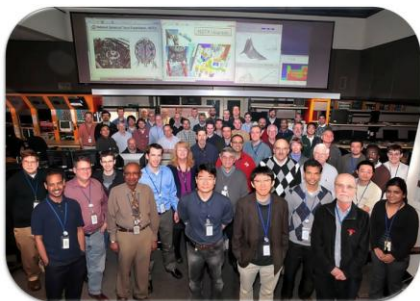
**J. Menard,**

*J. Canik, J. Chrzanowski, M. Denault, L. Dudek, T. Egebo, S. Gerhardt, T. Gray, W. Guttenfelder, J. Hosea, S. Kaye, C. Kessel, E. Kolemen, R. Maingi, C. Neumeyer, M. Ono, E. Perry, R. Ramakrishnan, R. Raman, Y. Ren, S. Sabbagh, M. Smith, R. Strykowski, V. Soukhanovskii, T. Stevenson, G. Taylor, P. Titus, K. Tresemer, M. Viola, M. Williams, R. Woolley, A. Zolfaghari, and the NSTX Team*

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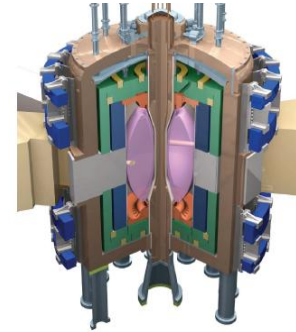


# Outline

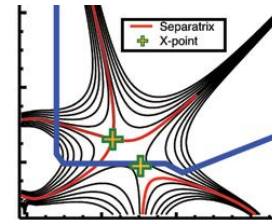
- **NSTX Mission**
- **Motivation for NSTX Upgrade**
- **NSTX Research Highlights and Upgrade Design Progress**
- **Summary**

# NSTX Mission Elements

- Advance ST as candidate for Fusion Nuclear Science Facility (FNSF)
- Develop solutions for plasma-material interface
- Advance toroidal confinement physics for ITER and beyond
- Develop ST as fusion energy system



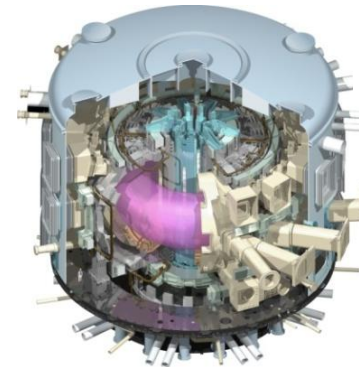
*ST-FNSF*



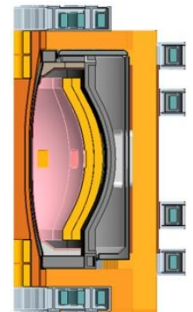
*"Snowflake"*



*Lithium*



*ITER*



*ST Pilot Plant*

# High-Priority Research Areas for ST-FNSF

ReNeW Thrust 16 (2009): “Develop the ST to advance fusion nuclear science”

1. Develop **MA-level plasma current formation and ramp-up**
2. Advance **innovative magnetic geometries, first wall solutions**
3. Understand **ST confinement and stability** at fusion-relevant parameters
4. Develop **stability control techniques** for long-pulse, disruption-free ops
5. **Sustain current, control profiles** with beams, waves, pumping, fueling
6. Develop normally-conducting radiation-tolerant **magnets** for ST applications
7. **Extend ST performance** to near-burning-plasma conditions

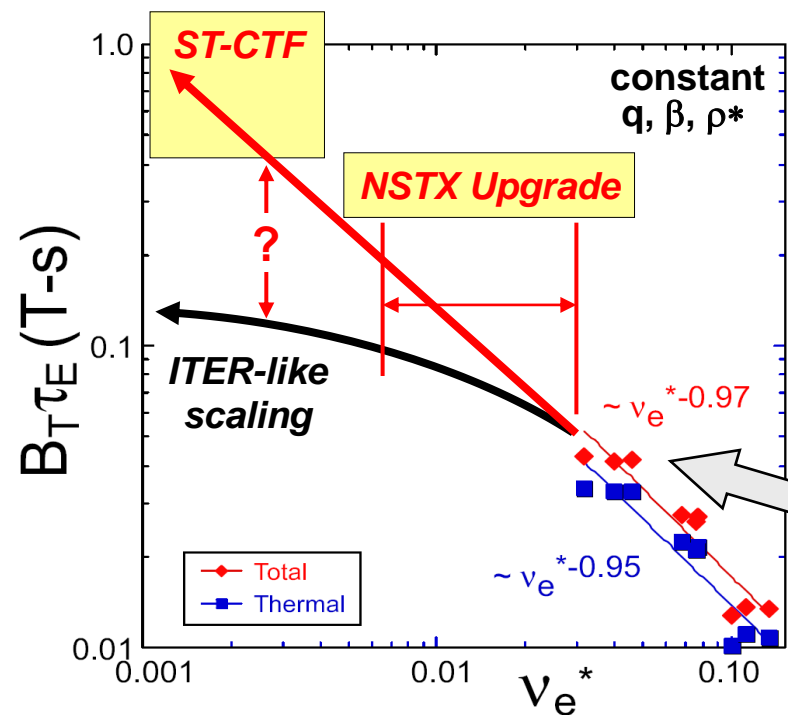
**This talk will focus on how NSTX and NSTX Upgrade address the ST-FNSF physics research needs (1-5) above**

# Access to reduced collisionality is needed to understand underlying causes of ST transport, scaling to next-steps

- Future ST's are projected to operate at 10-100x lower normalized collisionality  $\nu^*$

**Electron collisionality  $\nu_e^* \propto n_e / T_e^2$**

- Conventional tokamaks observe weak inverse dependence of confinement on  $\nu^*$



**STs observe much stronger  $\nu^*$  scaling**

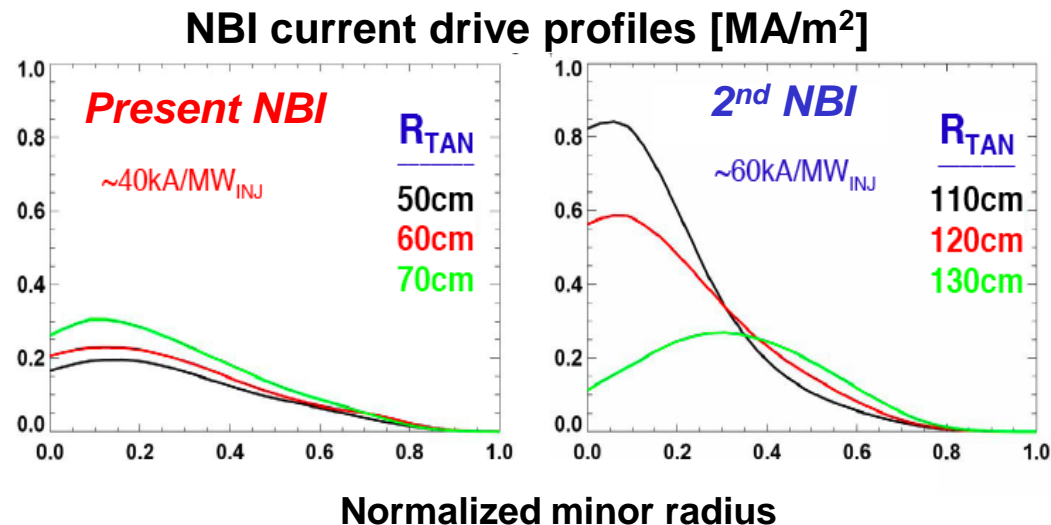
- Does favorable scaling extend to lower  $\nu^*$  ?
- What modes dominate e-transport in ST ?

- **NSTX H-mode thermal confinement scaling** differs from higher aspect ratio scaling:  
 $\tau_{E,NSTX} \propto B_T^{0.9} I_p^{0.4} \rightarrow$  strong  $B_T$  scaling       $\tau_{E,98y,2} \propto B_T^{0.15} I_p^{0.93} \rightarrow$  weak  $B_T$  scaling

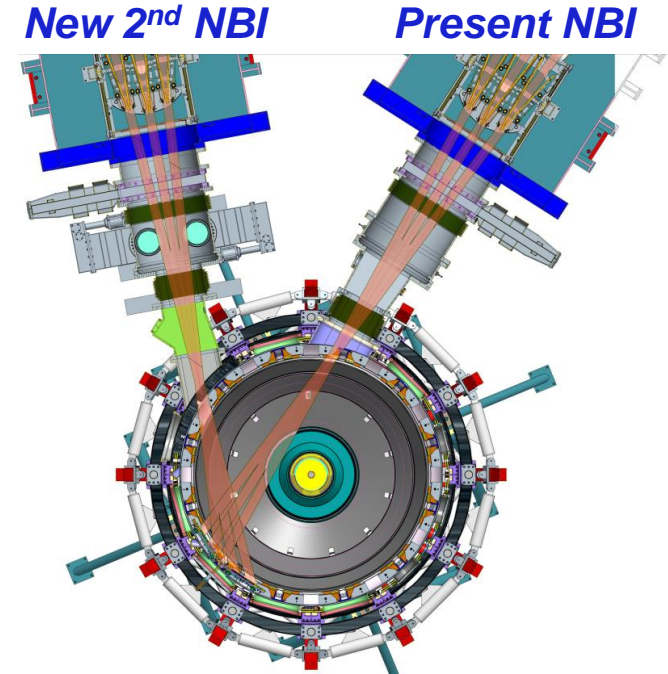
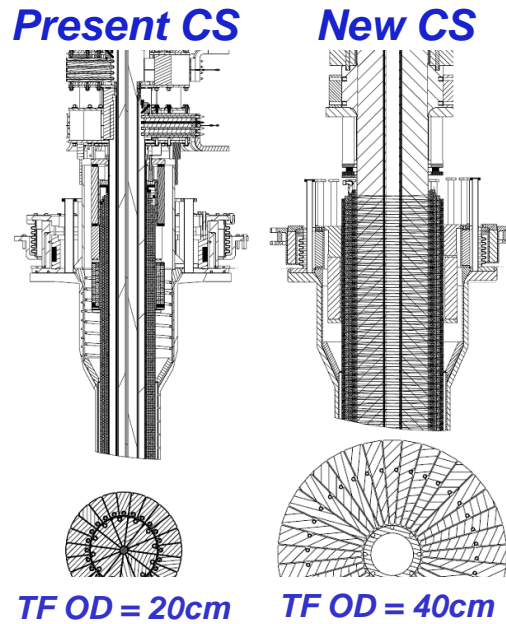
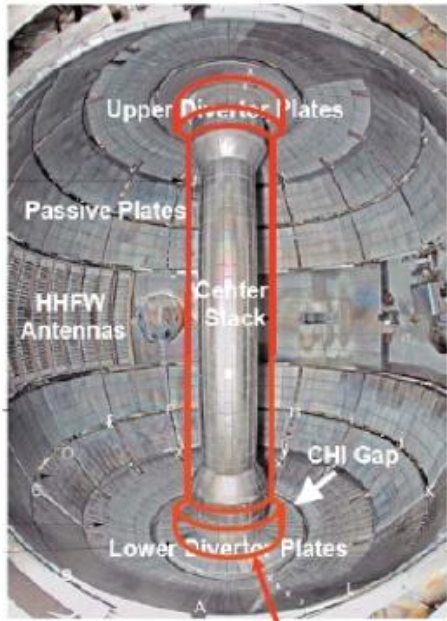
• **Upgrade:** Double field and current for 3-6x decrease in collisionality  
 $\rightarrow$  require 3-5x increase in pulse duration for profile equilibration

# Increased auxiliary heating and current drive are needed to fully exploit increased field, current, and pulse duration

- Higher heating power to access high  $T$  and  $\beta$  at low collisionality
  - Need additional 4-10MW, depending on confinement scaling
- Increased external current drive to access and study 100% non-inductive
  - Need 0.25-0.5MA compatible with conditions of ramp-up and sustained plasmas
- **Upgrade: double neutral beam power + more tangential injection**
  - More tangential injection  $\rightarrow$  up to 2 times higher efficiency, current profile control
  - ITER-level high-heat-flux plasma boundary physics capabilities & challenges



# NSTX Upgrade consists of two major elements that together bridge the device and performance gaps toward next-steps



**Outline of new center-stack (CS)**

	<b>NSTX</b>	<b>NSTX Upgrade</b>	<b>Fusion Nuclear Science Facility</b>
Aspect Ratio = $R_0 / a$	$\geq 1.3$	$\geq 1.5$	$\geq 1.5$
Plasma Current (MA)	1	2	4 $\rightarrow$ 10
Toroidal Field (T)	0.5	1	2-3
P/R, P/S (MW/m, m <sup>2</sup> )	10, 0.2*	20, 0.4*	30 $\rightarrow$ 60, 0.6 $\rightarrow$ 1.2

