#### A simple stellarator coil-design algorithm

#### S.R. Hudson & C. Zhu Presented at U. Maryland, 13 Dec. 2017

- 1) The Simplest Possible Algorithm<sup>©</sup> (SPA) for designing stellarator coils is described.
- 2) The coil geometry has "maximum freedom", and the target function is "minimally constrained".
- 3) Fast, reliable and insightful numerical algorithms are enabled by exploiting 1<sup>st</sup> and 2<sup>nd</sup> derivatives with respect to the coil geometry *and* the "target surface".
- 1) P. Merkel, Nucl. Fus., **27** 867 (1987)
- 2) M. Landreman, Nucl. Fus., **57** 046003 (2017)
- 3) Caoxiang Zhu, Stuart R. Hudson et al., Nucl. Fus., 58 345 016008 (2018)
- 4) R.L. Dewar, S.R. Hudson & P.F. Price, Phys. Lett. A., 194 49 (1994)

#### Vacuum fields in given domain described by Laplace

- 1. Given volume  $\mathcal{V}$ , with closed boundary  $\mathcal{S} \equiv \partial \mathcal{V}$ .
- 2. Vacuum fields satisfy  $\nabla \times \mathbf{B} = 0$ , suggests  $\mathbf{B} = \nabla \Phi$ .
- 3. Given  $\mathbf{B} \cdot \mathbf{n}$  on  $\mathcal{S}$ .
- 4. Constraint of net flux  $\oint_{\mathcal{S}} \mathbf{B} \cdot d\mathbf{s} = 0.$
- 5. Toroidal flux  $\Psi \equiv \oint_{\mathcal{L}} \mathbf{A} \cdot d\mathbf{l}$ , (require one loop integral per "hole").
- 6. In  $\mathcal{V}$ , solution to  $\nabla \cdot \nabla \Phi = 0$  is unique.

#### Mathematics becomes numerics: discretize currents and "regularize" functional.

- 1. Introduce  $\mathbf{x}_i(l)$ ,  $i = 1, \ldots, N_C$ , closed current-carrying curves, and let  $\bar{\mathbf{x}}(\theta, \zeta) \equiv S$ .
- 2. With finite degrees-of-freedom, cannot generally *exactly* recover arbitrary  $B_n \equiv \mathbf{B} \cdot \mathbf{n}$  on  $\mathcal{S}$ .
- 3. Instead, minimize the quadratic-flux functional with a penalty on length,

$$\mathcal{F}[\mathbf{x}_i, \bar{\mathbf{x}}] \equiv \oint_{\mathcal{S}} \frac{1}{2} B_n^2 ds + \omega L, \quad \text{where} \ L[\mathbf{x}_i] = \sum_i \oint |\mathbf{x}_i'| \, dl.$$
(1)

- 4. That's all the physics. All that's left is:
  - i. to use a suitable representation for the external currents, and
  - ii. to construct the derivatives of  $\mathcal{F}$ .
- 5 Optimal coils for given surface are defined by  $\frac{\delta \mathcal{F}}{\delta \mathbf{x}_i} = 0.$

### The Biot-Savart law gives the magnetic field, variation in curves gives variation in magnetic field.

1. The magnetic field is from Biot-Savart,

$$\mathbf{B}_{i}(\bar{\mathbf{x}}) = I_{i} \oint_{i} \frac{\mathbf{x}_{i}^{\prime} \times \mathbf{r}}{r^{3}} \, dl, \qquad (1)$$

where  $I_i$  is the current and  $\mathbf{r}(\theta, \zeta, l) \equiv \bar{\mathbf{x}}(\theta, \zeta) - \mathbf{x}_i(l)$  and  $\mathbf{x}'_i \equiv \frac{\partial \mathbf{x}_i}{\partial l}$ .