\* Includes 4MW of high-harmonic fast-wave (HHFW) heating power

# Center Stack Upgrade analysis and design are largely complete, and R&D activities are underway

**B and J each increase 2x → electromagnetic forces increase 4x**

Simpler Inner TF design  
(single layer of TF conductors)

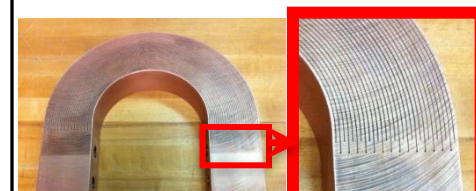
Improved Joint Design

OH coil wound on TF  
(with 0.1" gap)

Reinforced Coil Supports

Existing outer TF  
WITH water cooling

**TF Flex Strap R&D**



EDM  
Process



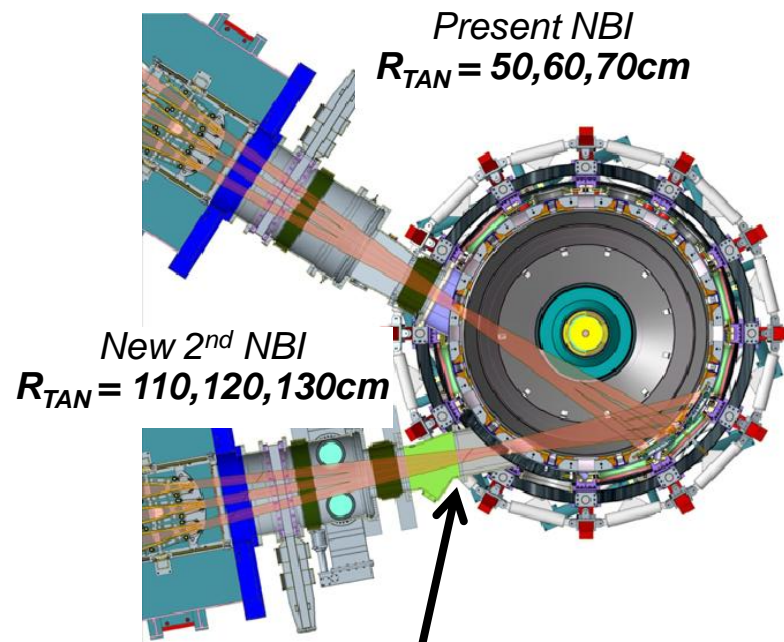
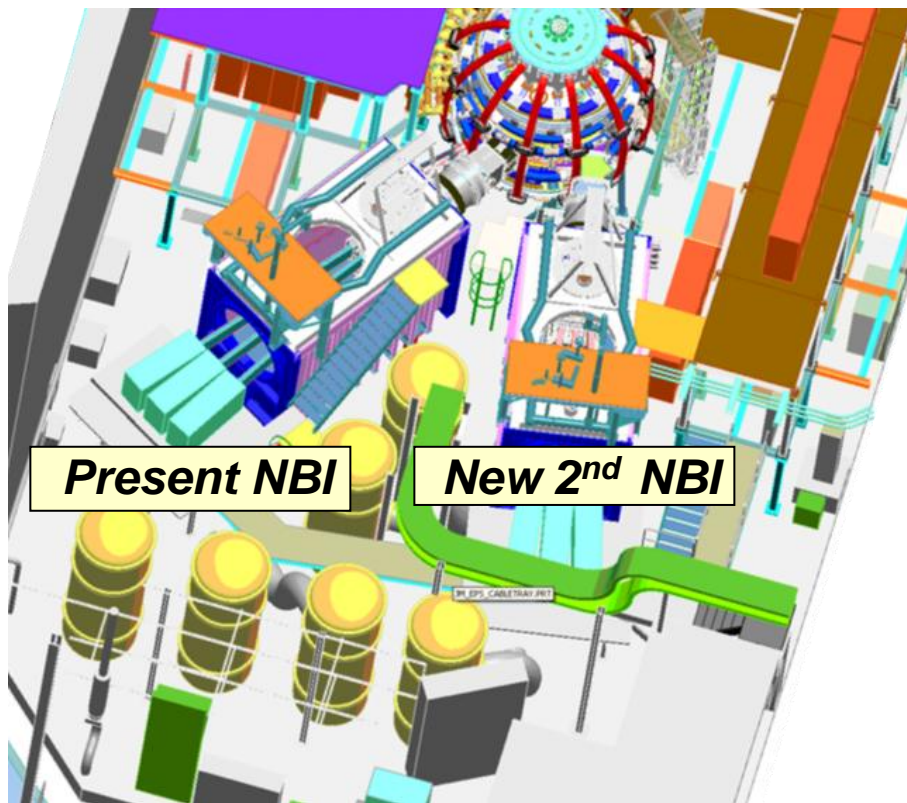
Successfully Tested  
to 300,000 cycles

Clipping Source:  
On-Demand Video Repository (ODV)

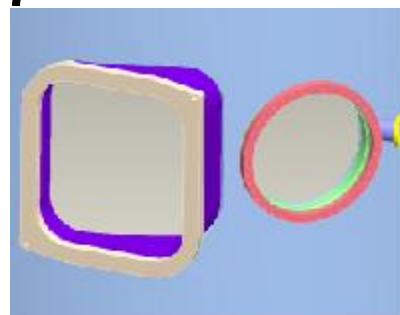


# 2nd NBI requires relocation of a TFTR NBI system to NSTX, diagnostic relocations, new port for more tangential NBI

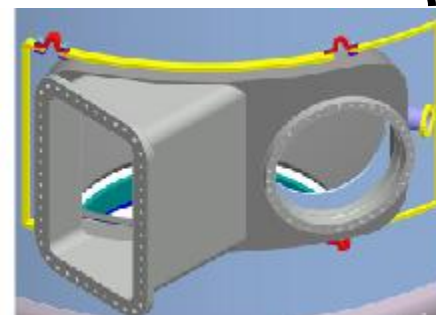
**NSTX**



- Decontamination of 2<sup>nd</sup> Beam line successfully completed in 2010
- Reassembly of 2<sup>nd</sup> Beam line has started



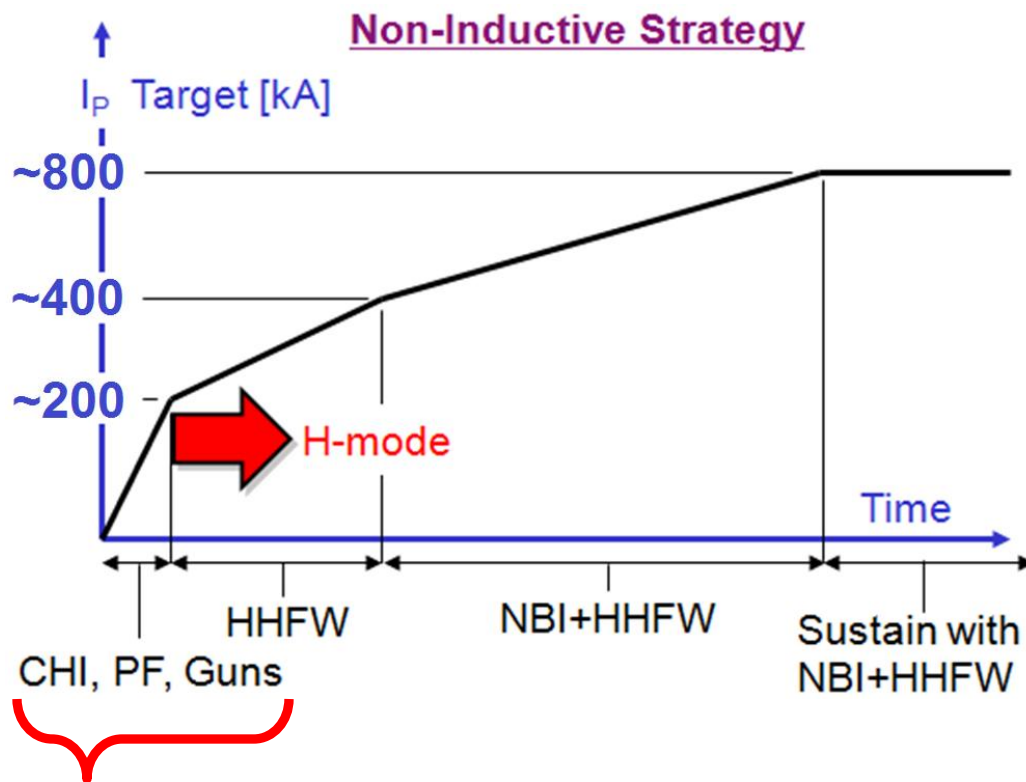
**Original NBI Port**



**New NBI Port**

# Plasma initiation with small or no transformer is unique challenge for ST-based Fusion Nuclear Science Facility

ST-FNSF has no/small central solenoid

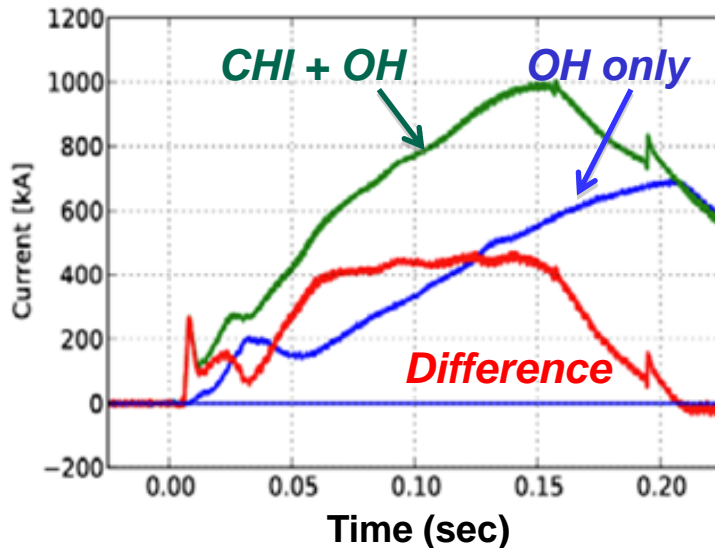
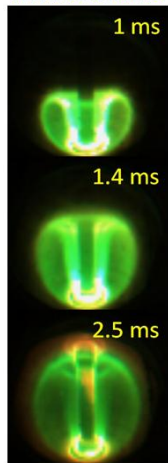


- Near-term NSTX Goal: Generate ~0.3-0.4MA full non-inductive start-up with Coaxial Helicity Injection + fast wave heating + NBI (need Upgrade)
- Upgrade goal: Provide physics basis for non-inductive ramp-up to high performance 100% non-inductive ST plasma → prototype FNSF

# Achieved substantial progress on Coaxial Helicity Injection (CHI) and fast wave heating of low-current plasmas in 2010

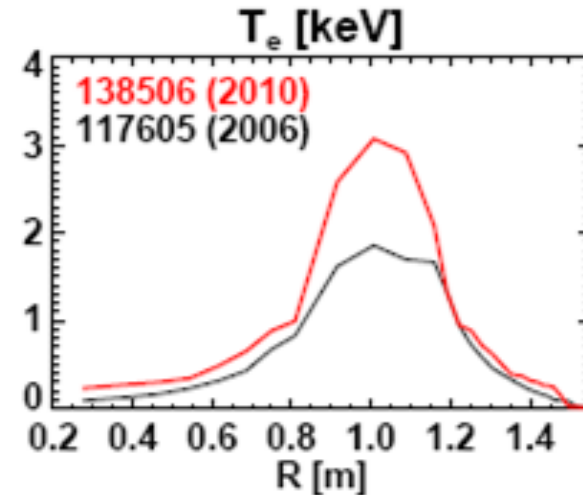
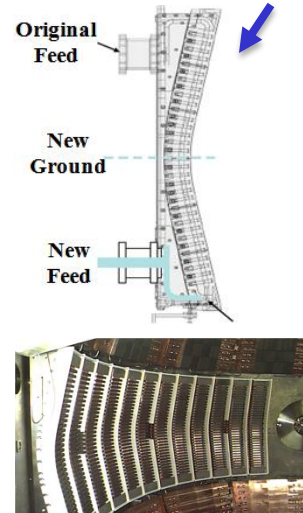
- Early in shot: produce 150-200kA
- Generated 1MA using 40% less flux than induction-only case
  - Low  $I_i \approx 0.35$ , and high elongation  $> 2$ 
    - suitable for advanced scenarios

Time after CHI starts



- CHI-driven current scales linearly with  $B_T$  → **2x higher in Upgrade**

- Achieved high  $T_e(0) \sim 3\text{keV}$  at  $I_p=300\text{kA}$  w/ only 1.4MW of HHFW
  - Previous best was  $T_e(0) \sim 1.5\text{keV}$  at twice the RF power
  - Enabled by 2009 antenna upgrades

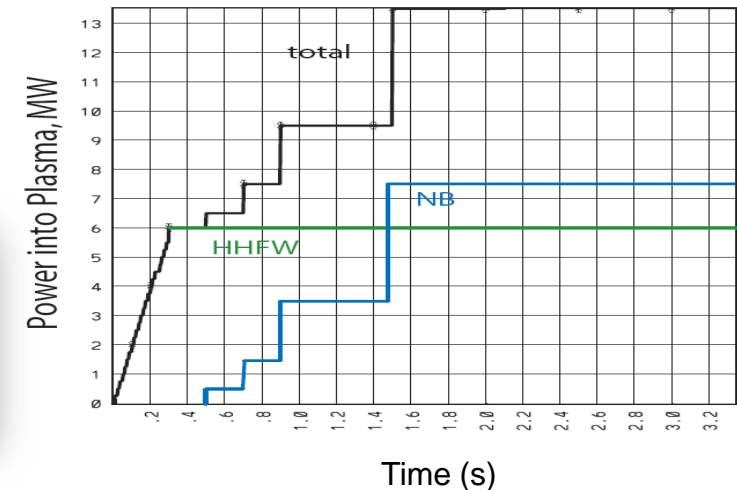
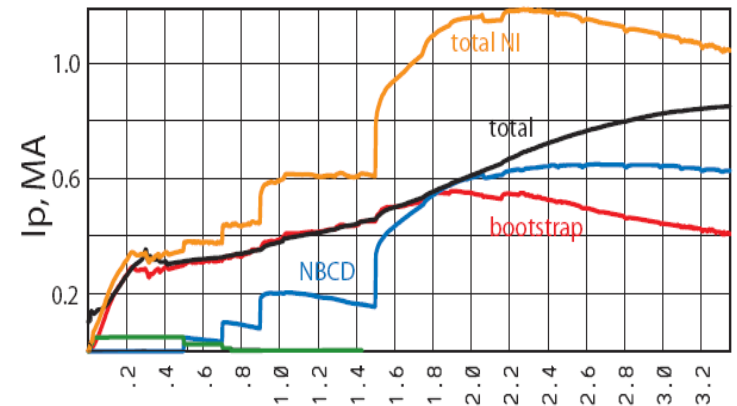
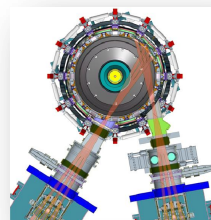
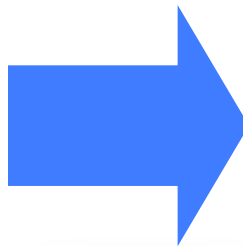
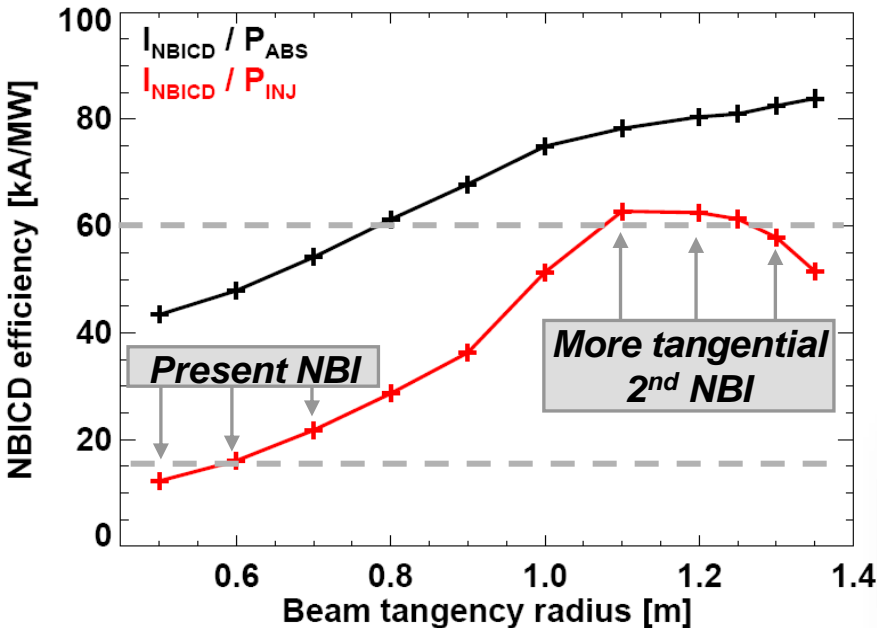


- Non-inductive fraction  $\sim 60-70\%$  with 25-30% from RFCD from high  $T_e(0)$
- **Projects to  $\sim 100\%$  NI at  $P_{RF} = 3-4\text{MW}$**

# Non-inductive ramp-up from ~0.4MA to ~1MA projected to be possible with new CS + more tangential 2<sup>nd</sup> NBI

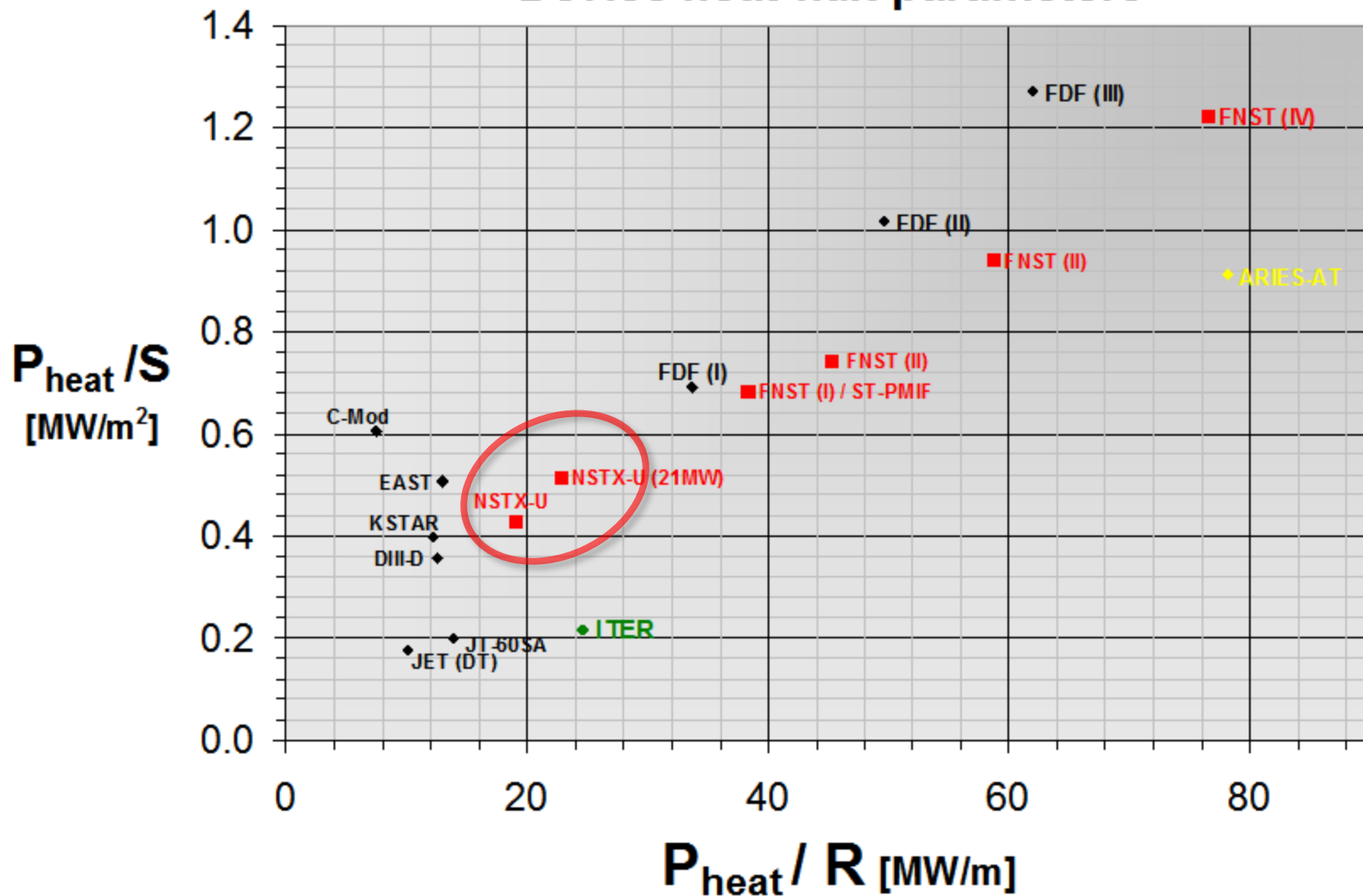
- New CS provides higher TF (improves stability), 3-5s needed for J(r) equilibration
- More tangential injection provides 3-4x higher CD at low  $I_p$ :
  - 2x higher absorption (40→80%) at low  $I_p = 0.4\text{MA}$
  - 1.5-2x higher current drive efficiency

$E_{\text{NBI}} = 100\text{keV}$ ,  $I_p = 0.40\text{MA}$ ,  $f_{\text{GW}} = 0.62$   
 $\bar{n}_e = 2.5 \times 10^{19}\text{m}^{-3}$ ,  $\bar{T}_e = 0.83\text{keV}$



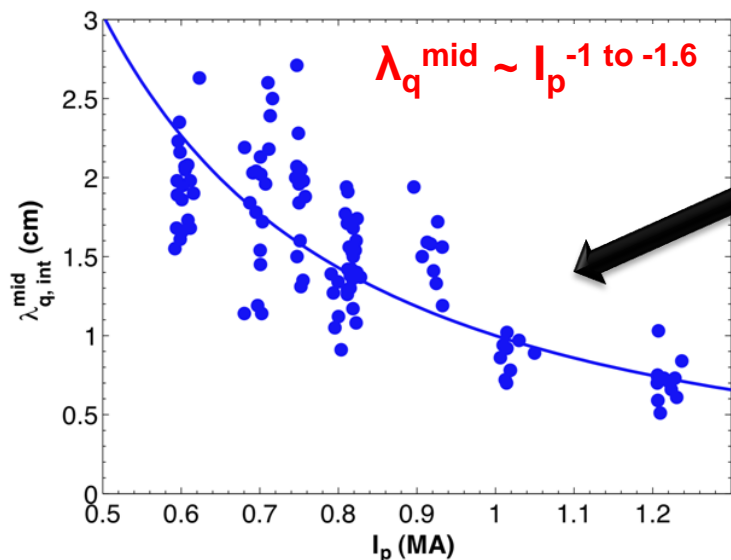
# NSTX Upgrade will extend normalized divertor and first-wall heat-loads much closer to FNS and Demo regimes

## Device heat-flux parameters



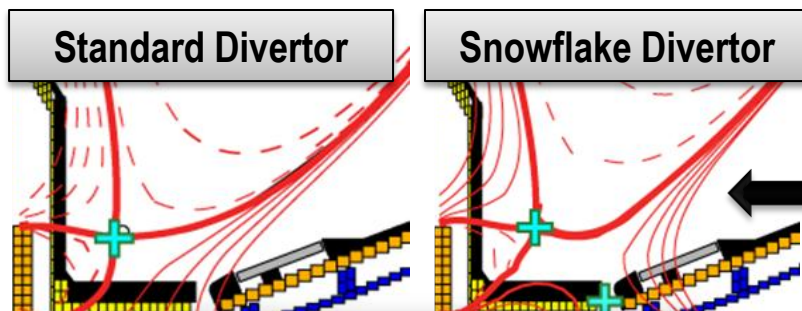
# NSTX has contributed strongly to divertor heat flux width studies\*, and is developing new heat-flux mitigation methods

\*Joint Research Milestone (3 U.S. Facilities)

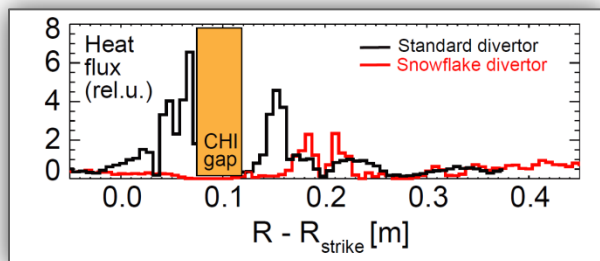


- Divertor heat flux width decreases with increased plasma current  $I_p$ 
  - Potentially major implications for ITER

→ **NSTX Upgrade with conventional divertor projects to very high peak heat flux up to 30-45MW/m<sup>2</sup>**