- 2. For simplicity, set  $I_i = 1$ . (Trivial solutions avoided, and can ignore toroidal flux constraint.)
- 3. Variations in the curve induce variations in the field,

$$\delta \mathbf{B}(\bar{\mathbf{x}}) = \oint_{i} (\delta \mathbf{x}_{i} \times \mathbf{x}_{i}') \cdot \mathbf{R}_{i} \, dl, \qquad (2)$$

where  $\mathbf{R} = \frac{3 \mathbf{r} \mathbf{r}}{r^5} - \frac{\mathbf{I}}{r^3}$ , and  $\mathbf{I}$  is the "idemfactor", e.g.  $\mathbf{I} = \mathbf{i} \mathbf{i} + \mathbf{j} \mathbf{j} + \mathbf{k} \mathbf{k}$ .

4. Let me go through the algebra more slowly.

$$\mathbf{B} = \oint \frac{(\mathbf{x}' \times \mathbf{r})}{r^3} \, dl, \text{ where } \mathbf{r} \equiv \bar{\mathbf{x}} - \mathbf{x}, \ r \equiv \sqrt{\mathbf{r} \cdot \mathbf{r}}, \ \mathbf{x}' \equiv \partial_l \mathbf{x} \tag{1}$$

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$$\delta \mathbf{B} = \oint \frac{(\delta \mathbf{x}' \times \mathbf{r})}{r^3} dl \qquad \qquad -\oint \frac{(\mathbf{x}' \times \delta \mathbf{x})}{r^3} dl + 3\oint \frac{(\mathbf{x}' \times \mathbf{r})(\mathbf{r} \cdot \delta \mathbf{x})}{r^5} dl$$
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Correct, but not "transparent". Do tangential variations,  $\delta \mathbf{x} \times \mathbf{x}' = 0$ , change **B**?

$$\mathbf{B} = \oint \frac{(\mathbf{x}' \times \mathbf{r})}{r^3} dl, \text{ where } \mathbf{r} \equiv \bar{\mathbf{x}} - \mathbf{x}, r \equiv \sqrt{\mathbf{r} \cdot \mathbf{r}}, \mathbf{x}' \equiv \partial_l \mathbf{x} \tag{1}$$

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$$= \oint (\delta \mathbf{x} \times \mathbf{x}') \cdot \left(\frac{\mathbf{r} \, 3 \, \mathbf{r}}{r^5} - \frac{\mathbf{I}}{r^3}\right) \, dl, \text{ where } \mathbf{v} \cdot \mathbf{I} = \mathbf{I} \cdot \mathbf{v} = \mathbf{v}, \tag{3}$$

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(2)

$$= \oint (\delta \mathbf{x} \times \mathbf{x}') \cdot \left(\frac{\mathbf{r} \, 3 \, \mathbf{r}}{r^5} - \frac{\mathbf{I}}{r^3}\right) \, dl, \text{ where } \mathbf{v} \cdot \mathbf{I} = \mathbf{I} \cdot \mathbf{v} = \mathbf{v}, \tag{3}$$

$$\delta \mathbf{B} = \oint (\delta \mathbf{x} \times \mathbf{x}') \cdot \mathbf{R} \, dl \tag{4}$$

This is concise, and shows that tangential variations,  $\delta \mathbf{x} \times \mathbf{x}' = 0$ , do not alter the field.

# Variations in line integrals with respect to variations in the line: length

$$L \equiv \oint (\mathbf{x}' \cdot \mathbf{x}')^{1/2} \, dl \tag{1}$$

$$\delta L = \oint (\mathbf{x}' \cdot \mathbf{x}')^{-1/2} (\mathbf{x}' \cdot \delta \mathbf{x}') \, dl \tag{2}$$

$$= \oint \delta \mathbf{x} \cdot \mathbf{x}' (\mathbf{x}' \cdot \mathbf{x}')^{-3/2} \mathbf{x}' \cdot \mathbf{x}'' \, dl - \oint \delta \mathbf{x} \cdot \mathbf{x}'' (\mathbf{x}' \cdot \mathbf{x}')^{-1/2} \, dl \tag{3}$$

Correct, but not transparent.

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Correct, but not transparent.

Use 
$$(\delta \mathbf{x} \times \mathbf{x}') \cdot (\mathbf{x}' \times \mathbf{x}'') = (\delta \mathbf{x} \cdot \mathbf{x}') \cdot (\mathbf{x}' \cdot \mathbf{x}'') - (\delta \mathbf{x} \cdot \mathbf{x}'') \cdot (\mathbf{x}' \cdot \mathbf{x}').$$
  

$$\delta L = -\oint (\delta \mathbf{x} \times \mathbf{x}') \cdot \boldsymbol{\kappa}, \text{ where } \boldsymbol{\kappa} \equiv \frac{\mathbf{x}' \times \mathbf{x}''}{(\mathbf{x}' \cdot \mathbf{x}')^{3/2}}$$
(4)

#### The first variation with respect to variations in the curve is easy to calculate

1. The first variation of the penalized quadratic-flux,  $\mathcal{F}[\mathbf{x}_i, \bar{\mathbf{x}}] \equiv \int_{\mathcal{S}} \frac{1}{2} B_n^2 ds + \omega L$ , is

$$\delta \mathcal{F} = \oint_{i} \delta \mathbf{x}_{i} \cdot \frac{\delta F}{\delta \mathbf{x}_{i}} \, dl, \qquad (1)$$

where 
$$\frac{\delta \mathcal{F}}{\delta \mathbf{x}_i} \equiv \mathbf{x}'_i \times \left( \oint_{\mathcal{S}} \mathbf{R}_{i,n} B_n \, ds + \omega \, \boldsymbol{\kappa}_i \right).$$
 (2)

2. "Slow motion" descent algorithm is easy to implement,

$$\frac{\partial \mathbf{x}_i}{\partial \tau} = -\frac{\delta \mathcal{F}}{\delta \mathbf{x}_i} , \quad \frac{\partial \mathcal{F}}{\partial \tau} = -\oint_i \left(\frac{\delta \mathcal{F}}{\delta \mathbf{x}_i}\right)^2 dl \le 0.$$
(3)

3. Coils cannot pass through surface (infinities); descent algorithm preserves linking

Gauss linking integral 
$$= \frac{1}{4\pi} \oint_{i} \oint_{a} \frac{\mathbf{x}_{i} - \mathbf{x}_{a}}{|\mathbf{x}_{i} - \mathbf{x}_{a}|^{3}} \cdot d\mathbf{x}_{i} \times d\mathbf{x}_{a}.$$
 (4)

# Second derivatives can be calculated, allows fast algorithms and sensitivity analysis.

1. Let  $\mathbf{c} \equiv {\mathbf{x}_{i,n}}$ , degrees-of-freedom that parameterize external currents.

For example,  $\mathbf{x}_i(l) = x_i(l)\mathbf{i} + y_i(l)\mathbf{j} + z_i(l)\mathbf{z}$  where

$$x_i(l) = \sum_n \left[ x_{i,n}^c \cos(nl) + x_{i,n}^s \sin(nl) \right]$$
(1)

$$y_i(l) = \sum_n \left[ y_{i,n}^c \cos(nl) + y_{i,n}^s \sin(nl) \right]$$
(2)

$$z_i(l) = \sum_n \left[ z_{i,n}^c \cos(nl) + z_{i,n}^s \sin(nl) \right]$$
(3)

2. 
$$\mathcal{F}(\mathbf{c} + \delta \mathbf{c}) \approx \mathcal{F}(\mathbf{c}) + \nabla_{\mathbf{c}} \mathcal{F} \cdot \delta \mathbf{c} + \frac{1}{2} \delta \mathbf{c}^T \cdot \nabla_{\mathbf{cc}}^2 \mathcal{F} \cdot \delta \mathbf{c}$$

- 3. Inverting Hessian allows Newton method.
  [C. Zhu, S.R. Hudson *et al.*, Plasma Phys. Control. Fusion, submitted (2018)]
- 4. Eigenvalues of Hessian describe sensitivity to coil placement errors. [C. Zhu, S.R. Hudson *et al.*, in preparation (2018)]