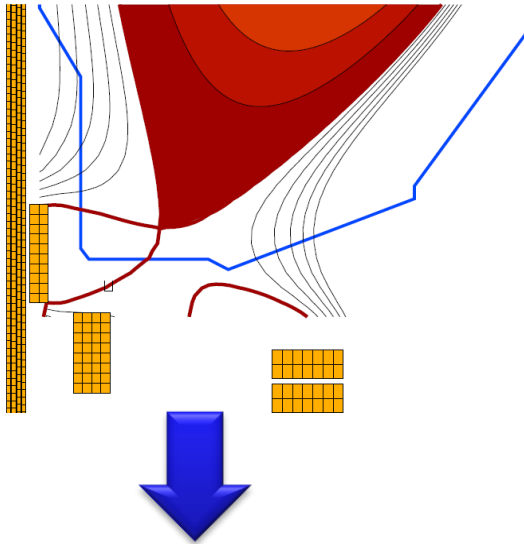
- Divertor heat flux inversely proportional to flux expansion over a factor of five
- **Snowflake** → high flux expansion 40-60, larger divertor volume and radiation



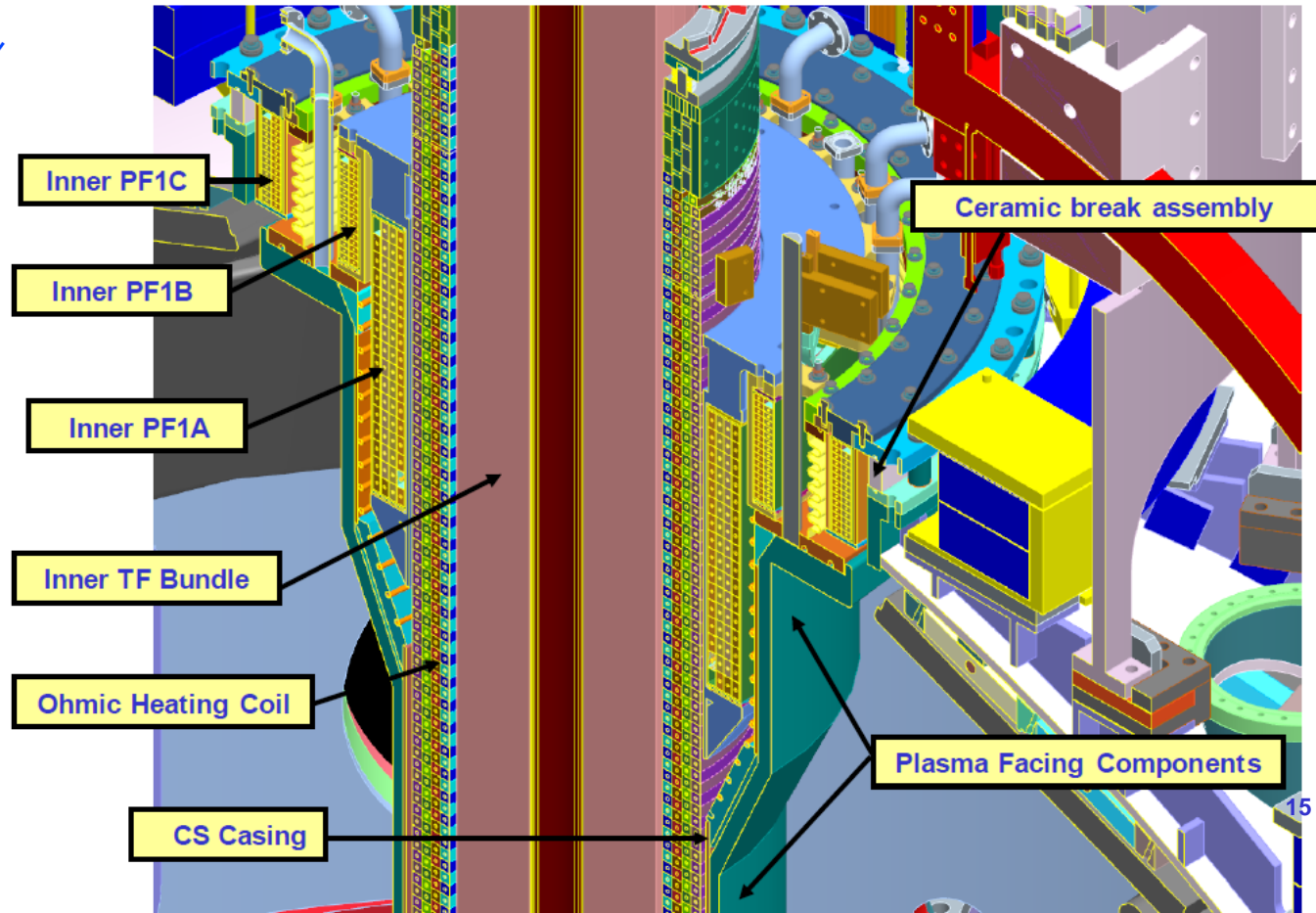
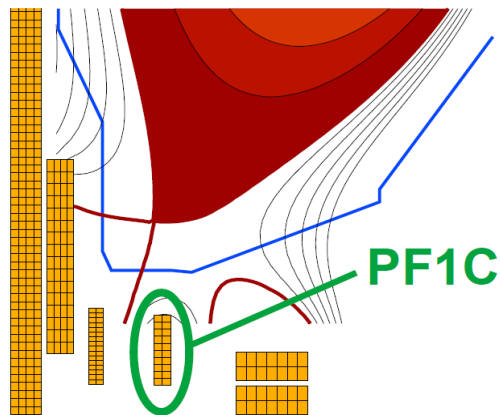
→ **U/D balanced snowflake divertor projects to acceptable heat flux < 10MW/m<sup>2</sup> in Upgrade at highest expected  $I_p = 2\text{MA}$ ,  $P_{\text{AUX}}=10-15\text{MW}$**

# Upgrade CS design provides additional coils for flexible and controllable divertor including snowflake, and supports CHI

## NSTX Snowflake

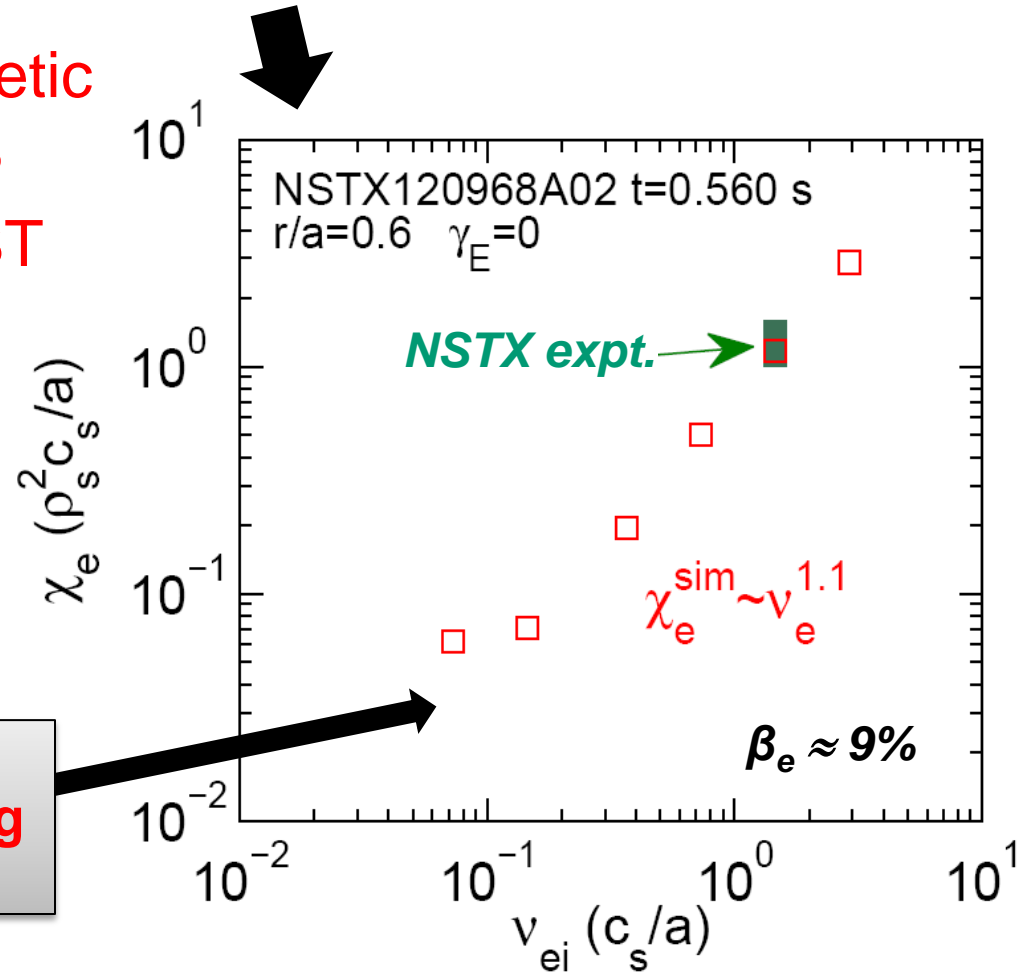


## NSTX-U Snowflake



# New NSTX turbulence simulations are advancing the understanding of ST energy confinement

- Non-linear gyrokinetic turbulence simulations of micro-tearing instabilities predict  $\chi_e \propto v_e^* \Rightarrow \tau_E \propto 1/v_e^*$
- Predominantly electromagnetic turbulence – result of high  $\beta$
- Candidate explanation for ST confinement scaling

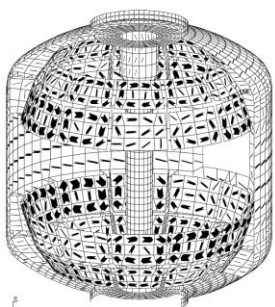


**Lower  $v_e^*$  accessible in Upgrade can clarify roles of micro-tearing vs. ETG, TEM in ST e-transport**



# NSTX is 1<sup>st</sup> tokamak to implement advanced resistive wall mode state-space controller, utilized it to sustain high $\beta_N \sim 6$

## Full 3-D model



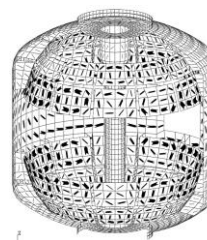
**-3000+ states**



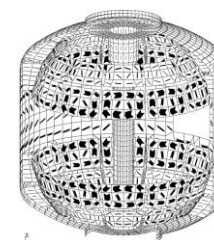
## State reduction (< 20 states)

RWM eigenfunction (2 phases, 2 states)

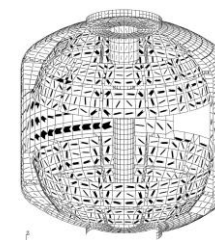
$(\hat{x}_1, \hat{x}_2)$



$\hat{x}_3$



$\hat{x}_4$



$\hat{x}_N$

truncate

- Device  $R, L$ , mutual inductances
- Instability  $B$  field / plasma response
- Modeled sensor response

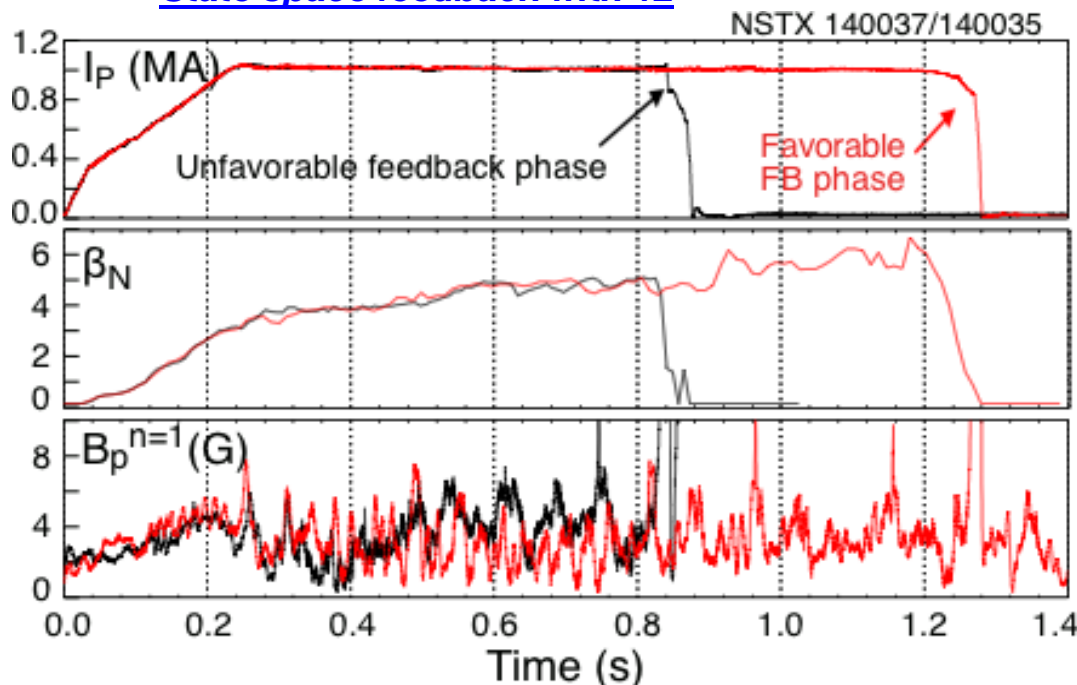
### Controller can compensate for wall currents