# The quadratic-flux is an analytic function of the surface. So, what happens if the surface varies?

1. The variation in F resulting from variations,  $\delta \mathbf{x}_i$  and  $\delta \bar{\mathbf{x}}$ , in the geometry of the *i*-th coil and the surface is

$$\delta^2 F = \oint_i \delta \mathbf{x}_i \cdot \oint_{\mathcal{S}} \frac{\delta^2 F}{\delta \mathbf{x}_i \delta \bar{\mathbf{x}}} \cdot \delta \bar{\mathbf{x}} \, ds \, dl, \tag{1}$$

where

$$\frac{\delta^2 F}{\delta \mathbf{x}_i \delta \bar{\mathbf{x}}} \equiv \mathbf{x}'_i \times (\mathbf{R}_S \cdot \nabla B_n + \mathbf{B}_S \cdot \nabla \mathbf{R}_n + B_n \mathbf{R} \cdot \mathbf{H}) \mathbf{n},$$
(2)

where

i.  $\mathbf{B}_S \equiv \mathbf{B} - B_n \mathbf{n}$  is the projection of  $\mathbf{B}$  in the tangent plane to  $\bar{\mathbf{x}}$ , and  $\mathbf{R}_S \equiv \mathbf{R} - \mathbf{R}_n \mathbf{n}$ . ii. The mean curvature can be written  $\mathbf{H} \equiv -\mathbf{n} (\nabla \cdot \mathbf{n})$ .

3. The shape of the optimal coils must change with the surface to preserve  $\nabla_{\mathbf{c}} \mathcal{F} = 0$ ,

 $\nabla_{\mathbf{c}} \mathcal{F}(\mathbf{c} + \delta \mathbf{c}, \mathbf{s} + \delta \mathbf{s}) \approx \nabla_{\mathbf{cc}}^2 \mathcal{F} \cdot \delta \mathbf{c} + \nabla_{\mathbf{cs}}^2 \mathcal{F} \cdot \delta \mathbf{s} = 0$ , and from this

$$\frac{\partial \mathbf{c}}{\partial \mathbf{s}} = -\left(\nabla_{\mathbf{cc}}^2 \mathcal{F}\right)^{-1} \cdot \nabla_{\mathbf{cs}}^2 \mathcal{F}.$$
(3)

1. Parameterized surface,  $\mathbf{x}(\theta, \zeta)$ , tangent vectors  $\mathbf{x}_{\theta} \equiv \frac{\partial \mathbf{x}}{\partial \theta}$  and  $\mathbf{x}_{\zeta} \equiv \frac{\partial \mathbf{x}}{\partial \zeta}$ ,

normal 
$$\mathbf{n} \equiv \frac{\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}}{|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|}, \quad d(\text{area}) \quad ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta.$$
 (1)

where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

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where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

2. Variations  $\mathbf{x}(\theta,\zeta) \to \mathbf{x}(\theta,\zeta) + \delta \mathbf{x}(\theta,\zeta)$  induce  $\delta \mathbf{x}_{\theta} \equiv \partial_{\theta} \delta \mathbf{x}, \quad \delta \mathbf{x}_{\zeta} \equiv \partial_{\zeta} \delta \mathbf{x}$ 

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \frac{1}{2} [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{-1/2} 2 (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} + \mathbf{x}_{\theta} \times \delta \mathbf{x}_{\zeta})$$
(2)

1. Parameterized surface,  $\mathbf{x}(\theta, \zeta)$ , tangent vectors  $\mathbf{x}_{\theta} \equiv \frac{\partial \mathbf{x}}{\partial \theta}$  and  $\mathbf{x}_{\zeta} \equiv \frac{\partial \mathbf{x}}{\partial \zeta}$ ,

normal 
$$\mathbf{n} \equiv \frac{\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}}{|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|}, \quad d(area) \quad ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta.$$
 (1)

where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \frac{1}{2} [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{-1/2} 2 (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} + \mathbf{x}_{\theta} \times \delta \mathbf{x}_{\zeta}) \quad (2)$$
  
=  $\mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta})$  (3)