- Including mode-induced current
- Examined for ITER

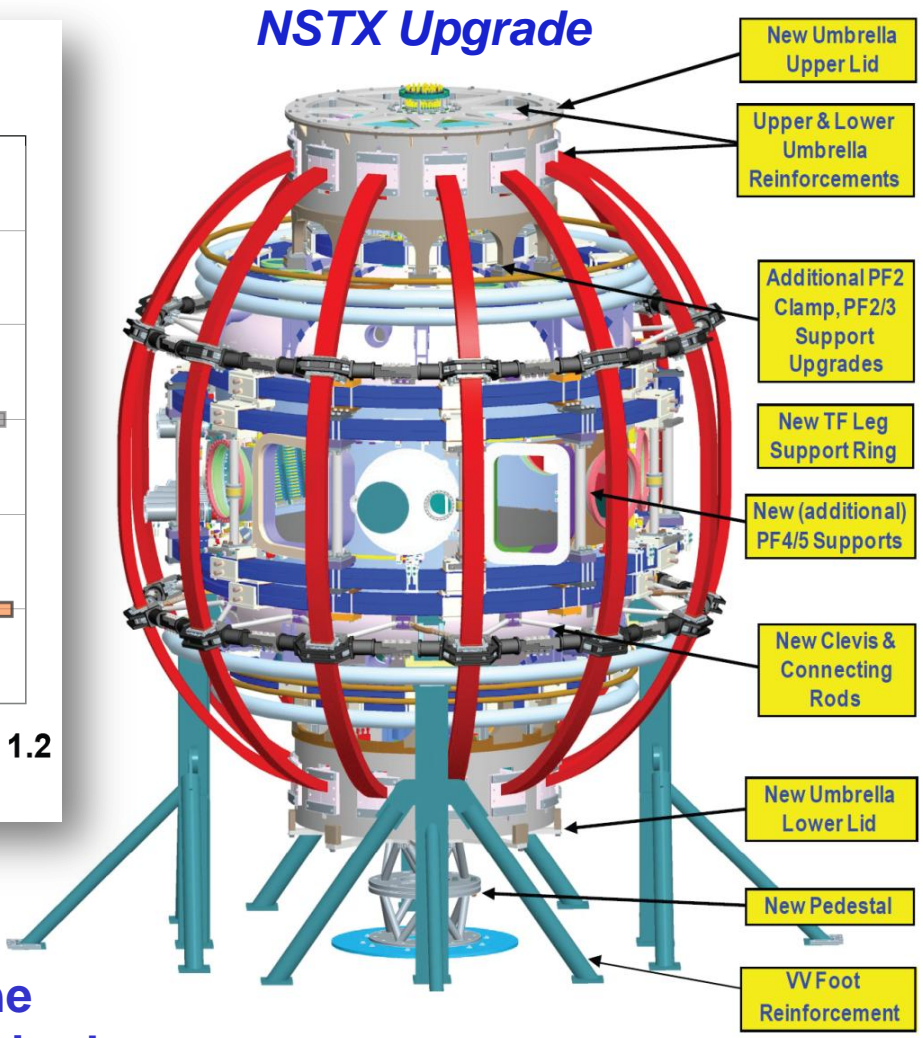
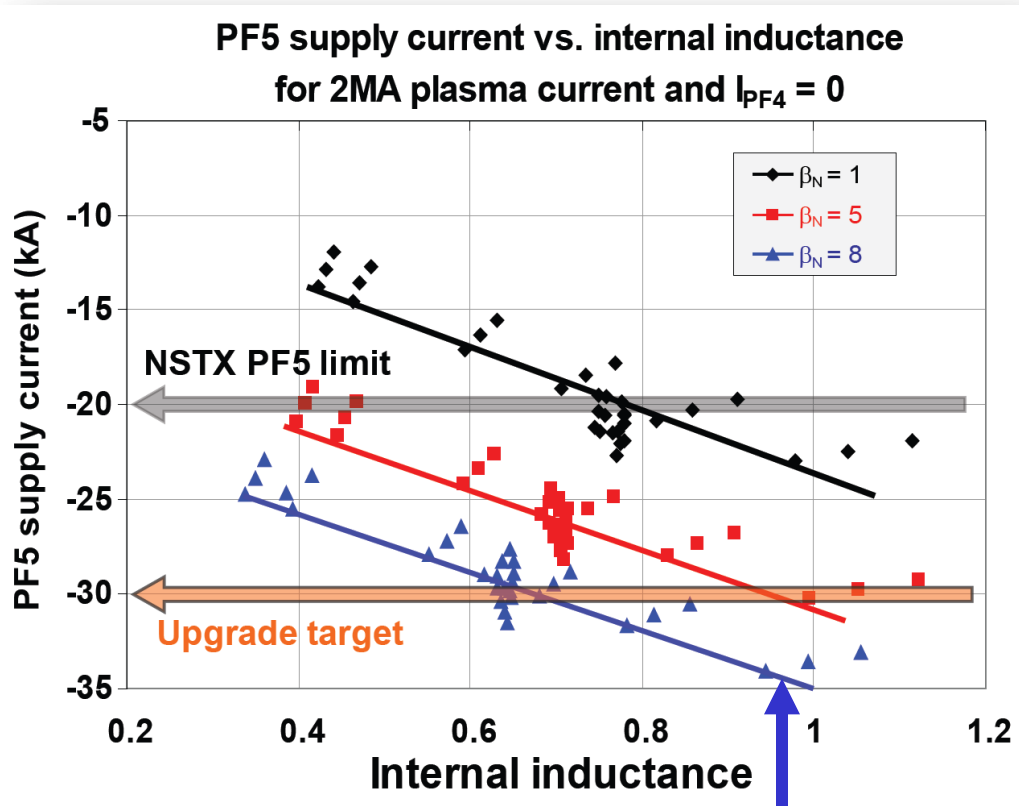
### Successful initial experiments

- Suppressed disruption due to  $n = 1$  applied error field
- Best feedback phase produced long pulse,  $\beta_N = 6.4$ ,  $\beta_N / I_i = 13$

## State space feedback with 12



# Upgrade structural enhancements designed to support high $\beta$ at full $I_p = 2\text{MA}$ , $B_T=1\text{T}$ : $\beta_N = 5, I_i \leq 1$ and $\beta_N = 8, I_i \leq 0.6$



High  $I_i$ , high- $\beta_N$  scenarios determine the maximum vertical field (PF5) current required

# In 2009-10, NSTX demonstrated sustained high-elongation configurations over a range of currents and fields

**High- $\beta_T$**   
 **$q^*=2.8$**

$B_T=0.44 T$   
 $I_P=1100 kA$

**Long Pulse**  
 **$q^*=3.9$**

$B_T=0.38 T$   
 $I_P=700 kA$

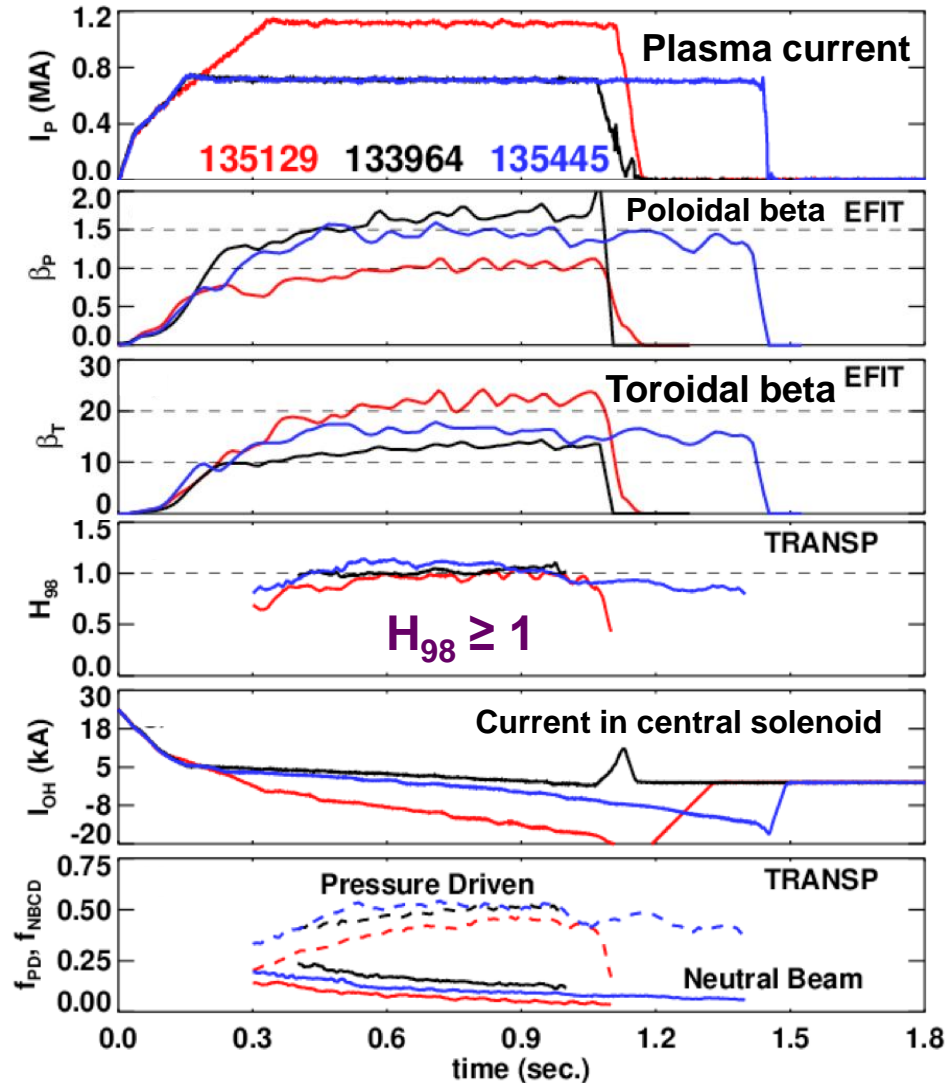
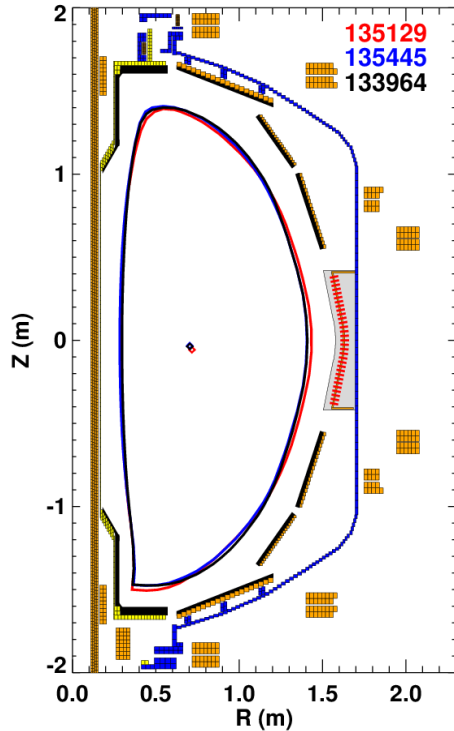
**High- $\beta_P$**   
 **$q^*=4.7$**

$B_T=0.48 T$   
 $I_P=700 kA$

$$q^* = \frac{\varepsilon(1 + \kappa^2)\pi a B_{T0}}{\mu_0 I_P}$$

$\kappa \sim 2.6-2.7$   
 $\delta \sim 0.8$

**Double Null**

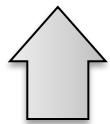
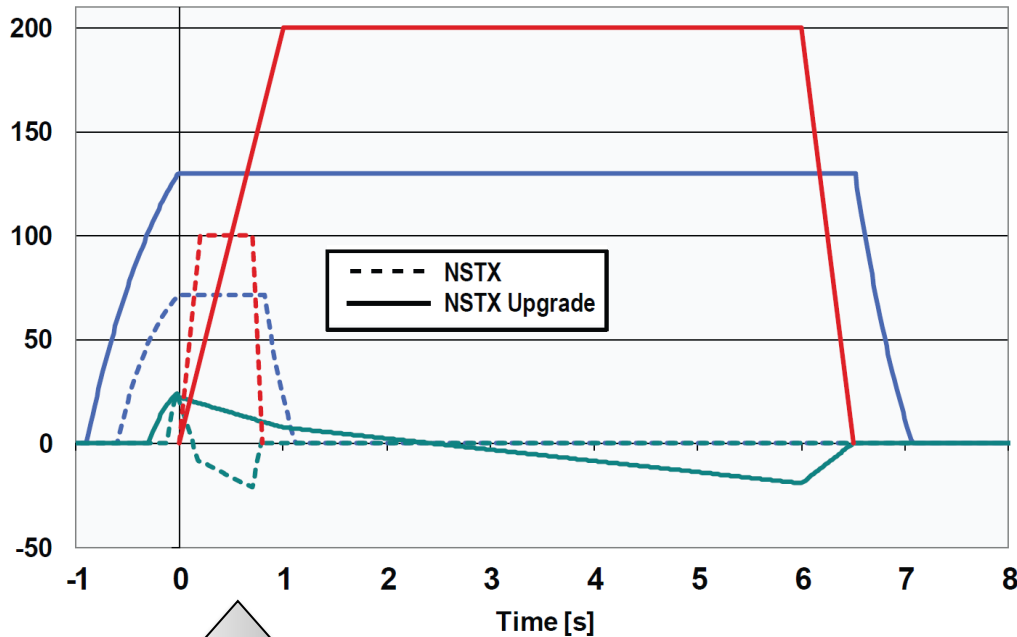


**Pulse-lengths limited by OH, TF coil heating limits**

# NSTX Upgrade supports 5x longer pulses and 100% non-inductive current drive, ultimately with $q$ profile control

## TF, OH, and Plasma Current

Units:  $I_{OH}$  and  $I_{TF}$  [kA],  $I_P$  [kA/10]

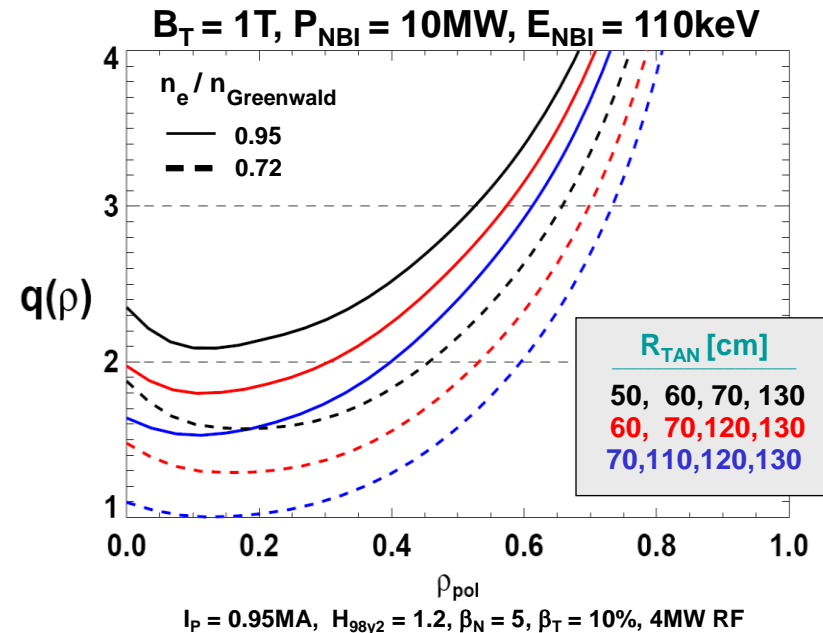


**Changes from NSTX to NSTX Upgrade:**

- $I_P$  and  $B_T$  2x higher, 3x OH flux, flat-top 5x longer,  $W_{TOT}$  up to 4x higher
- Minimum Aspect Ratio  $A = 1.3 \rightarrow 1.5$ , inter-shot time increased  $\sim 2x$

Fully non-inductive scenarios with  $q(r)$  profile will be controllable by:

- NBI source tangency radius
- plasma density
- plasma position (not shown)



$I_P = 0.95MA$ ,  $H_{98y2} = 1.2$ ,  $\beta_N = 5$ ,  $\beta_T = 10\%$ , 4MW RF

# Summary: NSTX and NSTX Upgrade strongly support FNSF development, Materials/PMI, and ITER

- **NSTX Research Highlights:**

- CHI+OH plasma current savings up to 400kA, RF heating of low  $I_p$  to 3keV
- Established divertor heat flux scalings, snowflake divertor for mitigation
- Non-linear simulations suggest micro-tearing may influence ST transport
- High  $\beta_N \sim 6$  sustained with advanced RWM control
- Long-pulse plasmas developed – duration limited by magnet capabilities

- **NSTX Upgrade Progress:**

- Design supports CHI/start-up, PMI, transport, high- $\beta$ , 100% NICD research
- New center-stack design and analysis complete – fabrication beginning
- 2<sup>nd</sup> NBI relocation/installation – ready to begin during Upgrade outage

- **NSTX Upgrade Schedule:**

- Project base-lined (CD-2) December 2010, Final Design Review last week
- NSTX operation to be completed February 2012
- NSTX Upgrade outage to begin April 2012
- NSTX Upgrade first plasma → end of 2014

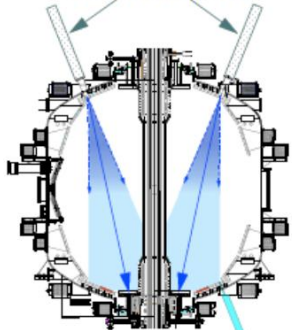
# BACKUP

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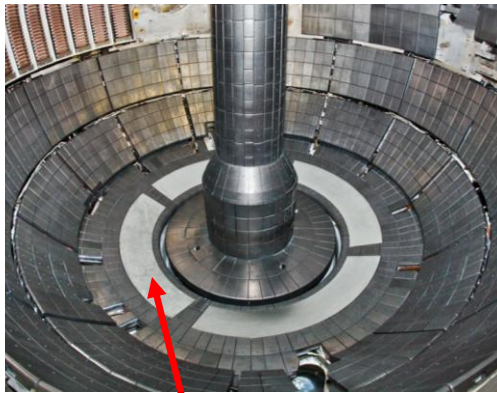
# NSTX is a world leader in assessing lithium plasma facing components as a possible PMI solution for magnetic fusion

- **Solid Li surface coatings**: Pump D, increase confinement, stored energy, pulse length, eliminate ELMs, reduce core MHD instabilities
- **Liquid Lithium Divertor (LLD) motivation**: provide volume D pumping capacity (> solid Li coatings) to provide longer pumping duration + potential for handling high heat flux

Dual Liquid Lithium Evaporator  
For Li wall coatings  
Now routinely used



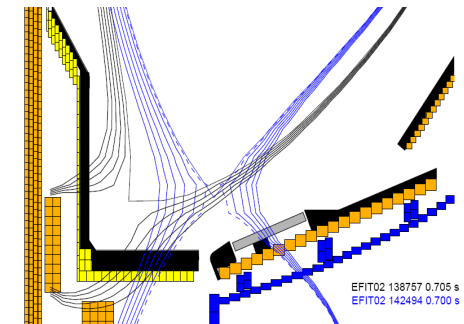
Li evaporators used to coat lower divertor, LLD



4 heatable LLD plates (Mo on Cu)  
Surface temp: 160 – 350+ °C



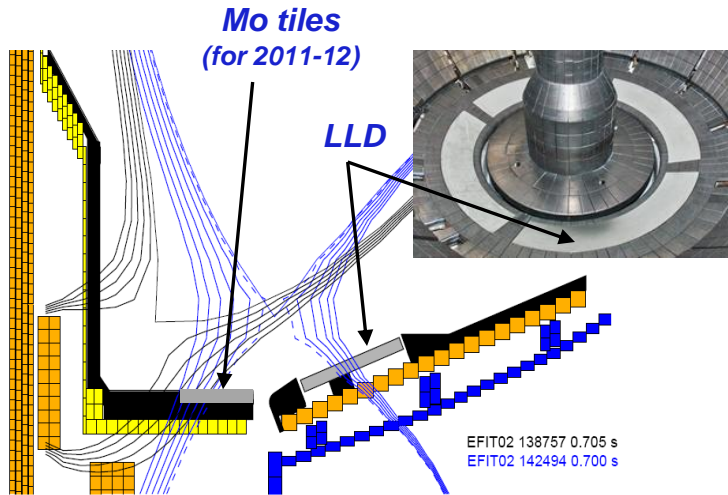
LLD surface cross section:  
plasma sprayed porous Mo



**Controlled scans of strike-point location:**  
On inboard divertor  
On LLD (outboard divertor)

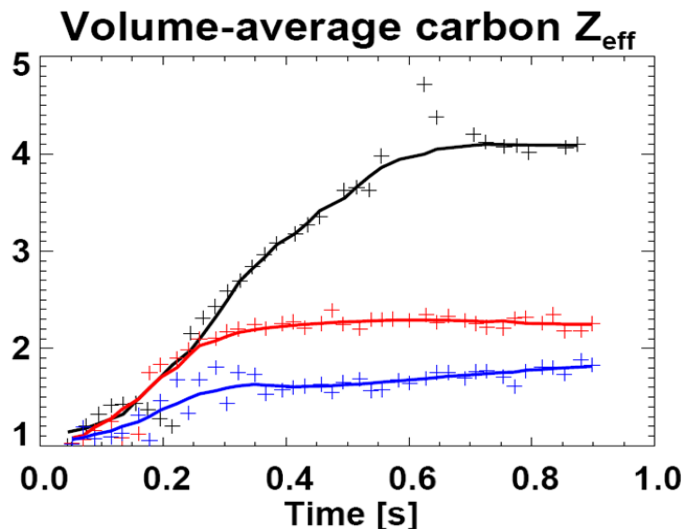
- FY2010: First LLD tests - filled with 67g Li by evaporation (2x needed to fill porosity)

# Operation with outer strike-point on Mo LLD (coated with Li) technically successful, achieved high plasma performance



LLD FY2010 results:

- **LLD did not increase D pumping beyond that achieved with LiTER**
  - Solid Li on C pumps D quite efficiently
  - Liquid Li reacts rapidly w/ background gases (LTX)
  - C on LLD may have impacted D pumping
- **No evidence of Mo from LLD in plasma during normal operation**
- **Operation with strike-point (SP) on LLD reduced core impurities**



◀ SP on inner carbon divertor (no ELMs)

◀ SP on LLD,  $T_{\text{LLD}} < T_{\text{Li-melt}}$

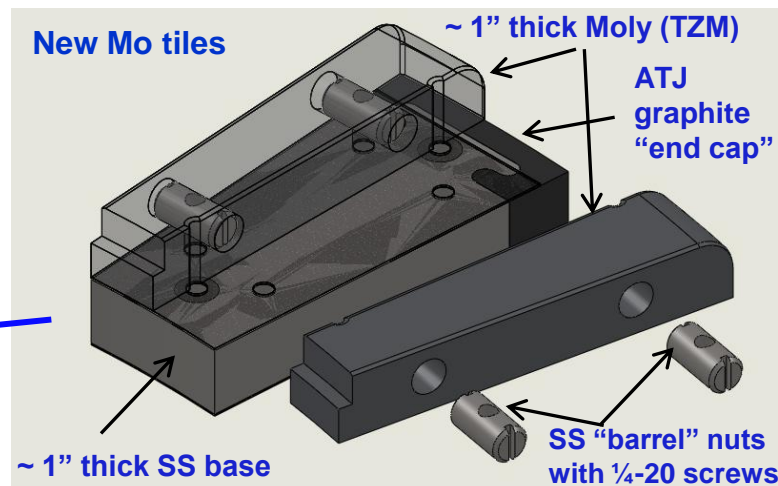
◀ SP on LLD,  $T_{\text{LLD}} > T_{\text{Li-melt}}$  (+ fueling differences)

- No ELMs, no  $\rightarrow$  small, small  $\rightarrow$  larger  
 $\rightarrow$  High-Z impurities also reduced,  $\beta_N > 4$  sustained

Understanding roles of  $\delta$ , C, Mo, Li, ELMs motivates Mo tiles on inboard divertor