1. Parameterized surface,  $\mathbf{x}(\theta, \zeta)$ , tangent vectors  $\mathbf{x}_{\theta} \equiv \frac{\partial \mathbf{x}}{\partial \theta}$  and  $\mathbf{x}_{\zeta} \equiv \frac{\partial \mathbf{x}}{\partial \zeta}$ ,

normal 
$$\mathbf{n} \equiv \frac{\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}}{|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|}, \quad d(area) \quad ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta.$$
 (1)

where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \frac{1}{2} [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{-1/2} 2 (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} + \mathbf{x}_{\theta} \times \delta \mathbf{x}_{\zeta})$$
(2)

$$= \mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta})$$
(3)

$$= \delta \mathbf{x}_{\theta} \cdot (\mathbf{x}_{\zeta} \times \mathbf{n}) - \delta \mathbf{x}_{\zeta} \cdot (\mathbf{x}_{\theta} \times \mathbf{n})$$
(4)

1. Parameterized surface,  $\mathbf{x}(\theta, \zeta)$ , tangent vectors  $\mathbf{x}_{\theta} \equiv \frac{\partial \mathbf{x}}{\partial \theta}$  and  $\mathbf{x}_{\zeta} \equiv \frac{\partial \mathbf{x}}{\partial \zeta}$ ,

normal 
$$\mathbf{n} \equiv \frac{\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}}{|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|}, \quad d(area) \quad ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta.$$
 (1)

where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \frac{1}{2} [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{-1/2} 2 (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} + \mathbf{x}_{\theta} \times \delta \mathbf{x}_{\zeta})$$
(2)

$$= \mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta})$$
(3)

$$= \delta \mathbf{x}_{\theta} \cdot (\mathbf{x}_{\zeta} \times \mathbf{n}) - \delta \mathbf{x}_{\zeta} \cdot (\mathbf{x}_{\theta} \times \mathbf{n})$$
(4)

$$\int \delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta = -\int \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta\theta} \times \mathbf{n} + \mathbf{x}_{\zeta} \partial_{\theta} \times \mathbf{n}) \, d\theta d\zeta + \int \delta \mathbf{x} \cdot (\mathbf{x}_{\theta\zeta} \times \mathbf{n} + \mathbf{x}_{\theta} \partial_{\zeta} \times \mathbf{n}) \, d\theta d\zeta$$
(5)

1. Parameterized surface,  $\mathbf{x}(\theta, \zeta)$ , tangent vectors  $\mathbf{x}_{\theta} \equiv \frac{\partial \mathbf{x}}{\partial \theta}$  and  $\mathbf{x}_{\zeta} \equiv \frac{\partial \mathbf{x}}{\partial \zeta}$ ,

normal 
$$\mathbf{n} \equiv \frac{\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}}{|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|}, \quad d(area) \quad ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta.$$
 (1)

where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \frac{1}{2} [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{-1/2} 2 (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} + \mathbf{x}_{\theta} \times \delta \mathbf{x}_{\zeta})$$
(2)

$$= \mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta})$$
(3)

$$= \delta \mathbf{x}_{\theta} \cdot (\mathbf{x}_{\zeta} \times \mathbf{n}) - \delta \mathbf{x}_{\zeta} \cdot (\mathbf{x}_{\theta} \times \mathbf{n})$$
(4)

$$\int \delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta = -\int \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta\theta} \times \mathbf{n} + \mathbf{x}_{\zeta} \partial_{\theta} \times \mathbf{n}) \, d\theta d\zeta + \int \delta \mathbf{x} \cdot (\mathbf{x}_{\theta\zeta} \times \mathbf{n} + \mathbf{x}_{\theta} \partial_{\zeta} \times \mathbf{n}) \, d\theta d\zeta$$
(5)  
$$= -\int \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta} \partial_{\theta} - \mathbf{x}_{\theta} \partial_{\zeta}) \times \mathbf{n} \, d\theta d\zeta$$
(6)