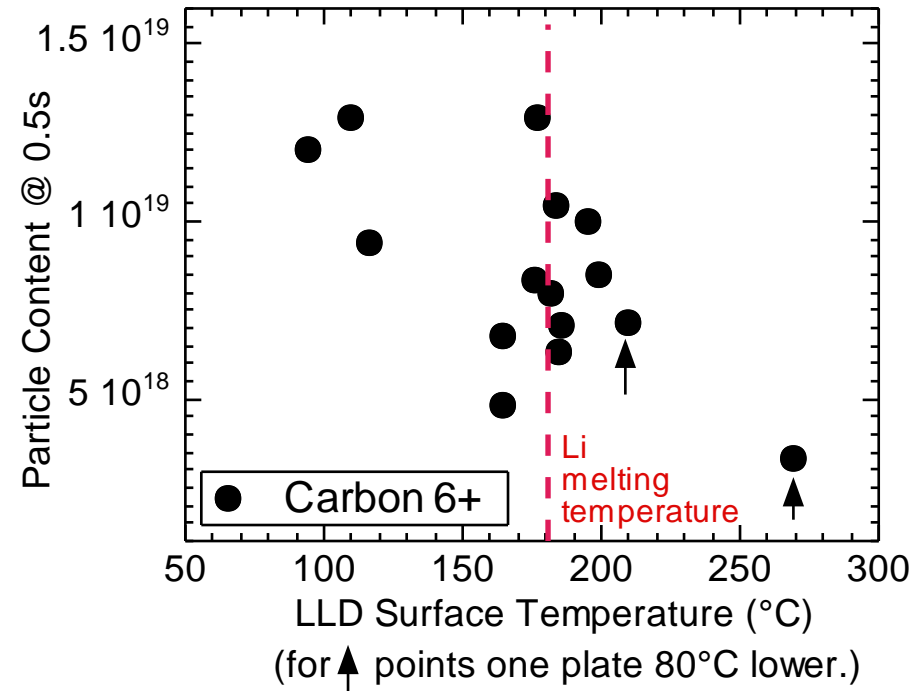
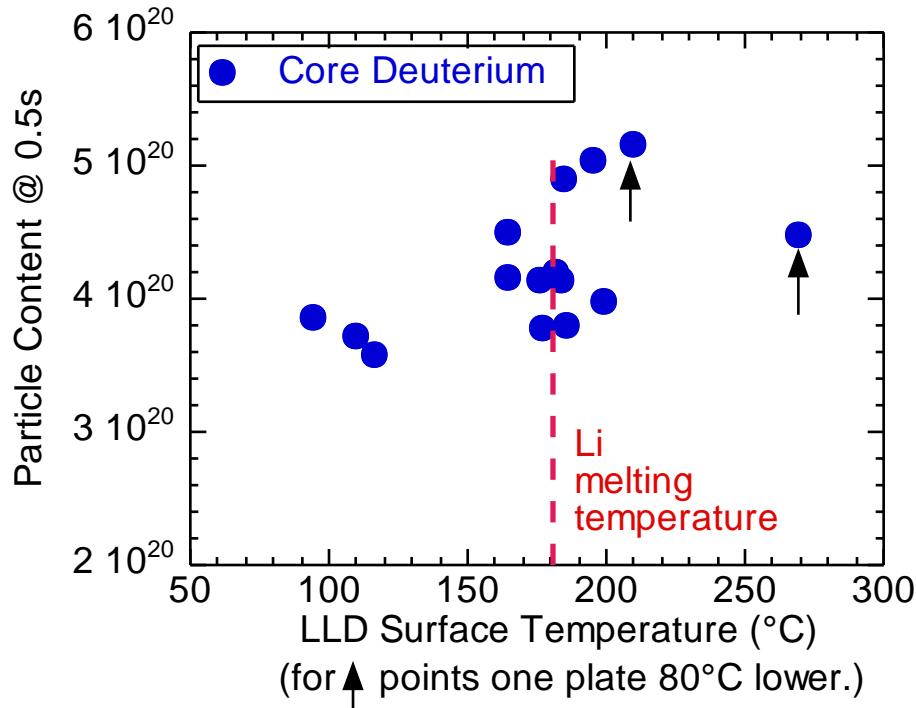
# Mo tiles have recently been installed on inboard divertor to inform decisions on Mo as candidate PFC for Upgrade



- Do Mo tiles provide improved LLD?
  - Li coating with LiTER ~ 2x outboard LLD rate
  - Plasma heating can melt Li during shot

- 2011-12: Assess Mo thermal, mechanical, impurity production performance
  - Does Li help protect Mo thermally? (2010: LLD exhibited temperature saturation)
  - Do Mo PFCs help reduce core C impurity accumulation in Li ELM-free H-mode?

# LLD pumping similar above or below Li melting temperature

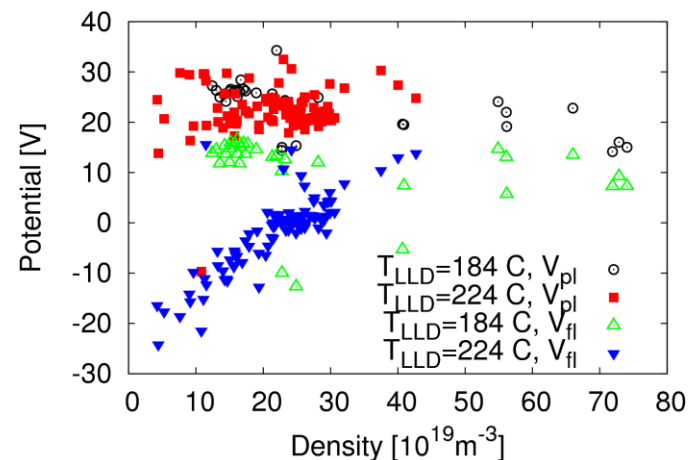


- Constant deuterium fueling for LLD 100% Li fill conditions, 4 plates air heated.
- As LLD surface temperature transitioned from solid temperatures to the liquid regime, the plasma electron and deuterium content remain relatively constant.
- Core carbon C6+ content decreased - may be due in part to increased ELMing and edge turbulence.
- No systematic trend in D-alpha, wall inventory, or ion pumping with a transition above the Li melting temperature.

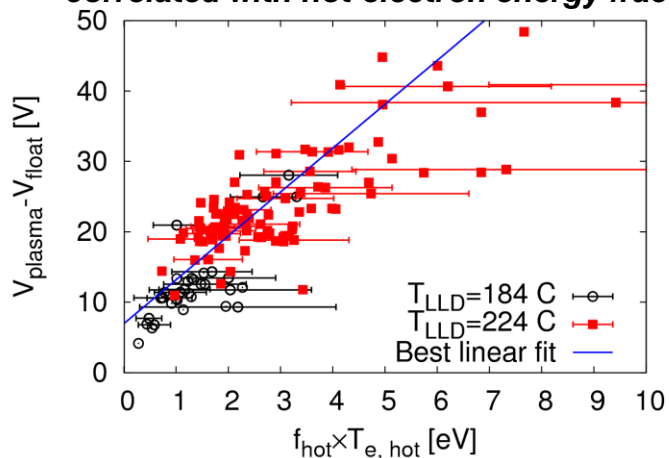
# Higher local electron temperature during LLD melting sequence despite increased fueling

- Langmuir probes indicate increase in near-surface electron temperature during LLD experiments
  - Discharge sequence indicated decreased fueling efficiency during LLD heating (gas increased,  $N_e$  constant)
  - Non-local and classical probe interpretations applied, increase in  $T_e$  consistent with increase in  $V_p - V_f$  difference
  - Temperature rise occurs in hot-electron population of the distribution function
  - Observations consistent with plasma-absorbing PFC

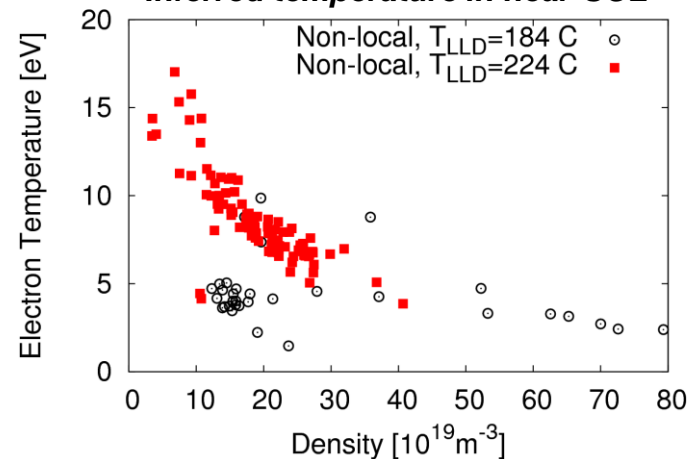
*Floating and Plasma Potentials*



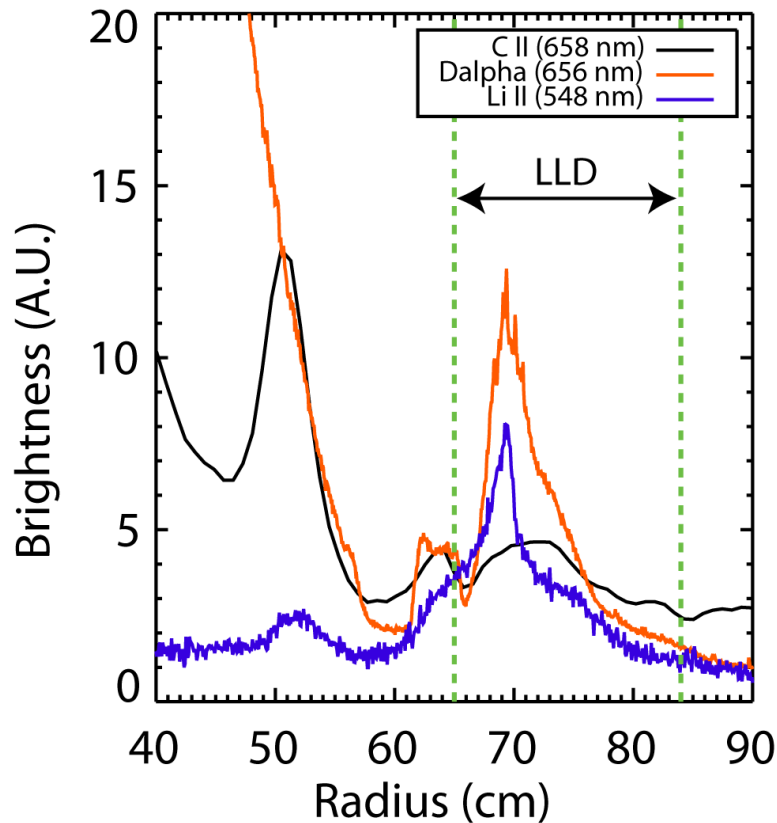
*Difference in potentials most strongly correlated with hot-electron energy fraction*



*Inferred temperature in near-SOL*

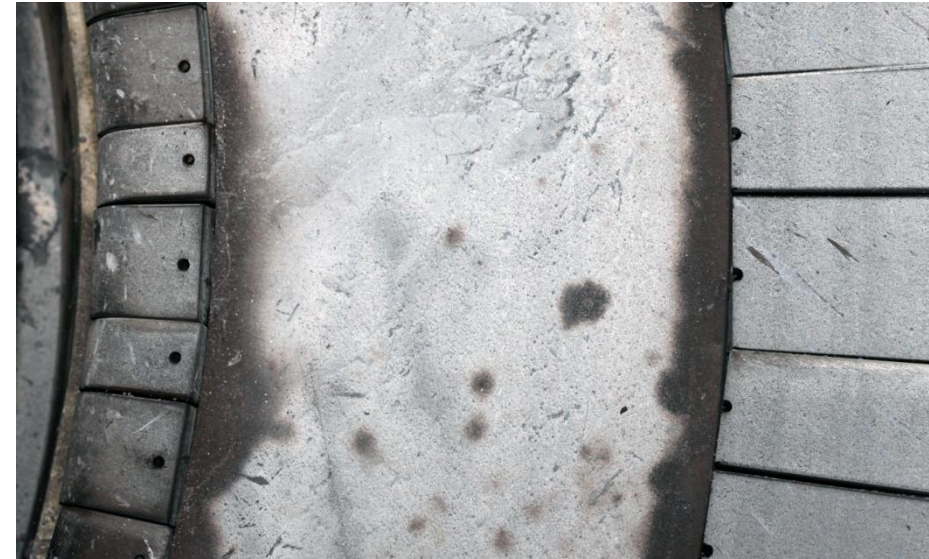


# LLD surface was not pure Li



- Carbon, lithium, and deuterium emission extends across LLD surface after overnight Li evaporation.
- No marked change at LLD location

LLD after vent at end of run



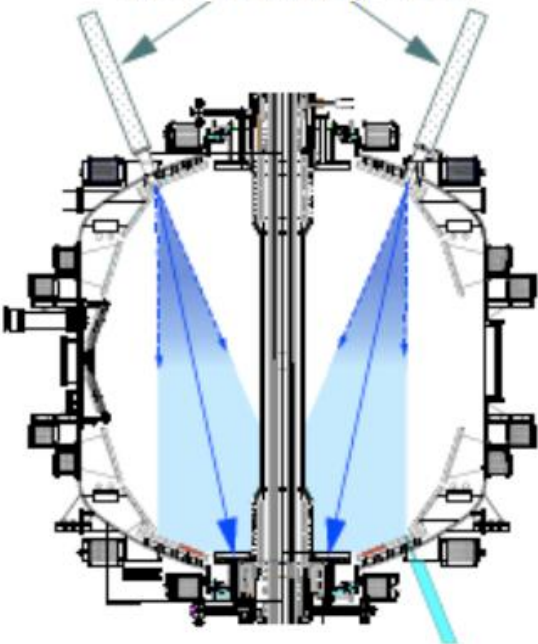
60 Radius (cm) 80

- LLD surface converted to  $\text{Li}_2\text{CO}_3$  following vent
- LLD edges exhibit evidence of sputtered graphite from plate to graphite tile (vessel-ground) arcing.
- Acetic acid tests on the LLD after run suggests that Li does wick into Mo pores and is depleted from the surface at blackened region.
- Reactions with residual gasses also likely