1. Parameterized surface,  $\mathbf{x}(\theta, \zeta)$ , tangent vectors  $\mathbf{x}_{\theta} \equiv \frac{\partial \mathbf{x}}{\partial \theta}$  and  $\mathbf{x}_{\zeta} \equiv \frac{\partial \mathbf{x}}{\partial \zeta}$ ,

normal 
$$\mathbf{n} \equiv \frac{\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}}{|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|}, \quad d(area) \quad ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta.$$
 (1)

where  $|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}.$ 

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \frac{1}{2} [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{-1/2} 2 (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}).(\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} + \mathbf{x}_{\theta} \times \delta \mathbf{x}_{\zeta})$$
(2)

$$= \mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta})$$
(3)

$$= \mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta})$$
(3)  
$$= \delta \mathbf{x}_{\theta} \cdot (\mathbf{x}_{\zeta} \times \mathbf{n}) - \delta \mathbf{x}_{\zeta} \cdot (\mathbf{x}_{\theta} \times \mathbf{n})$$
(4)

$$\int \delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| \, d\theta d\zeta = -\int \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta\theta} \times \mathbf{n} + \mathbf{x}_{\zeta} \partial_{\theta} \times \mathbf{n}) \, d\theta d\zeta + \int \delta \mathbf{x} \cdot (\mathbf{x}_{\theta\zeta} \times \mathbf{n} + \mathbf{x}_{\theta} \partial_{\zeta} \times \mathbf{n}) \, d\theta d\zeta$$
(5)

$$= -\int \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta} \partial_{\theta} - \mathbf{x}_{\theta} \partial_{\zeta}) \times \mathbf{n} \, d\theta d\zeta$$
(6)

$$= \int \delta \mathbf{x} \cdot \mathbf{H} \, ds, \text{ where } \mathbf{H} \equiv -\mathbf{n} \left( \nabla \cdot \mathbf{n} \right) = \text{mean curvature.}$$
(7)

# Can the surface be varied to simplify the coils under the constraint of conserved plasma properties?

1. Introduce a measure of coil complexity,  $\mathcal{C}(\mathbf{c})$ , that we wish to minimize, e.g. integrated torsion,

$$\mathcal{C} \equiv \oint \frac{\mathbf{x}' \cdot \mathbf{x}'' \times \mathbf{x}'''}{|\mathbf{x}' \times \mathbf{x}''|^2} dl \tag{1}$$

which quantifies "non-planar-ness" of the coils.

- 2. Introduce a plasma property,  $\mathcal{P}(\bar{\mathbf{x}})$ , that we wish to constrain, e.g. rotational-transform on axis.
- 3. Can minimize coil complexity subject to constrained plasma properties, i.e. extremize

$$\mathcal{G}(\bar{\mathbf{x}}) \equiv \mathcal{C}(\mathbf{x}_i(\bar{\mathbf{x}})) + \lambda \left[ \mathcal{P}(\bar{\mathbf{x}}) - \mathcal{P}_0 \right].$$
<sup>(2)</sup>

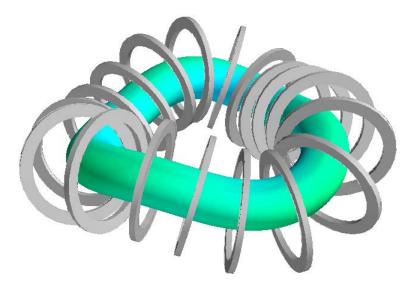
- 4. Rotational-transform is an easy first test: rotational-transform can be produced [Mercier (1964)]
  - i. by shaping the boundary (i.e., rotating elliptical boundary), or by
  - ii. by shaping the magnetic axis (through torsion), or

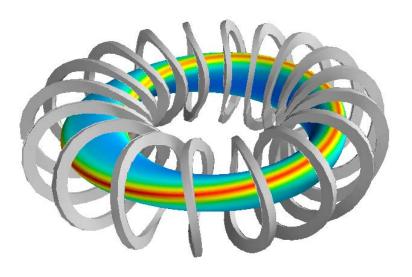
iii. by both.

5. Solutions satisfy  $\frac{\partial \mathbf{x}_i}{\partial \bar{\mathbf{x}}} \cdot \frac{\partial \mathcal{C}}{\partial \mathbf{x}_i} + \lambda \frac{\partial \mathcal{P}}{\partial \bar{\mathbf{x}}} = 0.$ 

#### A circular cross-section on an axis with torsion gives simpler coils than a rotating ellipse on a circular magnetic axis.

- 1. "Simple" in this case means more planar. Have not yet measured coil-coil spacing, for example.
- 2. The following have
  - i. the same rotational-transform on axis,  $\epsilon \approx 0.101,$  and good flux surfaces,
  - ii. total volume =  $0.7986m^3$ , 18 coils,
  - iii. average int. torsion of coils is  $0.005m^{-1}$  for circular cross-section high-torsion axis, and  $0.800m^{-1}$  for rotating elliptical cross-section circular axis.





area = 
$$\int_{\mathcal{S}} ds$$
, where  $ds \equiv |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| d\theta d\zeta$ , and  $\mathbf{x}_{\theta} \equiv \partial_{\theta} \mathbf{x}$  (1)

$$|\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = [(\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}) \cdot (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta})]^{1/2}$$
(2)

$$\delta |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}| = \mathbf{n} \cdot (\delta \mathbf{x}_{\theta} \times \mathbf{x}_{\zeta} - \delta \mathbf{x}_{\zeta} \times \mathbf{x}_{\theta}), \text{ where } \mathbf{n} = (\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}) / |\mathbf{x}_{\theta} \times \mathbf{x}_{\zeta}|$$
(3)

$$\delta(\text{area}) = \int_{\mathcal{S}} \partial_{\theta} \delta \mathbf{x} \cdot \mathbf{x}_{\zeta} \times \mathbf{n} \, d\theta d\zeta - \int_{\mathcal{S}} \partial_{\zeta} \delta \mathbf{x} \cdot \mathbf{x}_{\theta} \times \mathbf{n} \, d\theta d\zeta \tag{4}$$

$$= -\int_{\mathcal{S}} \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta\theta} \times \mathbf{n} + \mathbf{x}_{\zeta} \partial_{\theta} \times \mathbf{n}) \, d\theta d\zeta$$
(5)

$$+ \int_{\mathcal{S}} \delta \mathbf{x} \cdot (\mathbf{x}_{\theta\zeta} \times \mathbf{n} + \mathbf{x}_{\theta} \partial_{\zeta} \times \mathbf{n}) \, d\theta d\zeta \tag{6}$$

$$= -\int_{\mathcal{S}} \delta \mathbf{x} \cdot (\mathbf{x}_{\zeta} \partial_{\theta} - \mathbf{x}_{\theta} \partial_{\zeta}) \times \mathbf{n} \, d\theta d\zeta$$
<sup>(7)</sup>

$$= -\int_{\mathcal{S}} \delta \mathbf{x} \cdot (\mathbf{n} \times \nabla) \times \mathbf{n} \, ds, \text{ where } \mathbf{n} = \nabla s / |\nabla s| \text{ and } \nabla \equiv \nabla s \, \partial_s + \nabla \theta \, \partial_\theta + \nabla \zeta \, \partial_\zeta, \quad (8)$$

$$= -\int_{\mathcal{S}} \delta \mathbf{x} \cdot \mathbf{n} \, (\nabla \cdot \mathbf{n}) \, ds \qquad (9)$$

$$= -\int_{\mathcal{S}} \delta \mathbf{x} \cdot \mathbf{n} \left( \nabla \cdot \mathbf{n} \right) \, ds \tag{9}$$

$$= -\int_{\mathcal{S}} \delta \mathbf{x} \cdot \mathbf{H} \, ds, \quad \text{mean curvature } \mathbf{H} \equiv \mathbf{n} \left( \nabla \cdot \mathbf{n} \right) \tag{10}$$

#### 1) R.L. Dewar, S.R. Hudson & P.F. Price, Phys. Lett. A., **194** 49 (1994)

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