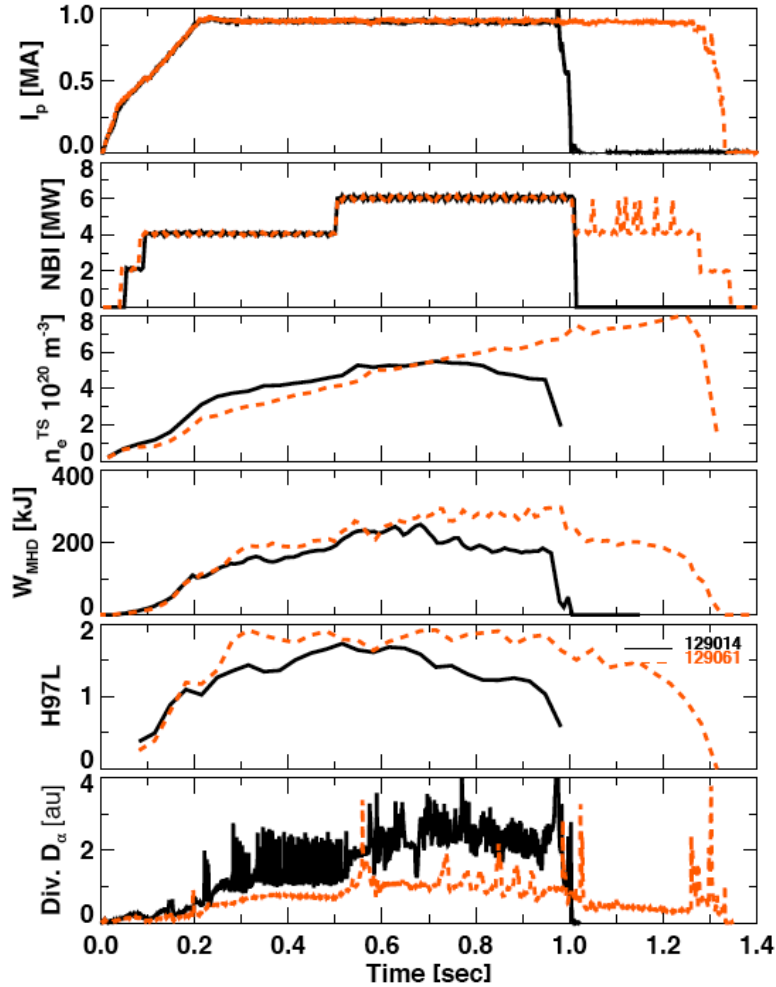
# Solid lithium surface coatings pump D, increase confinement, stored energy, and pulse length, and eliminate ELMs

• 2009: Lithium evaporation became baseline wall-conditioning tool

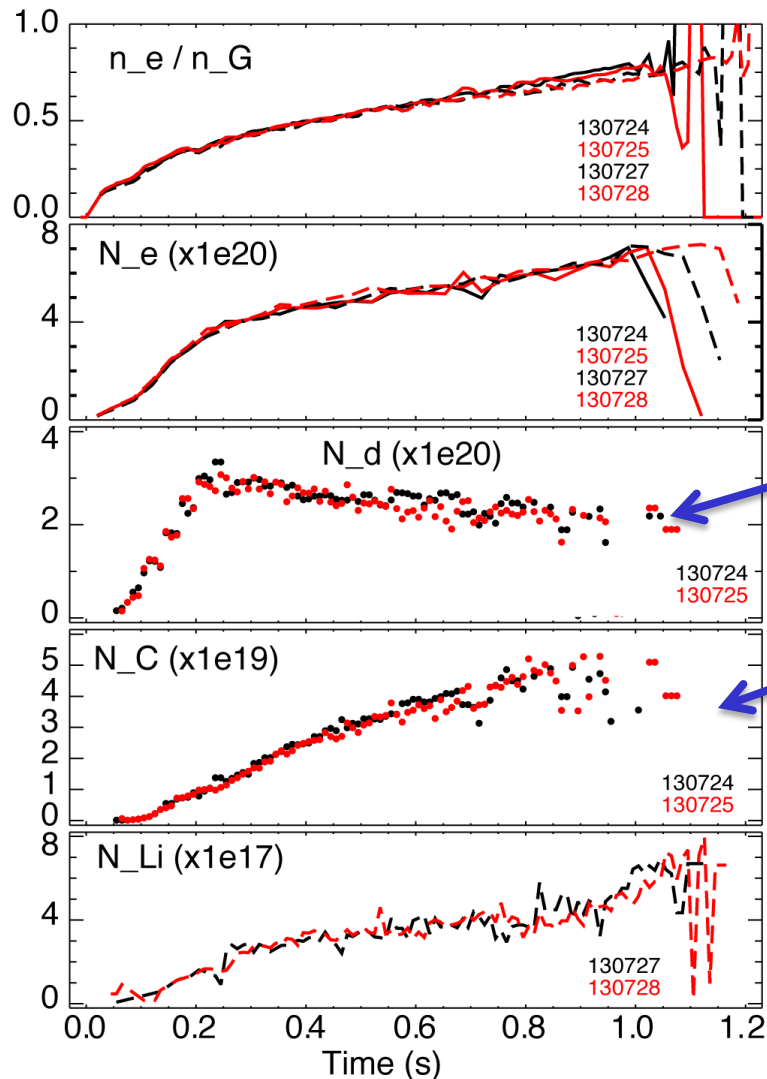
Dual Liquid Lithium Evaporator  
For Li wall coatings  
Now routinely used



- No longer perform between-shot He glow
- Typically deposit 50 to 300mg Li between shots



# With lithium coating pumping, deuteron inventory is constant or even decreasing, C accumulates, Li saturates



Electron density rises monotonically in lithium induced ELM-free H-mode

Strongly Li-pumped discharges exhibit D inventory pump-out

but C inventory increases

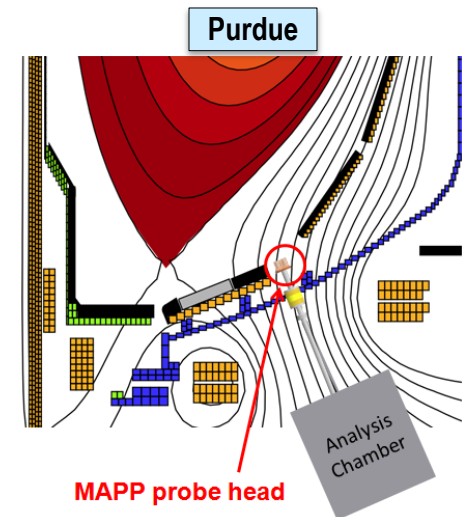
Li inventory increases slowly, remains at very low value

➤ Lithium screening efficiency is high, penetration factor is low:  $N_{Li} / \Gamma_{Li} \sim 0.0001$

As a result, NSTX is shifting emphasis from D inventory control to C impurity reduction

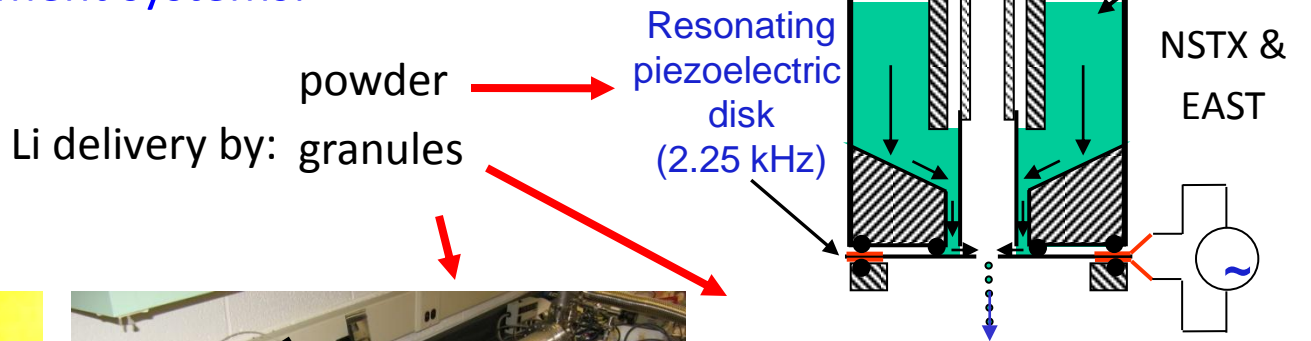
# New diagnostics will be used to investigate relationship between Li-conditioned surface composition & plasma behavior

- Chemistry of Li on C/Mo critical, complex, **under-diagnosed**
- Li very chemically active → *prompt* surface analysis required to characterize the lithiated surface conditions during a shot
- An in-situ materials analysis particle probe (MAPP) being installed on NSTX to provide prompt surface analysis
  - Ex-vessel but in-vacuo surface analysis **within minutes** of plasma exposure using state of the art tools
- Li experiments will utilize MAPP to study:
  - Reactions between evaporated Li and PFCs, gases
  - Correlation surface composition and plasma behavior, comparisons to lab experiments, modeling
  - Characterizations of fueling efficiency, recycling

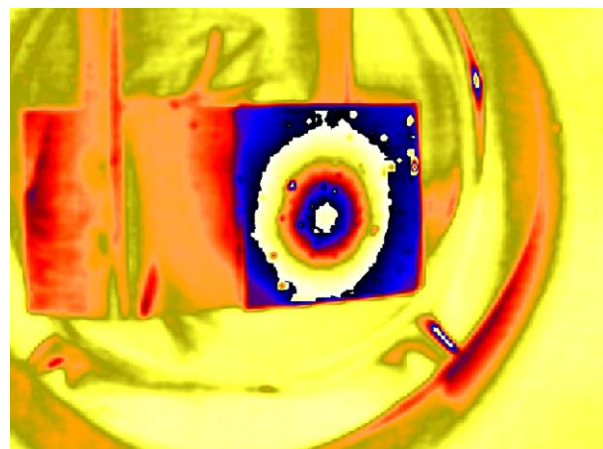


# Lithium Technology developed for NSTX needs

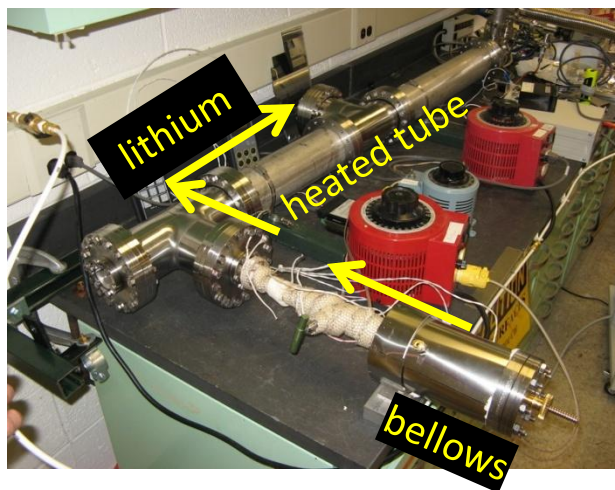
- R&D continuing for LLD performance at high heat flux.
- Continuous Li replenishment systems:



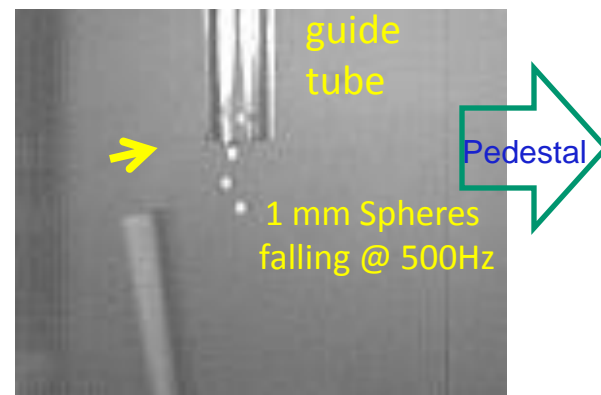
High heat flux test



False color image of LLD sample during NB exposure  
 $T \leq 225 \text{ }^\circ\text{C}$  @  $1.5 \text{ MW/m}^2$  - 3s.  
 Potential PFC for upgrade



10 g of molten Li moved  
 1.1m in vacuum and  
 ejected 7.6 cm from nozzle



500 Hz Impeller Rotating @ 95 m/s  
 Midplane injection for  
 ELM pacing